

APPENDIX 1

VICINITY MAP AND IMPERVIOUS SURFACE EXHIBIT

SITE

ROAD

WEST BORDEN ROAD

POSAS

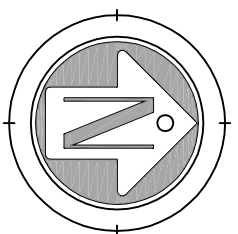
LAS

N.

WEST MISSION ROAD

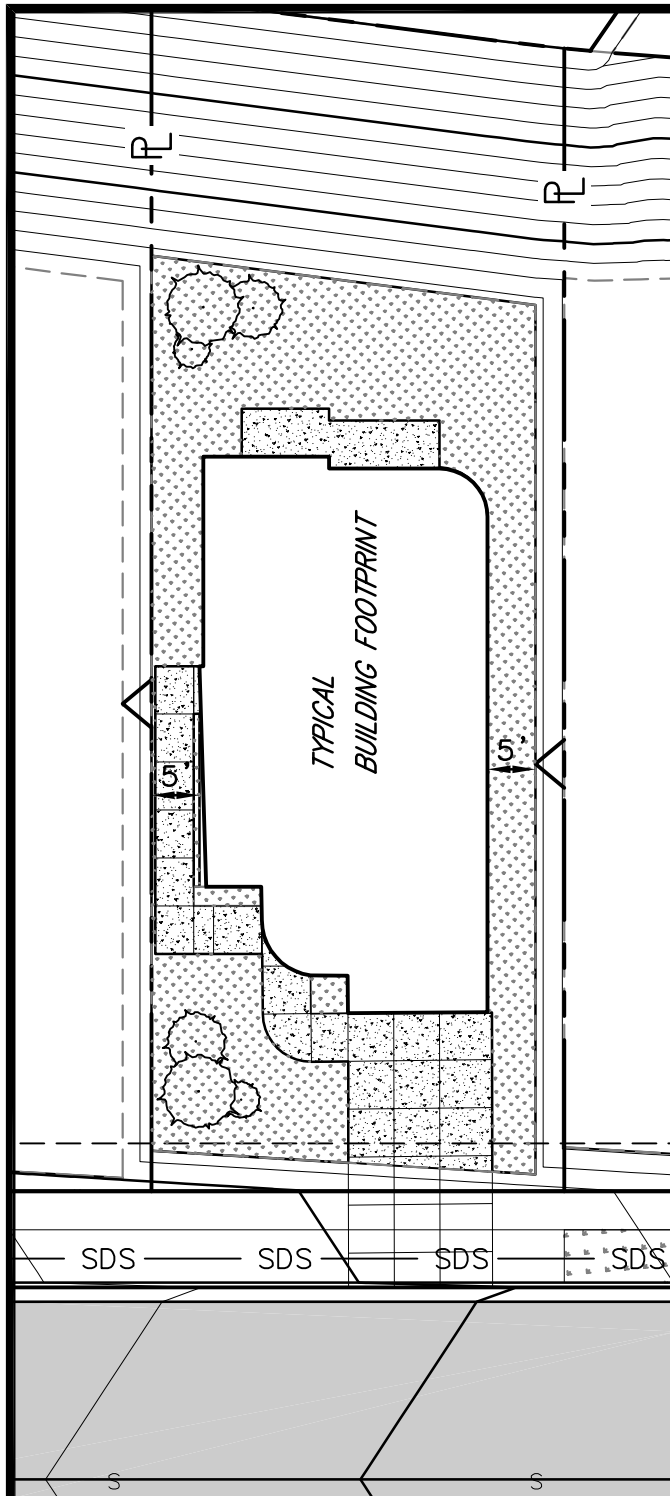
GRAND AVENUE

HWY 78



VICINITY MAP

NOT TO SCALE



IMPERVIOUS SURFACE

BUILDING FOOTPRINT=1576 SF

DRIVEWAY & PATHWAY =465 SF

PATIO =103 SF

TOTAL IMPERVIOUS SURFACE=2144 SF

EFFECTIVE LOT SURFACE (EXCLUDE THE SLOPE) =3676 SF

PERCENTAGE OF IMPERVIOUS:





$$\frac{2144 \text{ SF}}{3676 \text{ SF}} = 58\% \text{ IMPERVIOUS}$$

THEREFORE WE USE 60%
IMPERVIOUS AREA ASSUMPTION FOR
ALL PADS

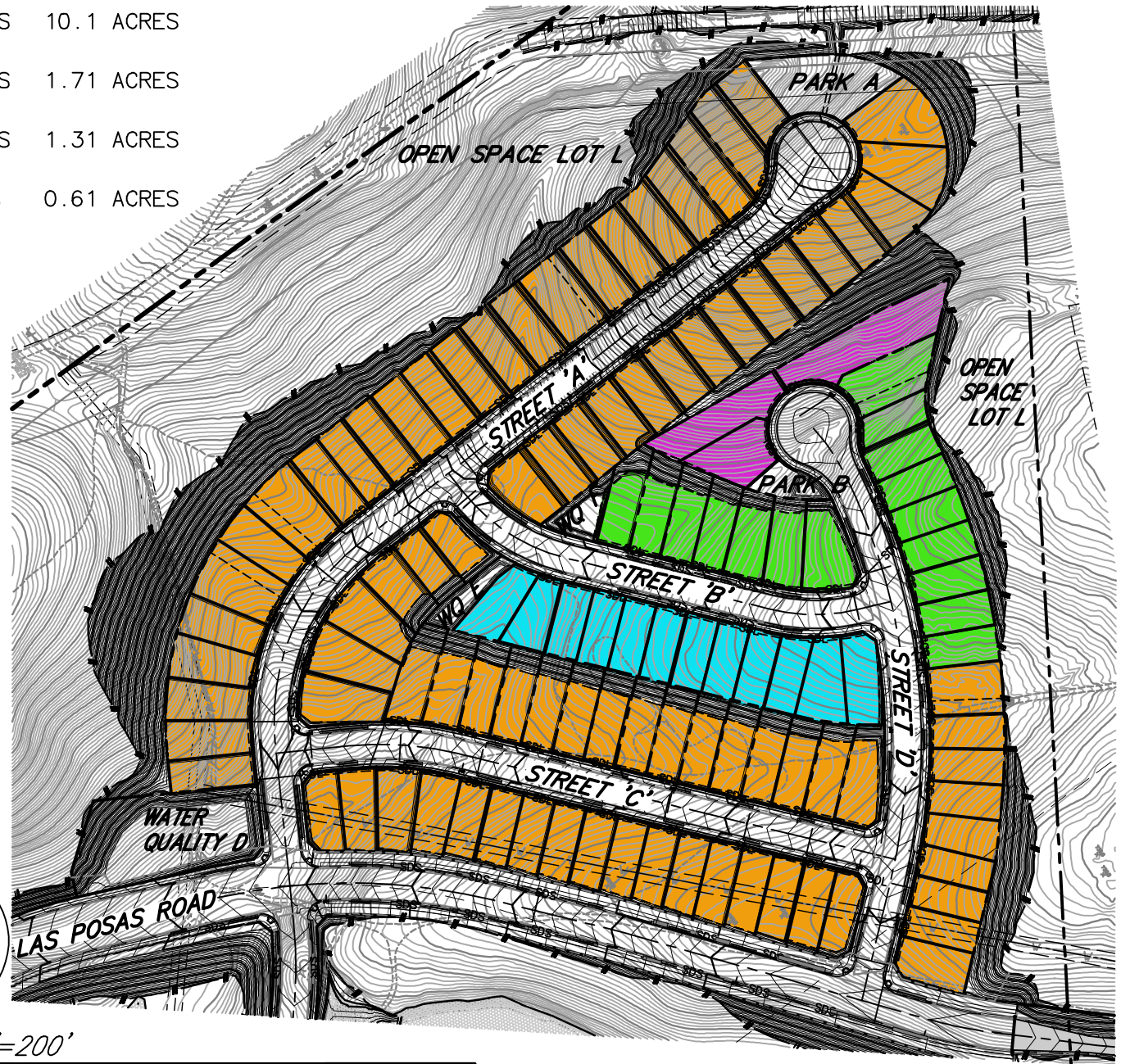
**SAN MARCOS HIGHLANDS
TYPICAL IMPERVIOUS SURFACE
LOT EXHIBIT**

SCALE 1"=20'

LEGEND

	WATER QUALITY D	86 LOTS	10.1 ACRES
	WATER QUALITY F	16 LOTS	1.71 ACRES
	WATER QUALITY E	12 LOTS	1.31 ACRES
	PARK B	3 LOTS	0.61 ACRES

WATER QUALITY BASINS EXHIBIT



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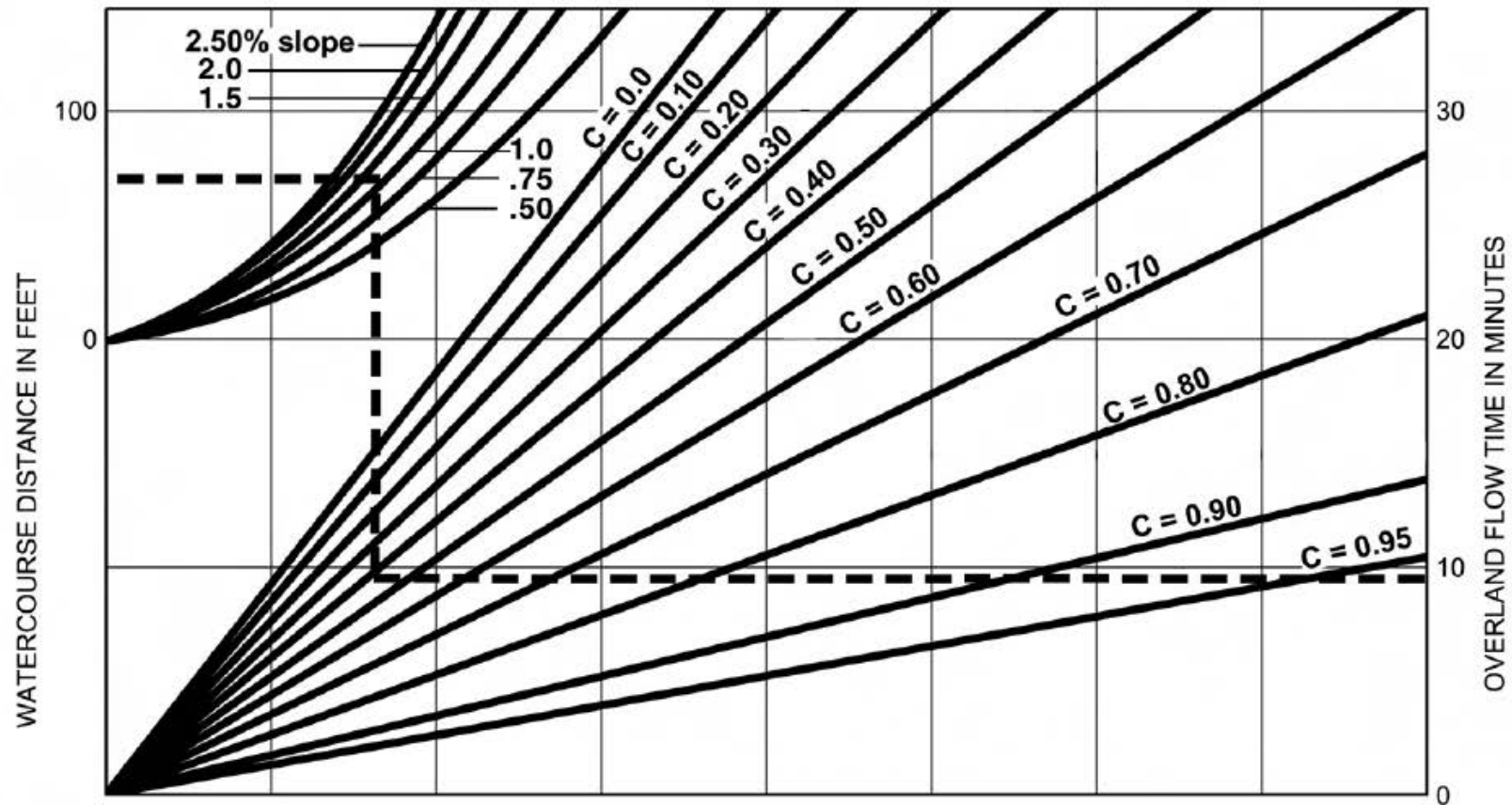


SCALE: 1"=200'



APPENDIX 2

CHARTS AND FIGURES FROM THE SAN DIEGO COUNTY HYDROLOGY MANUAL



EXAMPLE:

Given: Watercourse Distance (D) = 70 Feet
 Slope (s) = 1.3%
 Runoff Coefficient (C) = 0.41
 Overland Flow Time (T) = 9.5 Minutes

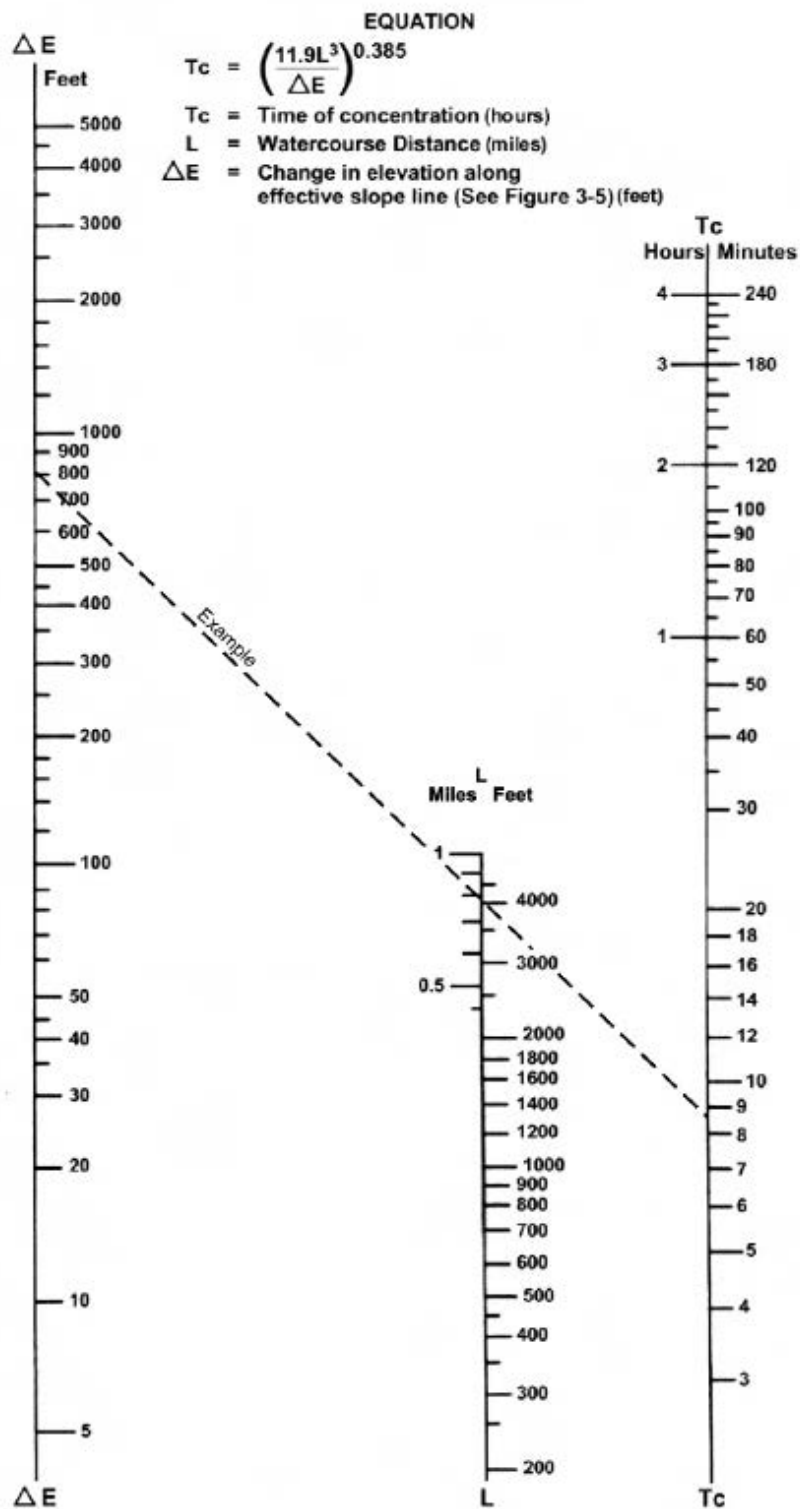
$$T = \frac{1.8 (1.1-C) \sqrt{D}}{\sqrt[3]{s}}$$

SOURCE: Airport Drainage, Federal Aviation Administration, 1965

Rational Formula - Overland Time of Flow Nomograph

F I G U R E

3-3

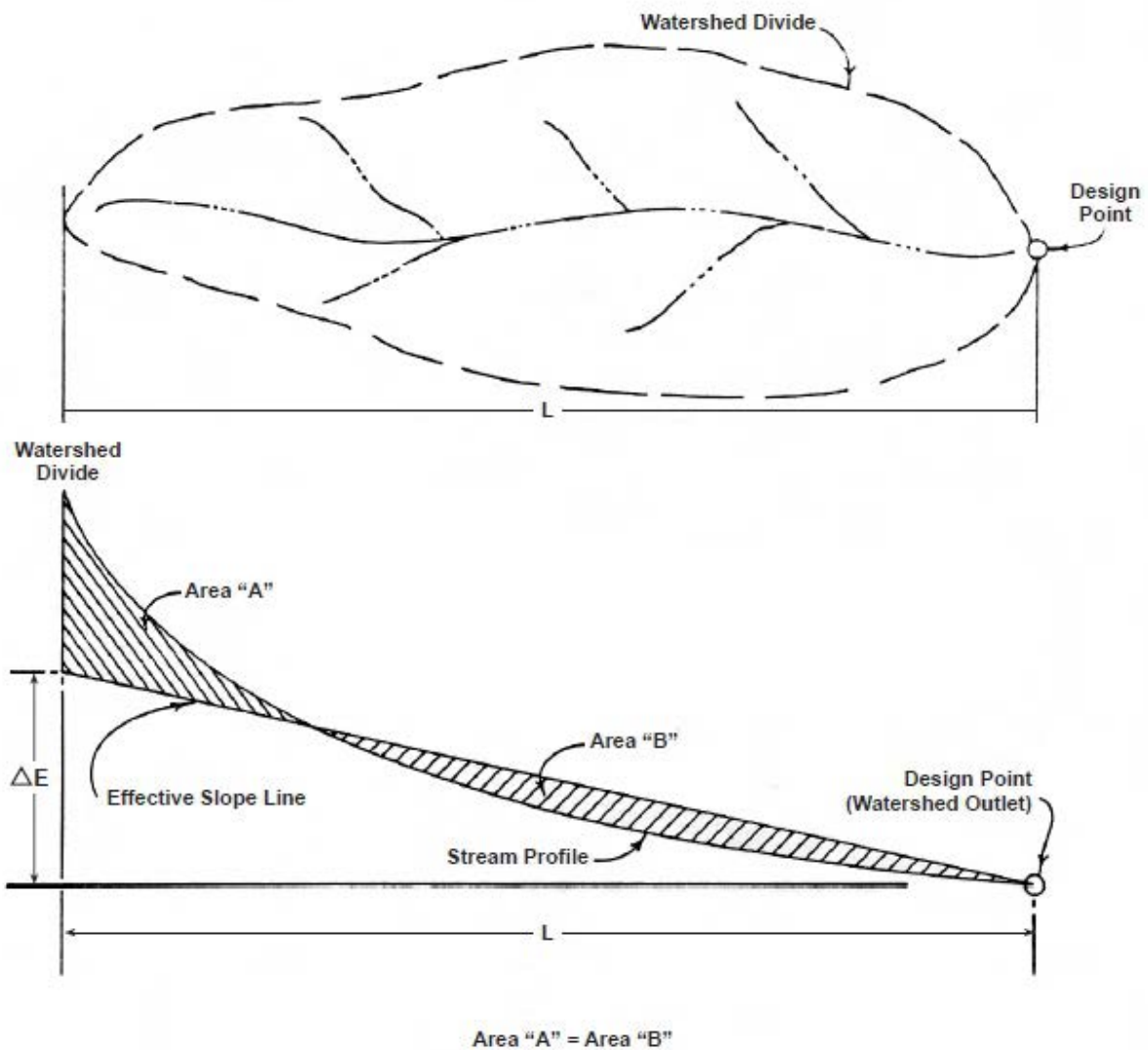


SOURCE: California Division of Highways (1941) and Kirpich (1940)

Nomograph for Determination of
Time of Concentration (T_c) or Travel Time (T_t) for Natural Watersheds

FIGURE

3-4

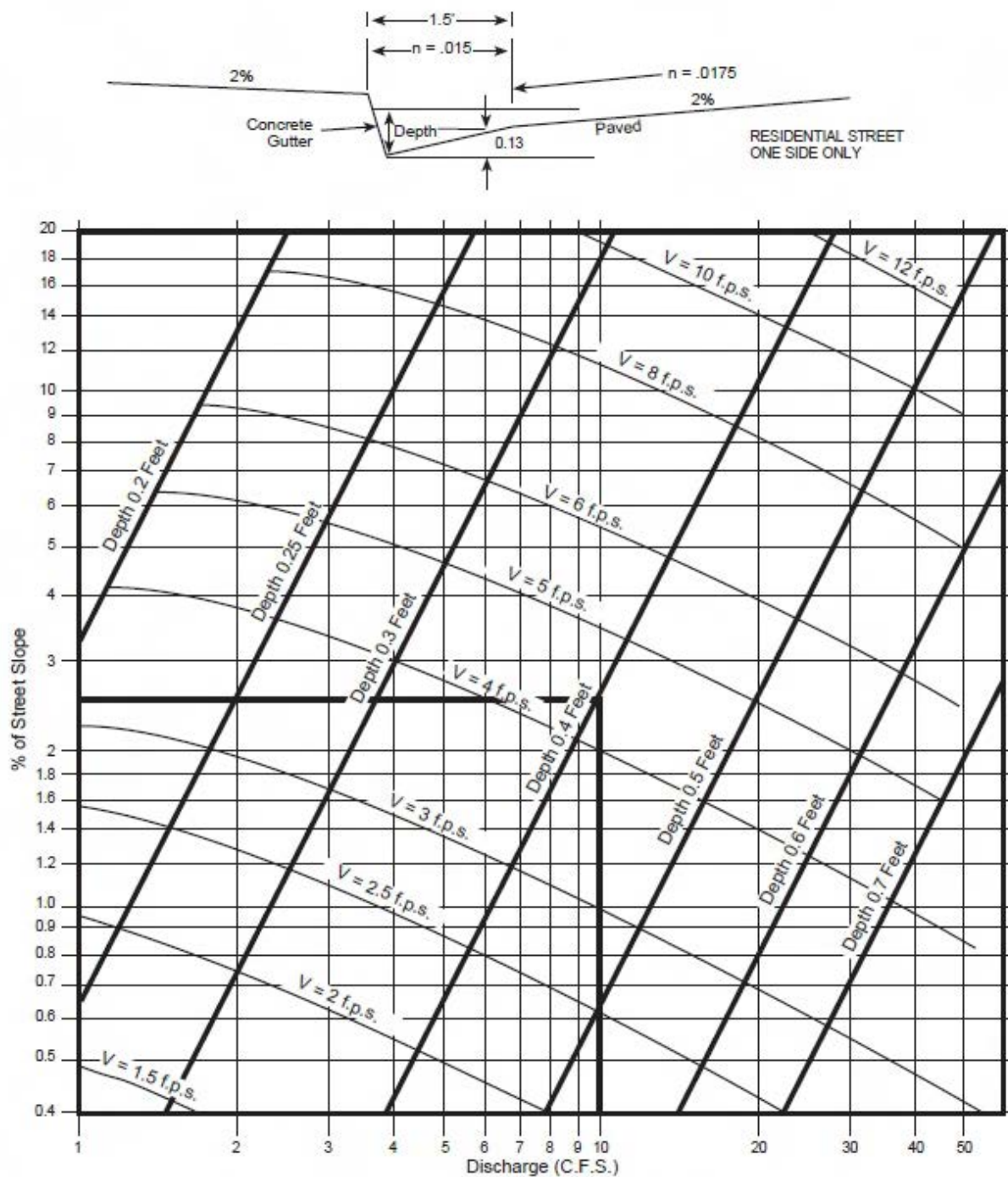


SOURCE: California Division of Highways (1941) and Kirpich (1940)

FIGURE

3-5

Computation of Effective Slope for Natural Watersheds



EXAMPLE:
Given: $Q = 10$ $S = 2.5\%$
Chart gives: Depth = 0.4, Velocity = 4.4 f.p.s.

SOURCE: San Diego County Department of Special District Services Design Manual

Gutter and Roadway Discharge - Velocity Chart

FIGURE

3-6

**Table 3-1
RUNOFF COEFFICIENTS FOR URBAN AREAS**

Land Use		Runoff Coefficient "C"				
NRCS Elements	County Elements	% IMPER.	Soil Type			
			A	B	C	D
Undisturbed Natural Terrain (Natural)	Permanent Open Space	0*	0.20	0.25	0.30	0.35
Low Density Residential (LDR)	Residential, 1.0 DU/A or less	10	0.27	0.32	0.36	0.41
Low Density Residential (LDR)	Residential, 2.0 DU/A or less	20	0.34	0.38	0.42	0.46
Low Density Residential (LDR)	Residential, 2.9 DU/A or less	25	0.38	0.41	0.45	0.49
Medium Density Residential (MDR)	Residential, 4.3 DU/A or less	30	0.41	0.45	0.48	0.52
Medium Density Residential (MDR)	Residential, 7.3 DU/A or less	40	0.48	0.51	0.54	0.57
Medium Density Residential (MDR)	Residential, 10.9 DU/A or less	45	0.52	0.54	0.57	0.60
Medium Density Residential (MDR)	Residential, 14.5 DU/A or less	50	0.55	0.58	0.60	0.63
High Density Residential (HDR)	Residential, 24.0 DU/A or less	65	0.66	0.67	0.69	0.71
High Density Residential (HDR)	Residential, 43.0 DU/A or less	80	0.76	0.77	0.78	0.79
Commercial/Industrial (N. Com)	Neighborhood Commercial	80	0.76	0.77	0.78	0.79
Commercial/Industrial (G. Com)	General Commercial	85	0.80	0.80	0.81	0.82
Commercial/Industrial (O.P. Com)	Office Professional/Commercial	90	0.83	0.84	0.84	0.85
Commercial/Industrial (Limited I.)	Limited Industrial	90	0.83	0.84	0.84	0.85
Commercial/Industrial (General I.)	General Industrial	95	0.87	0.87	0.87	0.87

*The values associated with 0% impervious may be used for direct calculation of the runoff coefficient as described in Section 3.1.2 (representing the pervious runoff coefficient, C_p , for the soil type), or for areas that will remain undisturbed in perpetuity. Justification must be given that the area will remain natural forever (e.g., the area is located in Cleveland National Forest).

DU/A = dwelling units per acre

NRCS = National Resources Conservation Service

Note that the Initial Time of Concentration should be reflective of the general land-use at the upstream end of a drainage basin. A single lot with an area of two or less acres does not have a significant effect where the drainage basin area is 20 to 600 acres.

Table 3-2 provides limits of the length (Maximum Length (L_M)) of sheet flow to be used in hydrology studies. Initial T_i values based on average C values for the Land Use Element are also included. These values can be used in planning and design applications as described below. Exceptions may be approved by the "Regulating Agency" when submitted with a detailed study.

Table 3-2

**MAXIMUM OVERLAND FLOW LENGTH (L_M)
& INITIAL TIME OF CONCENTRATION (T_i)**

Element*	DU/ Acre	.5%		1%		2%		3%		5%		10%	
		L_M	T_i	L_M	T_i	L_M	T_i	L_M	T_i	L_M	T_i	L_M	T_i
Natural		50	13.2	70	12.5	85	10.9	100	10.3	100	8.7	100	6.9
LDR	1	50	12.2	70	11.5	85	10.0	100	9.5	100	8.0	100	6.4
LDR	2	50	11.3	70	10.5	85	9.2	100	8.8	100	7.4	100	5.8
LDR	2.9	50	10.7	70	10.0	85	8.8	95	8.1	100	7.0	100	5.6
MDR	4.3	50	10.2	70	9.6	80	8.1	95	7.8	100	6.7	100	5.3
MDR	7.3	50	9.2	65	8.4	80	7.4	95	7.0	100	6.0	100	4.8
MDR	10.9	50	8.7	65	7.9	80	6.9	90	6.4	100	5.7	100	4.5
MDR	14.5	50	8.2	65	7.4	80	6.5	90	6.0	100	5.4	100	4.3
HDR	24	50	6.7	65	6.1	75	5.1	90	4.9	95	4.3	100	3.5
HDR	43	50	5.3	65	4.7	75	4.0	85	3.8	95	3.4	100	2.7
N. Com		50	5.3	60	4.5	75	4.0	85	3.8	95	3.4	100	2.7
G. Com		50	4.7	60	4.1	75	3.6	85	3.4	90	2.9	100	2.4
O.P./Com		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
Limited I		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
General I		50	3.7	60	3.2	70	2.7	80	2.6	90	2.3	100	1.9

*See Table 3-1 for more detailed description

APPENDIX 3

PRE-DEVELOPMENT HYDROLOGY CALCULATION

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 12/04/12

FINAL OUTFALL 10 - Las Posas Road: Node 1 TO 6
PRE DEVELOPMENT
100 Year Storm Event
File Name: 12052PRE.RD3

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL]
(1.0 DU/A or Less)
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Initial subarea total flow distance = 1012.000(Ft.)
Highest elevation = 1140.000(Ft.)
Lowest elevation = 900.000(Ft.)
Elevation difference = 240.000(Ft.) Slope = 23.715 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 23.72 %, in a development type of
1.0 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.32 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.4100) * (100.000^{.5})] / (23.715^{(1/3)}) = 4.32$
The initial area total distance of 1012.00 (Ft.) entered leaves a
remaining distance of 912.00 (Ft.)
Using Figure 3-4, the travel time for this distance is 2.58 minutes
for a distance of 912.00 (Ft.) and a slope of 23.72 %
with an elevation difference of 216.28(Ft.) from the end of the top area
 $Tt = [11.9 * length(Mi)^3] / (elevation change(Ft.))^{.385} * 60(min/hr)$
= 2.585 Minutes
 $Tt = [(11.9 * 0.1727^3) / (216.28)]^{.385} = 2.58$
Total initial area Ti = 4.32 minutes from Figure 3-3 formula plus
2.58 minutes from the Figure 3-4 formula = 6.91 minutes
Rainfall intensity (I) = 7.486(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.410
Subarea runoff = 45.998(CFS)
Total initial stream area = 14.986(Ac.)

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Process from Point/Station      2.000 to Point/Station      3.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

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-----
Estimated mean flow rate at midpoint of channel =    148.425(CFS)
Depth of flow =    1.083(Ft.), Average velocity =    12.664(Ft/s)
***** Irregular Channel Data *****

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-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              10.00
      2             100.00              0.00
      3             200.00              10.00
Manning's 'N' friction factor =    0.020

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```

-----
Sub-Channel flow =    148.425(CFS)
'      '      flow top width =    21.652(Ft.)
'      '      velocity=    12.664(Ft/s)
'      '      area =    11.720(Sq.Ft)
'      '      Froude number =    3.033

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Upstream point elevation =    900.000(Ft.)
Downstream point elevation =    721.000(Ft.)
Flow length =    2700.000(Ft.)
Travel time =    3.55 min.
Time of concentration =    10.46 min.
Depth of flow =    1.083(Ft.)
Average velocity =    12.664(Ft/s)
Total irregular channel flow =    148.425(CFS)
Irregular channel normal depth above invert elev. =    1.083(Ft.)
Average velocity of channel(s) =    12.664(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL      ]
(1.0 DU/A or Less      )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Rainfall intensity =    5.728(In/Hr) for a    100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.410  CA =    43.782
Subarea runoff =    204.795(CFS) for    91.800(Ac.)
Total runoff =    250.793(CFS)      Total area =    106.786(Ac.)
Depth of flow =    1.318(Ft.), Average velocity =    14.439(Ft/s)

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Process from Point/Station      3.000 to Point/Station      4.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

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-----
Estimated mean flow rate at midpoint of channel =    306.499(CFS)
Depth of flow =    1.720(Ft.), Average velocity =    10.365(Ft/s)
***** Irregular Channel Data *****

```

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              5.00
      2             100.00              0.00
      3             100.00              5.00
Manning's 'N' friction factor =    0.023

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-----
Sub-Channel flow =    306.500(CFS)
'      '      flow top width =    34.392(Ft.)
'      '      velocity=    10.365(Ft/s)
'      '      area =    29.570(Sq.Ft)
'      '      Froude number =    1.970

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Upstream point elevation = 721.000(Ft.)
 Downstream point elevation = 668.000(Ft.)
 Flow length = 1575.000(Ft.)
 Travel time = 2.53 min.
 Time of concentration = 12.99 min.
 Depth of flow = 1.720(Ft.)
 Average velocity = 10.365(Ft/s)
 Total irregular channel flow = 306.499(CFS)
 Irregular channel normal depth above invert elev. = 1.720(Ft.)
 Average velocity of channel(s) = 10.365(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [LOW DENSITY RESIDENTIAL]
 (1.0 DU/A or Less)
 Impervious value, Ai = 0.100
 Sub-Area C Value = 0.410
 Rainfall intensity = 4.981(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.410 CA = 72.709
 Subarea runoff = 111.349(CFS) for 70.554(Ac.)
 Total runoff = 362.143(CFS) Total area = 177.340(Ac.)
 Depth of flow = 1.831(Ft.), Average velocity = 10.807(Ft/s)

 Process from Point/Station 4.000 to Point/Station 4.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 177.340(Ac.)
 Runoff from this stream = 362.143(CFS)
 Time of concentration = 12.99 min.
 Rainfall intensity = 4.981(In/Hr)

 Process from Point/Station 9.000 to Point/Station 10.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [LOW DENSITY RESIDENTIAL]
 (1.0 DU/A or Less)
 Impervious value, Ai = 0.100
 Sub-Area C Value = 0.410
 Initial subarea total flow distance = 1909.000(Ft.)
 Highest elevation = 1302.000(Ft.)
 Lowest elevation = 820.000(Ft.)
 Elevation difference = 482.000(Ft.) Slope = 25.249 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 25.25 %, in a development type of
 1.0 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 4.23 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5} / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.4100) * (100.000^{.5}) / (25.249^{(1/3)})] = 4.23$
 The initial area total distance of 1909.00 (Ft.) entered leaves a
 remaining distance of 1809.00 (Ft.)
 Using Figure 3-4, the travel time for this distance is 4.28 minutes
 for a distance of 1809.00 (Ft.) and a slope of 25.25 %
 with an elevation difference of 456.75(Ft.) from the end of the top area
 $Tt = [11.9 * length(Mi)^3 / (elevation change(Ft.))]^{.385} * 60(min/hr)$
 $= 4.275 Minutes$
 $Tt = [(11.9 * 0.3426^3) / (456.75)]^{.385} = 4.28$
 Total initial area Ti = 4.23 minutes from Figure 3-3 formula plus

4.28 minutes from the Figure 3-4 formula = 8.51 minutes
 Rainfall intensity (I) = 6.544(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.410
 Subarea runoff = 60.081(CFS)
 Total initial stream area = 22.391(Ac.)

 Process from Point/Station 10.000 to Point/Station 4.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 197.122(CFS)
 Depth of flow = 0.923(Ft.), Average velocity = 11.577(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 100.00 0.00
 3 200.00 5.00
 Manning's 'N' friction factor = 0.020

 Sub-Channel flow = 197.122(CFS)
 ' ' flow top width = 36.907(Ft.)
 ' ' velocity = 11.577(Ft/s)
 ' ' area = 17.027(Sq.Ft)
 ' ' Froude number = 3.004

Upstream point elevation = 820.000(Ft.)
 Downstream point elevation = 668.000(Ft.)
 Flow length = 2228.000(Ft.)
 Travel time = 3.21 min.
 Time of concentration = 11.72 min.
 Depth of flow = 0.923(Ft.)
 Average velocity = 11.577(Ft/s)
 Total irregular channel flow = 197.122(CFS)
 Irregular channel normal depth above invert elev. = 0.923(Ft.)
 Average velocity of channel(s) = 11.577(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [LOW DENSITY RESIDENTIAL]
 (1.0 DU/A or Less)
 Impervious value, Ai = 0.100
 Sub-Area C Value = 0.410
 Rainfall intensity = 5.324(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.410 CA = 62.750
 Subarea runoff = 274.030(CFS) for 130.659(Ac.)
 Total runoff = 334.110(CFS) Total area = 153.050(Ac.)
 Depth of flow = 1.125(Ft.), Average velocity = 13.210(Ft/s)

 Process from Point/Station 4.000 to Point/Station 4.000
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 153.050(Ac.)
 Runoff from this stream = 334.110(CFS)
 Time of concentration = 11.72 min.
 Rainfall intensity = 5.324(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	362.143	12.99	4.981


```

2      334.110      11.72      5.324
Qmax(1) =
      1.000 *      1.000 *      362.143) +
      0.935 *      1.000 *      334.110) + =      674.683
Qmax(2) =
      1.000 *      0.902 *      362.143) +
      1.000 *      1.000 *      334.110) + =      660.656

Total of 2 streams to confluence:
Flow rates before confluence point:
      362.143      334.110
Maximum flow rates at confluence using above data:
      674.683      660.656
Area of streams before confluence:
      177.340      153.050
Results of confluence:
Total flow rate =      674.683(CFS)
Time of concentration =      12.993 min.
Effective stream area after confluence =      330.390(Ac.)

*****
Process from Point/Station      4.000 to Point/Station      5.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

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Estimated mean flow rate at midpoint of channel =      674.727(CFS)
Depth of flow =      0.567(Ft.), Average velocity =      8.040(Ft/s)
      ***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              24.00
      2              89.00              0.00
      3             235.00              0.00
      4             343.00             30.00
Manning's 'N' friction factor =      0.020
-----
Sub-Channel flow =      674.728(CFS)
'      '      flow top width =      150.142(Ft.)
'      '      velocity=      8.040(Ft/s)
'      '      area =      83.923(Sq.Ft)
'      '      Froude number =      1.895

Upstream point elevation =      668.000(Ft.)
Downstream point elevation =      631.000(Ft.)
Flow length =      1453.000(Ft.)
Travel time =      3.01 min.
Time of concentration =      16.01 min.
Depth of flow =      0.567(Ft.)
Average velocity =      8.040(Ft/s)
Total irregular channel flow =      674.727(CFS)
Irregular channel normal depth above invert elev. =      0.567(Ft.)
Average velocity of channel(s) =      8.040(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN      ]
(Permanent Open Space      )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
The area added to the existing stream causes a
a lower flow rate of Q =      623.034(CFS)
therefore the upstream flow rate of Q =      674.683(CFS) is being used
Rainfall intensity =      4.354(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.406 CA =      143.095
Subarea runoff =      0.000(CFS) for      21.815(Ac.)
Total runoff =      674.683(CFS)      Total area =      352.205(Ac.)
Depth of flow =      0.567(Ft.), Average velocity =      8.040(Ft/s)

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*****
Process from Point/Station      5.000 to Point/Station      5.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area =      352.205(Ac.)
Runoff from this stream =      674.683(CFS)
Time of concentration =      16.01 min.
Rainfall intensity =      4.354(In/Hr)

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*****
Process from Point/Station      7.000 to Point/Station      8.000
**** INITIAL AREA EVALUATION ****

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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL                      ]
(1.0 DU/A or Less                            )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Initial subarea total flow distance = 756.000(Ft.)
Highest elevation = 905.000(Ft.)
Lowest elevation = 780.000(Ft.)
Elevation difference = 125.000(Ft.) Slope = 16.534 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 16.53 %, in a development type of
1.0 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.88 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.4100)*( 100.000^0.5)]/( 16.534^(1/3))= 4.88
The initial area total distance of 756.00 (Ft.) entered leaves a
remaining distance of 656.00 (Ft.)
Using Figure 3-4, the travel time for this distance is 2.30 minutes
for a distance of 656.00 (Ft.) and a slope of 16.53 %
with an elevation difference of 108.46(Ft.) from the end of the top area
Tt = [11.9*length(Mi)^3]/(elevation change(Ft.))^0.385 *60(min/hr)
= 2.304 Minutes
Tt=[(11.9*0.1242^3)/(108.46)]^0.385= 2.30
Total initial area Ti = 4.88 minutes from Figure 3-3 formula plus
2.30 minutes from the Figure 3-4 formula = 7.18 minutes
Rainfall intensity (I) = 7.302(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.410
Subarea runoff = 67.627(CFS)
Total initial stream area = 22.588(Ac.)

```

```

*****
Process from Point/Station      8.000 to Point/Station      5.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

Estimated mean flow rate at midpoint of channel = 167.694(CFS)
Depth of flow = 2.182(Ft.), Average velocity = 17.616(Ft/s)
***** Irregular Channel Data *****

```

```

Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
1                  0.00                10.00
2                 20.00                 0.00
3                 40.00                10.00
Manning's 'N' friction factor = 0.020

```

```

Sub-Channel flow = 167.694(CFS)
'      '      flow top width = 8.727(Ft.)
'      '      velocity= 17.616(Ft/s)

```

```

      '      '      area =      9.519(Sq.Ft)
      '      '      Froude number =      2.972

Upstream point elevation = 780.000(Ft.)
Downstream point elevation = 631.000(Ft.)
Flow length = 2565.000(Ft.)
Travel time = 2.43 min.
Time of concentration = 9.61 min.
Depth of flow = 2.182(Ft.)
Average velocity = 17.616(Ft/s)
Total irregular channel flow = 167.694(CFS)
Irregular channel normal depth above invert elev. = 2.182(Ft.)
Average velocity of channel(s) = 17.616(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL ]
(1.0 DU/A or Less )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Rainfall intensity = 6.052(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.410 CA = 44.232
Subarea runoff = 200.061(CFS) for 85.295(Ac.)
Total runoff = 267.688(CFS) Total area = 107.883(Ac.)
Depth of flow = 2.600(Ft.), Average velocity = 19.801(Ft/s)

+++++
Process from Point/Station 5.000 to Point/Station 5.000
**** CONFLUENCE OF MINOR STREAMS ****

-----
Along Main Stream number: 1 in normal stream number 2
Stream flow area = 107.883(Ac.)
Runoff from this stream = 267.688(CFS)
Time of concentration = 9.61 min.
Rainfall intensity = 6.052(In/Hr)

+++++
Process from Point/Station 11.000 to Point/Station 5.000
**** INITIAL AREA EVALUATION ****

-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 2318.000(Ft.)
Highest elevation = 1025.000(Ft.)
Lowest elevation = 631.000(Ft.)
Elevation difference = 394.000(Ft.) Slope = 16.997 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 17.00 %, in a development type of
Permanent Open Space
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.25 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.3500)*( 100.000^0.5)/( 16.997^(1/3))]= 5.25
The initial area total distance of 2318.00 (Ft.) entered leaves a
remaining distance of 2218.00 (Ft.)
Using Figure 3-4, the travel time for this distance is 5.82 minutes
for a distance of 2218.00 (Ft.) and a slope of 17.00 %
with an elevation difference of 376.99(Ft.) from the end of the top area
Tt = [11.9*length(Mi)^3]/(elevation change(Ft.))]^0.385 *60(min/hr)

```

```

= 5.825 Minutes
Tt=[(11.9*0.4201^3)/(376.99)]^.385= 5.82
Total initial area Ti = 5.25 minutes from Figure 3-3 formula plus
5.82 minutes from the Figure 3-4 formula = 11.08 minutes
Rainfall intensity (I) = 5.521(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 43.714(CFS)
Total initial stream area = 22.622(Ac.)

*****
Process from Point/Station 5.000 to Point/Station 5.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 22.622(Ac.)
Runoff from this stream = 43.714(CFS)
Time of concentration = 11.08 min.
Rainfall intensity = 5.521(In/Hr)
Summary of stream data:

Stream No. Flow rate (CFS) TC (min) Rainfall Intensity (In/Hr)

1 674.683 16.01 4.354
2 267.688 9.61 6.052
3 43.714 11.08 5.521
Qmax(1) =
1.000 * 1.000 * 674.683) +
0.719 * 1.000 * 267.688) +
0.789 * 1.000 * 43.714) + = 901.743
Qmax(2) =
1.000 * 0.600 * 674.683) +
1.000 * 1.000 * 267.688) +
1.000 * 0.867 * 43.714) + = 710.539
Qmax(3) =
1.000 * 0.692 * 674.683) +
0.912 * 1.000 * 267.688) +
1.000 * 1.000 * 43.714) + = 754.794

Total of 3 streams to confluence:
Flow rates before confluence point:
674.683 267.688 43.714
Maximum flow rates at confluence using above data:
901.743 710.539 754.794
Area of streams before confluence:
352.205 107.883 22.622
Results of confluence:
Total flow rate = 901.743(CFS)
Time of concentration = 16.006 min.
Effective stream area after confluence = 482.710(Ac.)

*****
Process from Point/Station 5.000 to Point/Station 6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 912.970(CFS)
Depth of flow = 2.797(Ft.), Average velocity = 11.670(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 10.00
2 100.00 0.00
3 200.00 10.00
Manning's 'N' friction factor = 0.025
-----
Sub-Channel flow = 912.971(CFS)
' ' flow top width = 55.940(Ft.)

```

```

'      '      velocity= 11.670(Ft/s)
'      '      area = 78.232(Sq.Ft)
'      '      Froude number = 1.739

Upstream point elevation = 631.000(Ft.)
Downstream point elevation = 575.000(Ft.)
Flow length = 2257.000(Ft.)
Travel time = 3.22 min.
Time of concentration = 19.23 min.
Depth of flow = 2.797(Ft.)
Average velocity = 11.670(Ft/s)
Total irregular channel flow = 912.970(CFS)
Irregular channel normal depth above invert elev. = 2.797(Ft.)
Average velocity of channel(s) = 11.670(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL ]
(2.0 DU/A or Less )
Impervious value, Ai = 0.200
Sub-Area C Value = 0.460
Rainfall intensity = 3.868(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.414 CA = 238.909
Subarea runoff = 22.369(CFS) for 94.923(Ac.)
Total runoff = 924.112(CFS) Total area = 577.633(Ac.)
Depth of flow = 2.810(Ft.), Average velocity = 11.706(Ft/s)
End of computations, total study area = 577.633 (Ac.)

```

APPENDIX 4

POST-DEVELOPMENT HYDROLOGY CALCULATION


```

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13
-----
OUTFALL 1 - Las Posas Road: Node 500-511
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052OUTFALL1
-----
***** Hydrology Study Control Information *****
-----

Program License Serial Number 4012

-----
Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

+-----+
Process from Point/Station 500.000 to Point/Station 501.000
**** INITIAL AREA EVALUATION ****
+-----+
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 156.000(Ft.)
Highest elevation = 694.400(Ft.)
Lowest elevation = 693.000(Ft.)
Elevation difference = 1.400(Ft.) Slope = 0.897 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 0.90 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.52 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 65.000^0.5)/( 0.897^(1/3))]= 7.52
Rainfall intensity (I) = 7.085(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.650(CFS)
Total initial stream area = 0.153(Ac.)

+-----+
Process from Point/Station 501.000 to Point/Station 502.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
+-----+
Upstream point/station elevation = 688.500(Ft.)
Downstream point/station elevation = 687.000(Ft.)
Pipe length = 166.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.650(CFS)
Nearest computed pipe diameter = 9.00(In.)

```

Calculated individual pipe flow = 0.650(CFS)
 Normal flow depth in pipe = 4.03(In.)
 Flow top width inside pipe = 8.95(In.)
 Critical Depth = 4.39(In.)
 Pipe flow velocity = 3.39(Ft/s)
 Travel time through pipe = 0.82 min.
 Time of concentration (TC) = 8.34 min.

 Process from Point/Station 502.000 to Point/Station 502.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.34 min.
 Rainfall intensity = 6.630(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.223
 Subarea runoff = 0.829(CFS) for 0.219(Ac.)
 Total runoff = 1.480(CFS) Total area = 0.372(Ac.)

 Process from Point/Station 502.000 to Point/Station 503.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
 Downstream point/station elevation = 685.000(Ft.)
 Pipe length = 87.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.480(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.480(CFS)
 Normal flow depth in pipe = 4.97(In.)
 Flow top width inside pipe = 8.95(In.)
 Critical Depth = 6.72(In.)
 Pipe flow velocity = 5.91(Ft/s)
 Travel time through pipe = 0.25 min.
 Time of concentration (TC) = 8.59 min.

 Process from Point/Station 503.000 to Point/Station 503.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.59 min.
 Rainfall intensity = 6.507(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.281
 Subarea runoff = 0.351(CFS) for 0.097(Ac.)
 Total runoff = 1.831(CFS) Total area = 0.469(Ac.)

 Process from Point/Station 503.000 to Point/Station 504.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 685.000(Ft.)
Downstream point/station elevation = 682.100(Ft.)
Pipe length = 69.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.831(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.831(CFS)
Normal flow depth in pipe = 4.71(In.)
Flow top width inside pipe = 8.99(In.)
Critical Depth = 7.43(In.)
Pipe flow velocity = 7.82(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 8.73 min.

*****
Process from Point/Station 504.000 to Point/Station 510.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 682.100(Ft.)
Downstream point/station elevation = 681.300(Ft.)
Pipe length = 44.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.831(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.831(CFS)
Normal flow depth in pipe = 6.21(In.)
Flow top width inside pipe = 8.32(In.)
Critical Depth = 7.43(In.)
Pipe flow velocity = 5.64(Ft/s)
Travel time through pipe = 0.13 min.
Time of concentration (TC) = 8.86 min.

*****
Process from Point/Station 510.000 to Point/Station 510.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.469(Ac.)
Runoff from this stream = 1.831(CFS)
Time of concentration = 8.86 min.
Rainfall intensity = 6.375(In/Hr)

*****
Process from Point/Station 505.000 to Point/Station 506.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 156.000(Ft.)
Highest elevation = 694.400(Ft.)
Lowest elevation = 693.100(Ft.)
Elevation difference = 1.300(Ft.) Slope = 0.833 %
Top of Initial Area Slope adjusted by User to 1.000 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 1.00 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.26 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3)]
TC = [1.8*(1.1-0.6000)*( 65.000^.5)/( 1.000^(1/3)]= 7.26
Rainfall intensity (I) = 7.253(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.635(CFS)

```

Total initial stream area = 0.146(Ac.)

Process from Point/Station 506.000 to Point/Station 507.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.600(Ft.)
Downstream point/station elevation = 687.900(Ft.)
Pipe length = 83.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.635(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.635(CFS)
Normal flow depth in pipe = 4.06(In.)
Flow top width inside pipe = 8.96(In.)
Critical Depth = 4.34(In.)
Pipe flow velocity = 3.29(Ft/s)
Travel time through pipe = 0.42 min.
Time of concentration (TC) = 7.68 min.

Process from Point/Station 507.000 to Point/Station 507.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.68 min.
Rainfall intensity = 6.993(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.139
Subarea runoff = 0.338(CFS) for 0.086(Ac.)
Total runoff = 0.973(CFS) Total area = 0.232(Ac.)

Process from Point/Station 507.000 to Point/Station 508.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.900(Ft.)
Downstream point/station elevation = 686.900(Ft.)
Pipe length = 85.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.973(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.973(CFS)
Normal flow depth in pipe = 4.72(In.)
Flow top width inside pipe = 8.99(In.)
Critical Depth = 5.43(In.)
Pipe flow velocity = 4.14(Ft/s)
Travel time through pipe = 0.34 min.
Time of concentration (TC) = 8.02 min.

Process from Point/Station 508.000 to Point/Station 508.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600

Time of concentration = 8.02 min.
 Rainfall intensity = 6.800(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.189
 Subarea runoff = 0.312(CFS) for 0.083(Ac.)
 Total runoff = 1.285(CFS) Total area = 0.315(Ac.)

 Process from Point/Station 508.000 to Point/Station 509.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.900(Ft.)
 Downstream point/station elevation = 684.900(Ft.)
 Pipe length = 85.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.285(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.285(CFS)
 Normal flow depth in pipe = 4.54(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical Depth = 6.26(In.)
 Pipe flow velocity = 5.76(Ft/s)
 Travel time through pipe = 0.25 min.
 Time of concentration (TC) = 8.26 min.

 Process from Point/Station 509.000 to Point/Station 509.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.26 min.
 Rainfall intensity = 6.669(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.240
 Subarea runoff = 0.315(CFS) for 0.085(Ac.)
 Total runoff = 1.600(CFS) Total area = 0.400(Ac.)

 Process from Point/Station 509.000 to Point/Station 510.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 684.900(Ft.)
 Downstream point/station elevation = 681.300(Ft.)
 Pipe length = 85.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.600(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.600(CFS)
 Normal flow depth in pipe = 4.34(In.)
 Flow top width inside pipe = 8.99(In.)
 Critical Depth = 6.98(In.)
 Pipe flow velocity = 7.59(Ft/s)
 Travel time through pipe = 0.19 min.
 Time of concentration (TC) = 8.45 min.

 Process from Point/Station 510.000 to Point/Station 510.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000

```

Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.45 min.
Rainfall intensity = 6.573(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.285
Subarea runoff = 0.273(CFS) for 0.075(Ac.)
Total runoff = 1.873(CFS) Total area = 0.475(Ac.)

+++++
Process from Point/Station 510.000 to Point/Station 510.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.475(Ac.)
Runoff from this stream = 1.873(CFS)
Time of concentration = 8.45 min.
Rainfall intensity = 6.573(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 1.831 8.86 6.375
2 1.873 8.45 6.573
Qmax(1) =
1.000 * 1.000 * 1.831) +
0.970 * 1.000 * 1.873) + = 3.648
Qmax(2) =
1.000 * 0.954 * 1.831) +
1.000 * 1.000 * 1.873) + = 3.619

Total of 2 streams to confluence:
Flow rates before confluence point:
1.831 1.873
Maximum flow rates at confluence using above data:
3.648 3.619
Area of streams before confluence:
0.469 0.475
Results of confluence:
Total flow rate = 3.648(CFS)
Time of concentration = 8.862 min.
Effective stream area after confluence = 0.944(Ac.)

+++++
Process from Point/Station 510.000 to Point/Station 511.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 681.300(Ft.)
Downstream point/station elevation = 680.500(Ft.)
Pipe length = 23.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.648(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.648(CFS)
Normal flow depth in pipe = 6.35(In.)
Flow top width inside pipe = 11.98(In.)
Critical Depth = 9.78(In.)
Pipe flow velocity = 8.66(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 8.91 min.
End of computations, total study area = 0.944 (Ac.)

```


San Diego County Rational Hydrology Program
CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13

OUTFALL 2 - Las Posas Road: Node 504-523
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052OUTFALL2

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 504.000 to Point/Station 512.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 98.000(Ft.)
Highest elevation = 682.100(Ft.)
Lowest elevation = 678.500(Ft.)
Elevation difference = 3.600(Ft.) Slope = 3.673 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.67 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.53 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.673^{(1/3)}) = 5.53$
Rainfall intensity (I) = 8.638(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.565(CFS)
Total initial stream area = 0.109(Ac.)

Process from Point/Station 512.000 to Point/Station 513.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 678.500(Ft.)
Downstream point/station elevation = 675.200(Ft.)
Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.565(CFS)
Nearest computed pipe diameter = 6.00(In.)

Calculated individual pipe flow = 0.565(CFS)
Normal flow depth in pipe = 3.09(In.)
Flow top width inside pipe = 6.00(In.)
Critical Depth = 4.59(In.)
Pipe flow velocity = 5.54(Ft/s)
Travel time through pipe = 0.27 min.
Time of concentration (TC) = 5.80 min.

Process from Point/Station 513.000 to Point/Station 513.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.80 min.
Rainfall intensity = 8.376(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.125
Subarea runoff = 0.480(CFS) for 0.099(Ac.)
Total runoff = 1.045(CFS) Total area = 0.208(Ac.)

Process from Point/Station 513.000 to Point/Station 514.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 675.200(Ft.)
Downstream point/station elevation = 672.100(Ft.)
Pipe length = 86.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.045(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.045(CFS)
Normal flow depth in pipe = 4.82(In.)
Flow top width inside pipe = 4.78(In.)
Critical depth could not be calculated.
Pipe flow velocity = 6.18(Ft/s)
Travel time through pipe = 0.23 min.
Time of concentration (TC) = 6.04 min.

Process from Point/Station 514.000 to Point/Station 514.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.04 min.
Rainfall intensity = 8.167(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.184
Subarea runoff = 0.459(CFS) for 0.099(Ac.)
Total runoff = 1.504(CFS) Total area = 0.307(Ac.)

Process from Point/Station 514.000 to Point/Station 515.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 672.100(Ft.)
 Downstream point/station elevation = 668.800(Ft.)
 Pipe length = 92.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.504(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.504(CFS)
 Normal flow depth in pipe = 4.39(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical Depth = 6.78(In.)
 Pipe flow velocity = 7.02(Ft/s)
 Travel time through pipe = 0.22 min.
 Time of concentration (TC) = 6.25 min.

 Process from Point/Station 515.000 to Point/Station 515.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.25 min.
 Rainfall intensity = 7.982(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.243
 Subarea runoff = 0.435(CFS) for 0.098(Ac.)
 Total runoff = 1.940(CFS) Total area = 0.405(Ac.)

 Process from Point/Station 515.000 to Point/Station 516.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 668.800(Ft.)
 Downstream point/station elevation = 667.000(Ft.)
 Pipe length = 55.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.940(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.940(CFS)
 Normal flow depth in pipe = 5.27(In.)
 Flow top width inside pipe = 8.87(In.)
 Critical Depth = 7.61(In.)
 Pipe flow velocity = 7.21(Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 6.38 min.

 Process from Point/Station 516.000 to Point/Station 516.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.38 min.
 Rainfall intensity = 7.879(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.279
 Subarea runoff = 0.259(CFS) for 0.060(Ac.)
 Total runoff = 2.198(CFS) Total area = 0.465(Ac.)

```

*****
Process from Point/Station      516.000 to Point/Station      521.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 667.000(Ft.)
Downstream point/station elevation = 666.000(Ft.)
Pipe length = 45.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.198(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.198(CFS)
Normal flow depth in pipe = 6.62(In.)
Flow top width inside pipe = 7.94(In.)
Critical Depth = 7.98(In.)
Pipe flow velocity = 6.31(Ft/s)
Travel time through pipe = 0.12 min.
Time of concentration (TC) = 6.50 min.

```

```

*****
Process from Point/Station      521.000 to Point/Station      521.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.465(Ac.)
Runoff from this stream = 2.198(CFS)
Time of concentration = 6.50 min.
Rainfall intensity = 7.785(In/Hr)

```

```

*****
Process from Point/Station      510.000 to Point/Station      517.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 96.000(Ft.)
Highest elevation = 686.800(Ft.)
Lowest elevation = 683.000(Ft.)
Elevation difference = 3.800(Ft.) Slope = 3.958 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.96 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.40 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 90.000^0.5)]/( 3.958^(1/3))= 5.40
Rainfall intensity (I) = 8.777(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.495(CFS)
Total initial stream area = 0.094(Ac.)

```

```

*****
Process from Point/Station      517.000 to Point/Station      518.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 678.500(Ft.)
Downstream point/station elevation = 675.200(Ft.)
Pipe length = 87.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.495(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.495(CFS)
Normal flow depth in pipe = 2.83(In.)

```

Flow top width inside pipe = 5.99(In.)
Critical Depth = 4.31(In.)
Pipe flow velocity = 5.43(Ft/s)
Travel time through pipe = 0.27 min.
Time of concentration (TC) = 5.66 min.

Process from Point/Station 518.000 to Point/Station 518.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.66 min.
Rainfall intensity = 8.508(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.108
Subarea runoff = 0.424(CFS) for 0.086(Ac.)
Total runoff = 0.919(CFS) Total area = 0.180(Ac.)

Process from Point/Station 518.000 to Point/Station 519.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 675.200(Ft.)
Downstream point/station elevation = 672.000(Ft.)
Pipe length = 83.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.919(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.919(CFS)
Normal flow depth in pipe = 4.19(In.)
Flow top width inside pipe = 5.51(In.)
Critical Depth = 5.56(In.)
Pipe flow velocity = 6.28(Ft/s)
Travel time through pipe = 0.22 min.
Time of concentration (TC) = 5.88 min.

Process from Point/Station 519.000 to Point/Station 519.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.88 min.
Rainfall intensity = 8.301(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.157
Subarea runoff = 0.381(CFS) for 0.081(Ac.)
Total runoff = 1.300(CFS) Total area = 0.261(Ac.)

Process from Point/Station 519.000 to Point/Station 520.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 672.000(Ft.)
Downstream point/station elevation = 669.000(Ft.)

```

Pipe length = 84.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.300(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.300(CFS)
Normal flow depth in pipe = 4.05(In.)
Flow top width inside pipe = 8.95(In.)
Critical Depth = 6.31(In.)
Pipe flow velocity = 6.75(Ft/s)
Travel time through pipe = 0.21 min.
Time of concentration (TC) = 6.09 min.

*****
Process from Point/Station 520.000 to Point/Station 520.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.09 min.
Rainfall intensity = 8.118(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.206
Subarea runoff = 0.371(CFS) for 0.082(Ac.)
Total runoff = 1.671(CFS) Total area = 0.343(Ac.)

*****
Process from Point/Station 520.000 to Point/Station 521.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 669.000(Ft.)
Downstream point/station elevation = 666.000(Ft.)
Pipe length = 57.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.671(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.671(CFS)
Normal flow depth in pipe = 4.18(In.)
Flow top width inside pipe = 8.98(In.)
Critical Depth = 7.12(In.)
Pipe flow velocity = 8.32(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 6.21 min.

*****
Process from Point/Station 521.000 to Point/Station 521.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.21 min.
Rainfall intensity = 8.021(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.238
Subarea runoff = 0.240(CFS) for 0.054(Ac.)
Total runoff = 1.911(CFS) Total area = 0.397(Ac.)

*****

```

Process from Point/Station 521.000 to Point/Station 521.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.397(Ac.)
 Runoff from this stream = 1.911(CFS)
 Time of concentration = 6.21 min.
 Rainfall intensity = 8.021(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.198	6.50	7.785
2	1.911	6.21	8.021

Qmax(1) =
 1.000 * 1.000 * 2.198) +
 0.971 * 1.000 * 1.911) + = 4.053
 Qmax(2) =
 1.000 * 0.955 * 2.198) +
 1.000 * 1.000 * 1.911) + = 4.009

Total of 2 streams to confluence:
 Flow rates before confluence point:
 2.198 1.911

Maximum flow rates at confluence using above data:
 4.053 4.009

Area of streams before confluence:
 0.465 0.397

Results of confluence:
 Total flow rate = 4.053(CFS)
 Time of concentration = 6.501 min.
 Effective stream area after confluence = 0.862(Ac.)

 Process from Point/Station 521.000 to Point/Station 523.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 666.000(Ft.)
 Downstream point/station elevation = 665.000(Ft.)
 Pipe length = 25.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 4.053(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 4.053(CFS)
 Normal flow depth in pipe = 6.48(In.)
 Flow top width inside pipe = 11.96(In.)
 Critical Depth = 10.23(In.)
 Pipe flow velocity = 9.36(Ft/s)
 Travel time through pipe = 0.04 min.
 Time of concentration (TC) = 6.55 min.
 End of computations, total study area = 0.862 (Ac.)

San Diego County Rational Hydrology Program
CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13

OUTFALL 3 - Las Posas Road: Combination of Street A, B, C, D and WQ Pond E, F, and Park B
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052OUTFALL3

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 90.000(Ft.)
Highest elevation = 750.000(Ft.)
Lowest elevation = 745.000(Ft.)
Elevation difference = 5.000(Ft.) Slope = 5.556 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 5.56 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 5.70 minutes
(for slope value of 5.00 %)
Rainfall intensity (I) = 8.474(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.336(CFS)
Total initial stream area = 0.066(Ac.)

Process from Point/Station 2.000 to Point/Station 3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 737.000(Ft.)
Downstream point/station elevation = 732.000(Ft.)
Pipe length = 54.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.336(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.336(CFS)

Normal flow depth in pipe = 1.80(In.)
Flow top width inside pipe = 5.50(In.)
Critical Depth = 3.52(In.)
Pipe flow velocity = 6.76(Ft/s)
Travel time through pipe = 0.13 min.
Time of concentration (TC) = 5.83 min.

Process from Point/Station 3.000 to Point/Station 3.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.83 min.
Rainfall intensity = 8.349(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.077
Subarea runoff = 0.306(CFS) for 0.062(Ac.)
Total runoff = 0.641(CFS) Total area = 0.128(Ac.)

Process from Point/Station 3.000 to Point/Station 4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 732.000(Ft.)
Downstream point/station elevation = 727.000(Ft.)
Pipe length = 54.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.641(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.641(CFS)
Normal flow depth in pipe = 2.55(In.)
Flow top width inside pipe = 5.93(In.)
Critical Depth = 4.88(In.)
Pipe flow velocity = 8.08(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 5.94 min.

Process from Point/Station 4.000 to Point/Station 4.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.94 min.
Rainfall intensity = 8.248(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.115
Subarea runoff = 0.304(CFS) for 0.063(Ac.)
Total runoff = 0.945(CFS) Total area = 0.191(Ac.)

Process from Point/Station 4.000 to Point/Station 5.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 727.000(Ft.)

Downstream point/station elevation = 717.000(Ft.)
 Pipe length = 100.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.945(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.945(CFS)
 Normal flow depth in pipe = 3.11(In.)
 Flow top width inside pipe = 6.00(In.)
 Critical Depth = 5.60(In.)
 Pipe flow velocity = 9.18(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 6.13 min.

 Process from Point/Station 5.000 to Point/Station 5.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.13 min.
 Rainfall intensity = 8.089(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.160
 Subarea runoff = 0.351(CFS) for 0.076(Ac.)
 Total runoff = 1.296(CFS) Total area = 0.267(Ac.)

 Process from Point/Station 5.000 to Point/Station 6.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 717.000(Ft.)
 Downstream point/station elevation = 710.000(Ft.)
 Pipe length = 110.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.296(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 1.296(CFS)
 Normal flow depth in pipe = 4.51(In.)
 Flow top width inside pipe = 5.18(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 8.17(Ft/s)
 Travel time through pipe = 0.22 min.
 Time of concentration (TC) = 6.35 min.

 Process from Point/Station 6.000 to Point/Station 6.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.35 min.
 Rainfall intensity = 7.904(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.205
 Subarea runoff = 0.321(CFS) for 0.074(Ac.)
 Total runoff = 1.617(CFS) Total area = 0.341(Ac.)

```

*****
Process from Point/Station      6.000 to Point/Station      6.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.341(Ac.)
 Runoff from this stream = 1.617(CFS)
 Time of concentration = 6.35 min.
 Rainfall intensity = 7.904(In/Hr)

```

*****
Process from Point/Station      6.100 to Point/Station      6.100
**** USER DEFINED FLOW INFORMATION AT A POINT ****

```

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Rainfall intensity (I) = 4.747(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 14.00 min. Rain intensity = 4.75(In/Hr)
 Total area = 30.120(Ac.) Total runoff = 53.150(CFS)

```

*****
Process from Point/Station      6.100 to Point/Station      6.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 695.000(Ft.)
 Downstream point/station elevation = 692.400(Ft.)
 Pipe length = 160.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 53.150(CFS)
 Nearest computed pipe diameter = 33.00(In.)
 Calculated individual pipe flow = 53.150(CFS)
 Normal flow depth in pipe = 22.08(In.)
 Flow top width inside pipe = 31.06(In.)
 Critical Depth = 28.62(In.)
 Pipe flow velocity = 12.57(Ft/s)
 Travel time through pipe = 0.21 min.
 Time of concentration (TC) = 14.21 min.

```

*****
Process from Point/Station      6.000 to Point/Station      6.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 30.120(Ac.)
 Runoff from this stream = 53.150(CFS)
 Time of concentration = 14.21 min.
 Rainfall intensity = 4.701(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.617	6.35	7.904
2	53.150	14.21	4.701
Qmax(1) =			
	1.000 *	1.000 *	1.617) +
	1.000 *	0.447 *	53.150) + = 25.367
Qmax(2) =			
	0.595 *	1.000 *	1.617) +
	1.000 *	1.000 *	53.150) + = 54.112

Total of 2 streams to confluence:
Flow rates before confluence point:
1.617 53.150
Maximum flow rates at confluence using above data:
25.367 54.112
Area of streams before confluence:
0.341 30.120
Results of confluence:
Total flow rate = 54.112(CFS)
Time of concentration = 14.212 min.
Effective stream area after confluence = 30.461(Ac.)

Process from Point/Station 6.000 to Point/Station 13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 692.400(Ft.)
Downstream point/station elevation = 692.000(Ft.)
Pipe length = 10.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 54.112(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 54.112(CFS)
Normal flow depth in pipe = 19.55(In.)
Flow top width inside pipe = 24.14(In.)
Critical depth could not be calculated.
Pipe flow velocity = 17.56(Ft/s)
Travel time through pipe = 0.01 min.
Time of concentration (TC) = 14.22 min.

Process from Point/Station 13.000 to Point/Station 13.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 30.461(Ac.)
Runoff from this stream = 54.112(CFS)
Time of concentration = 14.22 min.
Rainfall intensity = 4.699(In/Hr)

Process from Point/Station 1.000 to Point/Station 7.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 94.000(Ft.)
Highest elevation = 750.000(Ft.)
Lowest elevation = 745.000(Ft.)
Elevation difference = 5.000(Ft.) Slope = 5.319 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 5.32 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 5.70 minutes
(for slope value of 5.00 %)
Rainfall intensity (I) = 8.474(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.422(CFS)
Total initial stream area = 0.083(Ac.)

```

*****
Process from Point/Station      7.000 to Point/Station      8.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 737.000(Ft.)
Downstream point/station elevation = 733.000(Ft.)
Pipe length = 54.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.422(CFS)
Given pipe size = 6.00(In.)
Calculated individual pipe flow = 0.422(CFS)
Normal flow depth in pipe = 2.16(In.)
Flow top width inside pipe = 5.76(In.)
Critical Depth = 3.97(In.)
Pipe flow velocity = 6.65(Ft/s)
Travel time through pipe = 0.14 min.
Time of concentration (TC) = 5.84 min.

*****
Process from Point/Station      8.000 to Point/Station      8.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.84 min.
Rainfall intensity = 8.347(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.086
Subarea runoff = 0.299(CFS) for 0.061(Ac.)
Total runoff = 0.721(CFS) Total area = 0.144(Ac.)

*****
Process from Point/Station      8.000 to Point/Station      9.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 733.000(Ft.)
Downstream point/station elevation = 729.000(Ft.)
Pipe length = 50.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.721(CFS)
Given pipe size = 6.00(In.)
Calculated individual pipe flow = 0.721(CFS)
Normal flow depth in pipe = 2.84(In.)
Flow top width inside pipe = 5.99(In.)
Critical Depth = 5.12(In.)
Pipe flow velocity = 7.89(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 5.94 min.

*****
Process from Point/Station      9.000 to Point/Station      9.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.94 min.
Rainfall intensity = 8.251(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area

```

(Q=KCIA) is C = 0.600 CA = 0.118
 Subarea runoff = 0.254(CFS) for 0.053(Ac.)
 Total runoff = 0.975(CFS) Total area = 0.197(Ac.)

 Process from Point/Station 9.000 to Point/Station 10.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 729.000(Ft.)
 Downstream point/station elevation = 722.000(Ft.)
 Pipe length = 77.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.975(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.975(CFS)
 Normal flow depth in pipe = 3.27(In.)
 Flow top width inside pipe = 5.98(In.)
 Critical Depth = 5.64(In.)
 Pipe flow velocity = 8.92(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 6.08 min.

 Process from Point/Station 10.000 to Point/Station 10.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.08 min.
 Rainfall intensity = 8.125(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.151
 Subarea runoff = 0.248(CFS) for 0.054(Ac.)
 Total runoff = 1.224(CFS) Total area = 0.251(Ac.)

 Process from Point/Station 10.000 to Point/Station 11.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 722.000(Ft.)
 Downstream point/station elevation = 712.000(Ft.)
 Pipe length = 99.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.224(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 1.224(CFS)
 Normal flow depth in pipe = 3.65(In.)
 Flow top width inside pipe = 5.86(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 9.79(Ft/s)
 Travel time through pipe = 0.17 min.
 Time of concentration (TC) = 6.25 min.

 Process from Point/Station 11.000 to Point/Station 11.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)

```

Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      6.25 min.
Rainfall intensity =      7.983(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA =      0.191
Subarea runoff =      0.304(CFS) for      0.068(Ac.)
Total runoff =      1.528(CFS)      Total area =      0.319(Ac.)

*****
Process from Point/Station      11.000 to Point/Station      12.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 712.000(Ft.)
Downstream point/station elevation = 709.000(Ft.)
Pipe length = 99.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.528(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.528(CFS)
Normal flow depth in pipe = 4.66(In.)
Flow top width inside pipe = 8.99(In.)
Critical Depth = 6.83(In.)
Pipe flow velocity = 6.62(Ft/s)
Travel time through pipe = 0.25 min.
Time of concentration (TC) = 6.50 min.

*****
Process from Point/Station      12.000 to Point/Station      12.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.50 min.
Rainfall intensity = 7.784(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.224
Subarea runoff = 0.219(CFS) for 0.055(Ac.)
Total runoff = 1.747(CFS)      Total area = 0.374(Ac.)

*****
Process from Point/Station      12.000 to Point/Station      13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 709.000(Ft.)
Downstream point/station elevation = 692.000(Ft.)
Pipe length = 34.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.747(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.747(CFS)
Normal flow depth in pipe = 2.79(In.)
Flow top width inside pipe = 5.98(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.57(Ft/s)
Travel time through pipe = 0.03 min.
Time of concentration (TC) = 6.53 min.

*****
Process from Point/Station      13.000 to Point/Station      13.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

```

Stream flow area = 0.374(Ac.)
 Runoff from this stream = 1.747(CFS)
 Time of concentration = 6.53 min.
 Rainfall intensity = 7.761(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	54.112	14.22	4.699
2	1.747	6.53	7.761

Qmax(1) =
 1.000 * 1.000 * 54.112) +
 0.605 * 1.000 * 1.747) + = 55.169

Qmax(2) =
 1.000 * 0.459 * 54.112) +
 1.000 * 1.000 * 1.747) + = 26.600

Total of 2 streams to confluence:
 Flow rates before confluence point:
 54.112 1.747
 Maximum flow rates at confluence using above data:
 55.169 26.600
 Area of streams before confluence:
 30.461 0.374
 Results of confluence:
 Total flow rate = 55.169(CFS)
 Time of concentration = 14.222 min.
 Effective stream area after confluence = 30.835(Ac.)

 Process from Point/Station 13.000 to Point/Station 14.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 692.000(Ft.)
 Downstream point/station elevation = 691.300(Ft.)
 Pipe length = 83.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 55.169(CFS)
 Nearest computed pipe diameter = 36.00(In.)
 Calculated individual pipe flow = 55.169(CFS)
 Normal flow depth in pipe = 26.72(In.)
 Flow top width inside pipe = 31.49(In.)
 Critical Depth = 28.94(In.)
 Pipe flow velocity = 9.81(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 14.36 min.

 Process from Point/Station 14.000 to Point/Station 14.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 The area added to the existing stream causes a
 a lower flow rate of Q = 51.409(CFS)
 therefore the upstream flow rate of Q = 55.169(CFS) is being used
 Time of concentration = 14.36 min.
 Rainfall intensity = 4.669(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.356 CA = 11.011
 Subarea runoff = 0.000(CFS) for 0.066(Ac.)
 Total runoff = 55.169(CFS) Total area = 30.901(Ac.)


```

*****
Process from Point/Station      14.000 to Point/Station      14.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 30.901(Ac.)
 Runoff from this stream = 55.169(CFS)
 Time of concentration = 14.36 min.
 Rainfall intensity = 4.669(In/Hr)

```

*****
Process from Point/Station      6.000 to Point/Station      14.000
**** INITIAL AREA EVALUATION ****

```

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 83.000(Ft.)
 Highest elevation = 715.000(Ft.)
 Lowest elevation = 707.000(Ft.)
 Elevation difference = 8.000(Ft.) Slope = 9.639 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 9.64 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 4.50 minutes
 (for slope value of 10.00 %)
 Calculated TC of 4.500 minutes is less than 5 minutes,
 resetting TC to 5.0 minutes for rainfall intensity calculations
 Rainfall intensity (I) = 9.222(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.365(CFS)
 Total initial stream area = 0.066(Ac.)

```

*****
Process from Point/Station      14.000 to Point/Station      14.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.066(Ac.)
 Runoff from this stream = 0.365(CFS)
 Time of concentration = 4.50 min.
 Rainfall intensity = 9.222(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	55.169	14.36	4.669
2	0.365	4.50	9.222
Qmax(1) =			
	1.000 *	1.000 *	55.169) +
	0.506 *	1.000 *	0.365) + = 55.354
Qmax(2) =			
	1.000 *	0.313 *	55.169) +
	1.000 *	1.000 *	0.365) + = 17.650

Total of 2 streams to confluence:
 Flow rates before confluence point:
 55.169 0.365

Maximum flow rates at confluence using above data:
 55.354 17.650
 Area of streams before confluence:
 30.901 0.066
 Results of confluence:
 Total flow rate = 55.354(CFS)
 Time of concentration = 14.363 min.
 Effective stream area after confluence = 30.967(Ac.)

 Process from Point/Station 14.000 to Point/Station 19.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.300(Ft.)
 Downstream point/station elevation = 690.700(Ft.)
 Pipe length = 58.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 55.354(CFS)
 Nearest computed pipe diameter = 36.00(In.)
 Calculated individual pipe flow = 55.354(CFS)
 Normal flow depth in pipe = 24.70(In.)
 Flow top width inside pipe = 33.41(In.)
 Critical Depth = 28.97(In.)
 Pipe flow velocity = 10.70(Ft/s)
 Travel time through pipe = 0.09 min.
 Time of concentration (TC) = 14.45 min.

 Process from Point/Station 19.000 to Point/Station 19.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 30.967(Ac.)
 Runoff from this stream = 55.354(CFS)
 Time of concentration = 14.45 min.
 Rainfall intensity = 4.650(In/Hr)

 Process from Point/Station 12.000 to Point/Station 17.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 74.000(Ft.)
 Highest elevation = 713.000(Ft.)
 Lowest elevation = 706.000(Ft.)
 Elevation difference = 7.000(Ft.) Slope = 9.459 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 9.46 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 4.50 minutes
 (for slope value of 10.00 %)
 Calculated TC of 4.500 minutes is less than 5 minutes,
 resetting TC to 5.0 minutes for rainfall intensity calculations
 Rainfall intensity (I) = 9.222(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.315(CFS)
 Total initial stream area = 0.057(Ac.)

Process from Point/Station 17.000 to Point/Station 18.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 700.000(Ft.)
 Downstream point/station elevation = 695.000(Ft.)
 Pipe length = 52.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.315(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.315(CFS)
 Normal flow depth in pipe = 1.73(In.)
 Flow top width inside pipe = 5.43(In.)
 Critical Depth = 3.41(In.)
 Pipe flow velocity = 6.72(Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 4.63 min.

 Process from Point/Station 18.000 to Point/Station 18.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 4.63 min.
 Rainfall intensity = 9.222(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.056
 Subarea runoff = 0.205(CFS) for 0.037(Ac.)
 Total runoff = 0.520(CFS) Total area = 0.094(Ac.)

 Process from Point/Station 18.000 to Point/Station 19.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 695.000(Ft.)
 Downstream point/station elevation = 690.700(Ft.)
 Pipe length = 38.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.520(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.520(CFS)
 Normal flow depth in pipe = 2.16(In.)
 Flow top width inside pipe = 5.76(In.)
 Critical Depth = 4.41(In.)
 Pipe flow velocity = 8.21(Ft/s)
 Travel time through pipe = 0.08 min.
 Time of concentration (TC) = 4.71 min.

 Process from Point/Station 19.000 to Point/Station 19.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.094(Ac.)
 Runoff from this stream = 0.520(CFS)
 Time of concentration = 4.71 min.
 Rainfall intensity = 9.222(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	55.354	14.45	4.650

```

2          0.520          4.71          9.222
Qmax(1) =
          1.000 *          1.000 *          55.354) +
          0.504 *          1.000 *          0.520) + =          55.616
Qmax(2) =
          1.000 *          0.326 *          55.354) +
          1.000 *          1.000 *          0.520) + =          18.544

```

```

Total of 2 streams to confluence:
Flow rates before confluence point:
          55.354          0.520
Maximum flow rates at confluence using above data:
          55.616          18.544
Area of streams before confluence:
          30.967          0.094
Results of confluence:
Total flow rate =          55.616(CFS)
Time of concentration =          14.453 min.
Effective stream area after confluence =          31.061(Ac.)

```

```

*****
Process from Point/Station          19.000 to Point/Station          15.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =          690.700(Ft.)
Downstream point/station elevation =          690.000(Ft.)
Pipe length =          41.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow =          55.616(CFS)
Nearest computed pipe diameter =          33.00(In.)
Calculated individual pipe flow =          55.616(CFS)
Normal flow depth in pipe =          22.43(In.)
Flow top width inside pipe =          30.80(In.)
Critical Depth =          29.11(In.)
Pipe flow velocity =          12.94(Ft/s)
Travel time through pipe =          0.05 min.
Time of concentration (TC) =          14.51 min.

```

```

*****
Process from Point/Station          15.000 to Point/Station          15.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
The area added to the existing stream causes a
a lower flow rate of Q =          51.729(CFS)
therefore the upstream flow rate of Q =          55.616(CFS) is being used
Time of concentration =          14.51 min.
Rainfall intensity =          4.639(In/Hr) for a          100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.358 CA =          11.150
Subarea runoff =          0.000(CFS) for          0.073(Ac.)
Total runoff =          55.616(CFS)          Total area =          31.134(Ac.)

```

```

*****
Process from Point/Station          15.000 to Point/Station          21.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =          690.000(Ft.)
Downstream point/station elevation =          687.000(Ft.)
Pipe length =          62.50(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow =          55.616(CFS)
Nearest computed pipe diameter =          27.00(In.)

```

Calculated individual pipe flow = 55.616(CFS)
Normal flow depth in pipe = 18.61(In.)
Flow top width inside pipe = 24.99(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.04(Ft/s)
Travel time through pipe = 0.05 min.
Time of concentration (TC) = 14.56 min.

Process from Point/Station 21.000 to Point/Station 21.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 31.134(Ac.)
Runoff from this stream = 55.616(CFS)
Time of concentration = 14.56 min.
Rainfall intensity = 4.628(In/Hr)

Process from Point/Station 18.000 to Point/Station 20.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 101.000(Ft.)
Highest elevation = 701.000(Ft.)
Lowest elevation = 693.000(Ft.)
Elevation difference = 8.000(Ft.) Slope = 7.921 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 7.92 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 4.50 minutes
(for slope value of 10.00 %)
Calculated TC of 4.500 minutes is less than 5 minutes,
resetting TC to 5.0 minutes for rainfall intensity calculations
Rainfall intensity (I) = 9.222(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.404(CFS)
Total initial stream area = 0.073(Ac.)

Process from Point/Station 20.000 to Point/Station 21.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
Downstream point/station elevation = 687.000(Ft.)
Pipe length = 40.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.404(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.404(CFS)
Normal flow depth in pipe = 2.84(In.)
Flow top width inside pipe = 5.99(In.)
Critical Depth = 3.88(In.)
Pipe flow velocity = 4.41(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 4.65 min.

Process from Point/Station 21.000 to Point/Station 21.000

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.073(Ac.)
 Runoff from this stream = 0.404(CFS)
 Time of concentration = 4.65 min.
 Rainfall intensity = 9.222(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	55.616	14.56	4.628
2	0.404	4.65	9.222

Qmax(1) =
 1.000 * 1.000 * 55.616) +
 0.502 * 1.000 * 0.404) + = 55.819
 Qmax(2) =
 1.000 * 0.319 * 55.616) +
 1.000 * 1.000 * 0.404) + = 18.170

Total of 2 streams to confluence:
 Flow rates before confluence point:
 55.616 0.404
 Maximum flow rates at confluence using above data:
 55.819 18.170
 Area of streams before confluence:
 31.134 0.073
 Results of confluence:
 Total flow rate = 55.819(CFS)
 Time of concentration = 14.560 min.
 Effective stream area after confluence = 31.207(Ac.)

 Process from Point/Station 21.000 to Point/Station 16.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
 Downstream point/station elevation = 686.800(Ft.)
 Pipe length = 12.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 55.819(CFS)
 Nearest computed pipe diameter = 33.00(In.)
 Calculated individual pipe flow = 55.819(CFS)
 Normal flow depth in pipe = 22.69(In.)
 Flow top width inside pipe = 30.59(In.)
 Critical Depth = 29.16(In.)
 Pipe flow velocity = 12.82(Ft/s)
 Travel time through pipe = 0.02 min.
 Time of concentration (TC) = 14.58 min.

 Process from Point/Station 16.000 to Point/Station 16.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 The area added to the existing stream causes a
 a lower flow rate of Q = 51.921(CFS)
 therefore the upstream flow rate of Q = 55.819(CFS) is being used
 Time of concentration = 14.58 min.
 Rainfall intensity = 4.625(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area

(Q=KCIA) is C = 0.359 CA = 11.227
 Subarea runoff = 0.000(CFS) for 0.054(Ac.)
 Total runoff = 55.819(CFS) Total area = 31.261(Ac.)

 Process from Point/Station 16.000 to Point/Station 43.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.800(Ft.)
 Downstream point/station elevation = 684.000(Ft.)
 Pipe length = 12.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 55.819(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 55.819(CFS)
 Normal flow depth in pipe = 13.31(In.)
 Flow top width inside pipe = 20.23(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 34.73(Ft/s)
 Travel time through pipe = 0.01 min.
 Time of concentration (TC) = 14.58 min.

 Process from Point/Station 43.000 to Point/Station 43.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 31.261(Ac.)
 Runoff from this stream = 55.819(CFS)
 Time of concentration = 14.58 min.
 Rainfall intensity = 4.624(In/Hr)

 Process from Point/Station 43.000 to Point/Station 43.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 9.00 min. Rain intensity = 6.31(In/Hr)
 Total area = 3.835(Ac.) Total runoff = 14.250(CFS)

 Process from Point/Station 43.000 to Point/Station 43.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 3.835(Ac.)
 Runoff from this stream = 14.250(CFS)
 Time of concentration = 9.00 min.
 Rainfall intensity = 6.312(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	55.819	14.58	4.624
2	14.250	9.00	6.312

Qmax(1) = 1.000 * 1.000 * 55.819) +

```

Total of 2 streams to confluence:
Flow rates before confluence point:
    55.819      14.250
Maximum flow rates at confluence using above data:
    66.258      48.702
Area of streams before confluence:
    31.261      3.835
Results of confluence:
Total flow rate =      66.258(CFS)
Time of concentration =      14.582 min.
Effective stream area after confluence =      35.096(Ac.)

```

```

Upstream point/station elevation = 684.600(Ft.)
Downstream point/station elevation = 680.500(Ft.)
Pipe length = 81.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 66.258(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 66.258(CFS)
Normal flow depth in pipe = 21.02(In.)
Flow top width inside pipe = 22.42(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.94(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 14.65 min.

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
The area added to the existing stream causes a
a lower flow rate of Q =      62.565(CFS)
therefore the upstream flow rate of Q =      66.258(CFS) is being used
Time of concentration =      14.65 min.
Rainfall intensity =      4.610(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.386      CA =      13.572
Subarea runoff =      0.000(CFS) for      0.074(Ac.)
Total runoff =      66.258(CFS)      Total area =      35.170(Ac.)

```

```
Upstream point/station elevation = 680.500(Ft.)
Downstream point/station elevation = 674.300(Ft.)
Pipe length = 80.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 66.258(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 66.258(CFS)
Normal flow depth in pipe = 17.74(In.)
Flow top width inside pipe = 25.63(In.)
```


Critical depth could not be calculated.
 Pipe flow velocity = 23.91(Ft/s)
 Travel time through pipe = 0.06 min.
 Time of concentration (TC) = 14.71 min.

 Process from Point/Station 24.000 to Point/Station 24.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 35.170(Ac.)
 Runoff from this stream = 66.258(CFS)
 Time of concentration = 14.71 min.
 Rainfall intensity = 4.599(In/Hr)

 Process from Point/Station 20.000 to Point/Station 23.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 191.000(Ft.)
 Highest elevation = 693.000(Ft.)
 Lowest elevation = 680.000(Ft.)
 Elevation difference = 13.000(Ft.) Slope = 6.806 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 6.81 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 4.75 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (100.000^{.5})] / (6.806^{(1/3)}) = 4.75$
 Rainfall intensity (I) = 9.533(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.949(CFS)
 Total initial stream area = 0.166(Ac.)

 Process from Point/Station 23.000 to Point/Station 24.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 675.500(Ft.)
 Downstream point/station elevation = 674.300(Ft.)
 Pipe length = 33.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.949(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.949(CFS)
 Normal flow depth in pipe = 4.39(In.)
 Flow top width inside pipe = 5.31(In.)
 Critical Depth = 5.60(In.)
 Pipe flow velocity = 6.15(Ft/s)
 Travel time through pipe = 0.09 min.
 Time of concentration (TC) = 4.84 min.

 Process from Point/Station 24.000 to Point/Station 24.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.166(Ac.)

Runoff from this stream = 0.949(CFS)
 Time of concentration = 4.84 min.
 Rainfall intensity = 9.419(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	66.258	14.71	4.599
2	0.949	4.84	9.419

Qmax(1) =
 1.000 * 1.000 * 66.258) +
 0.488 * 1.000 * 0.949) + = 66.721
 Qmax(2) =
 1.000 * 0.329 * 66.258) +
 1.000 * 1.000 * 0.949) + = 22.750

Total of 2 streams to confluence:
 Flow rates before confluence point:
 66.258 0.949
 Maximum flow rates at confluence using above data:
 66.721 22.750
 Area of streams before confluence:
 35.170 0.166
 Results of confluence:
 Total flow rate = 66.721(CFS)
 Time of concentration = 14.705 min.
 Effective stream area after confluence = 35.336(Ac.)

 Process from Point/Station 24.000 to Point/Station 25.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 674.300(Ft.)
 Downstream point/station elevation = 673.500(Ft.)
 Pipe length = 50.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 66.721(CFS)
 Nearest computed pipe diameter = 33.00(In.)
 Calculated individual pipe flow = 66.721(CFS)
 Normal flow depth in pipe = 26.95(In.)
 Flow top width inside pipe = 25.53(In.)
 Critical Depth = 30.76(In.)
 Pipe flow velocity = 12.84(Ft/s)
 Travel time through pipe = 0.06 min.
 Time of concentration (TC) = 14.77 min.

 Process from Point/Station 25.000 to Point/Station 25.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 35.336(Ac.)
 Runoff from this stream = 66.721(CFS)
 Time of concentration = 14.77 min.
 Rainfall intensity = 4.586(In/Hr)

 Process from Point/Station 25.200 to Point/Station 25.100
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000

Sub-Area C Value = 0.350
 Initial subarea total flow distance = 237.000(Ft.)
 Highest elevation = 732.000(Ft.)
 Lowest elevation = 710.500(Ft.)
 Elevation difference = 21.500(Ft.) Slope = 9.072 %
 Top of Initial Area Slope adjusted by User to 11.400 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 11.40 %, in a development type of
 Permanent Open Space
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 6.90 minutes
 (for slope value of 10.00 %)
 Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
 Subarea runoff = 6.975(CFS)
 Total initial stream area = 2.660(Ac.)

 Process from Point/Station 25.100 to Point/Station 25.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 705.000(Ft.)
 Downstream point/station elevation = 673.500(Ft.)
 Pipe length = 193.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 6.975(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 6.975(CFS)
 Normal flow depth in pipe = 5.89(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 18.18(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 7.08 min.

 Process from Point/Station 25.000 to Point/Station 25.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 2.660(Ac.)
 Runoff from this stream = 6.975(CFS)
 Time of concentration = 7.08 min.
 Rainfall intensity = 7.370(In/Hr)

 Process from Point/Station 22.000 to Point/Station 25.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 130.000(Ft.)
 Highest elevation = 685.000(Ft.)
 Lowest elevation = 678.000(Ft.)
 Elevation difference = 7.000(Ft.) Slope = 5.385 %
 Top of Initial Area Slope adjusted by User to 5.750 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 5.75 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.02 minutes

```

TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 100.000^.5)/( 5.750^(1/3))]= 5.02
Rainfall intensity (I) = 9.194(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.530(CFS)
Total initial stream area = 0.096(Ac.)

*****
Process from Point/Station 25.000 to Point/Station 25.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.096(Ac.)
Runoff from this stream = 0.530(CFS)
Time of concentration = 5.02 min.
Rainfall intensity = 9.194(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 66.721 14.77 4.586
2 6.975 7.08 7.370
3 0.530 5.02 9.194

Qmax(1) =
1.000 * 1.000 * 66.721) +
0.622 * 1.000 * 6.975) +
0.499 * 1.000 * 0.530) + = 71.325

Qmax(2) =
1.000 * 0.479 * 66.721) +
1.000 * 1.000 * 6.975) +
0.802 * 1.000 * 0.530) + = 39.368

Qmax(3) =
1.000 * 0.340 * 66.721) +
1.000 * 0.710 * 6.975) +
1.000 * 1.000 * 0.530) + = 28.174

Total of 3 streams to confluence:
Flow rates before confluence point:
66.721 6.975 0.530
Maximum flow rates at confluence using above data:
71.325 39.368 28.174
Area of streams before confluence:
35.336 2.660 0.096
Results of confluence:
Total flow rate = 71.325(CFS)
Time of concentration = 14.770 min.
Effective stream area after confluence = 38.092(Ac.)

*****
Process from Point/Station 25.000 to Point/Station 26.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 673.500(Ft.)
Downstream point/station elevation = 669.000(Ft.)
Pipe length = 111.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 71.325(CFS)
Nearest computed pipe diameter = 30.00(In.)
Calculated individual pipe flow = 71.325(CFS)
Normal flow depth in pipe = 21.52(In.)
Flow top width inside pipe = 27.02(In.)
Critical depth could not be calculated.
Pipe flow velocity = 18.93(Ft/s)
Travel time through pipe = 0.10 min.
Time of concentration (TC) = 14.87 min.

*****

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Process from Point/Station      26.000 to Point/Station      26.000
**** SUBAREA FLOW ADDITION ****

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```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
The area added to the existing stream causes a
a lower flow rate of Q =      67.210(CFS)
therefore the upstream flow rate of Q =      71.325(CFS) is being used
Time of concentration =      14.87 min.
Rainfall intensity =      4.566(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.385  CA =      14.720
Subarea runoff =      0.000(CFS) for      0.099(Ac.)
Total runoff =      71.325(CFS)      Total area =      38.191(Ac.)

```

```

*****
Process from Point/Station      26.000 to Point/Station      26.000
**** CONFLUENCE OF MINOR STREAMS ****

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```

Along Main Stream number: 1 in normal stream number 1
Stream flow area =      38.191(Ac.)
Runoff from this stream =      71.325(CFS)
Time of concentration =      14.87 min.
Rainfall intensity =      4.566(In/Hr)

```

```

*****
Process from Point/Station      25.000 to Point/Station      26.000
**** INITIAL AREA EVALUATION ****

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```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 110.000(Ft.)
Highest elevation = 678.000(Ft.)
Lowest elevation = 673.500(Ft.)
Elevation difference = 4.500(Ft.) Slope = 4.091 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 4.09 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.63 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*(100.000^0.5)/(4.091^(1/3))]= 5.63
Rainfall intensity (I) = 8.545(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.508(CFS)
Total initial stream area = 0.099(Ac.)

```

```

*****
Process from Point/Station      26.000 to Point/Station      26.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.099(Ac.)
Runoff from this stream = 0.508(CFS)
Time of concentration = 5.63 min.

```

Rainfall intensity = 8.545(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	71.325	14.87	4.566
2	0.508	5.63	8.545

Qmax(1) =
 1.000 * 1.000 * 71.325) +
 0.534 * 1.000 * 0.508) + = 71.596
 Qmax(2) =
 1.000 * 0.378 * 71.325) +
 1.000 * 1.000 * 0.508) + = 27.503

Total of 2 streams to confluence:
 Flow rates before confluence point:
 71.325 0.508
 Maximum flow rates at confluence using above data:
 71.596 27.503
 Area of streams before confluence:
 38.191 0.099
 Results of confluence:
 Total flow rate = 71.596(CFS)
 Time of concentration = 14.868 min.
 Effective stream area after confluence = 38.290(Ac.)

 Process from Point/Station 26.000 to Point/Station 63.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 669.000(Ft.)
 Downstream point/station elevation = 662.000(Ft.)
 Pipe length = 148.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 71.596(CFS)
 Nearest computed pipe diameter = 30.00(In.)
 Calculated individual pipe flow = 71.596(CFS)
 Normal flow depth in pipe = 20.34(In.)
 Flow top width inside pipe = 28.03(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 20.20(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 14.99 min.

 Process from Point/Station 63.000 to Point/Station 63.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 1
 Stream flow area = 38.290(Ac.)
 Runoff from this stream = 71.596(CFS)
 Time of concentration = 14.99 min.
 Rainfall intensity = 4.542(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 23.000 to Point/Station 27.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450

```

Sub-Area C Value = 0.600
Initial subarea total flow distance = 111.000(Ft.)
Highest elevation = 680.000(Ft.)
Lowest elevation = 675.000(Ft.)
Elevation difference = 5.000(Ft.) Slope = 4.505 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 4.50 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.45 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 100.000^0.5)/( 4.505^(1/3))]= 5.45
Rainfall intensity (I) = 8.724(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.445(CFS)
Total initial stream area = 0.085(Ac.)

*****
Process from Point/Station 27.000 to Point/Station 28.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 670.000(Ft.)
Downstream point/station elevation = 664.000(Ft.)
Pipe length = 76.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.445(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.445(CFS)
Normal flow depth in pipe = 2.18(In.)
Flow top width inside pipe = 5.77(In.)
Critical Depth = 4.08(In.)
Pipe flow velocity = 6.90(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 5.63 min.

*****
Process from Point/Station 28.000 to Point/Station 28.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.63 min.
Rainfall intensity = 8.539(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.085
Subarea runoff = 0.278(CFS) for 0.056(Ac.)
Total runoff = 0.722(CFS) Total area = 0.141(Ac.)

*****
Process from Point/Station 28.000 to Point/Station 29.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 664.000(Ft.)
Downstream point/station elevation = 663.000(Ft.)
Pipe length = 66.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.722(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.722(CFS)
Normal flow depth in pipe = 3.70(In.)
Flow top width inside pipe = 8.86(In.)
Critical Depth = 4.65(In.)
Pipe flow velocity = 4.22(Ft/s)

```

Travel time through pipe = 0.26 min.
Time of concentration (TC) = 5.89 min.

Process from Point/Station 29.000 to Point/Station 29.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.89 min.
Rainfall intensity = 8.293(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.122
Subarea runoff = 0.288(CFS) for 0.062(Ac.)
Total runoff = 1.010(CFS) Total area = 0.203(Ac.)

Process from Point/Station 29.000 to Point/Station 29.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 663.000(Ft.)
Downstream point/station elevation = 662.500(Ft.)
Pipe length = 32.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.010(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.010(CFS)
Normal flow depth in pipe = 4.44(In.)
Flow top width inside pipe = 9.00(In.)
Critical Depth = 5.53(In.)
Pipe flow velocity = 4.65(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 6.01 min.

Process from Point/Station 29.100 to Point/Station 29.100
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 0.203(Ac.)
Runoff from this stream = 1.010(CFS)
Time of concentration = 6.01 min.
Rainfall intensity = 8.191(In/Hr)

Process from Point/Station 62.000 to Point/Station 62.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 9.00 min. Rain intensity = 6.31(In/Hr)
Total area = 51.810(Ac.) Total runoff = 135.500(CFS)


```

*****
Process from Point/Station      62.000 to Point/Station      29.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 663.000(Ft.)
Downstream point/station elevation = 662.500(Ft.)
Pipe length = 34.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 135.500(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 135.500(CFS)
Normal flow depth in pipe = 34.13(In.)
Flow top width inside pipe = 38.53(In.)
Critical Depth = 41.17(In.)
Pipe flow velocity = 15.07(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 9.04 min.

```

```

*****
Process from Point/Station      29.100 to Point/Station      29.100
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 2 in normal stream number 2
Stream flow area = 51.810(Ac.)
Runoff from this stream = 135.500(CFS)
Time of concentration = 9.04 min.
Rainfall intensity = 6.295(In/Hr)
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.010	6.01	8.191
2	135.500	9.04	6.295
Qmax(1) =			
	1.000 *	1.000 *	1.010) +
	1.000 *	0.665 *	135.500) + = 91.094
Qmax(2) =			
	0.769 *	1.000 *	1.010) +
	1.000 *	1.000 *	135.500) + = 136.276

```

Total of 2 streams to confluence:
Flow rates before confluence point:
1.010 135.500
Maximum flow rates at confluence using above data:
91.094 136.276
Area of streams before confluence:
0.203 51.810
Results of confluence:
Total flow rate = 136.276(CFS)
Time of concentration = 9.038 min.
Effective stream area after confluence = 52.013(Ac.)

```

```

*****
Process from Point/Station      29.100 to Point/Station      63.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 662.500(Ft.)
Downstream point/station elevation = 662.000(Ft.)
Pipe length = 36.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 136.276(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 136.276(CFS)
Normal flow depth in pipe = 35.25(In.)
Flow top width inside pipe = 37.08(In.)
Critical Depth = 41.24(In.)
Pipe flow velocity = 14.69(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 9.08 min.

```

```

*****
Process from Point/Station      63.000 to Point/Station      63.000
**** CONFLUENCE OF MAIN STREAMS ****

```

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 52.013(Ac.)
Runoff from this stream = 136.276(CFS)
Time of concentration = 9.08 min.
Rainfall intensity = 6.277(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	71.596	14.99	4.542
2	136.276	9.08	6.277

Qmax(1) =
1.000 * 1.000 * 71.596) +
0.724 * 1.000 * 136.276) + = 170.212

Qmax(2) =
1.000 * 0.606 * 71.596) +
1.000 * 1.000 * 136.276) + = 179.637

Total of 2 main streams to confluence:

Flow rates before confluence point:

71.596 136.276

Maximum flow rates at confluence using above data:

170.212 179.637

Area of streams before confluence:

38.290 52.013

Results of confluence:

Total flow rate = 179.637(CFS)

Time of concentration = 9.078 min.

Effective stream area after confluence = 90.303(Ac.)

```

*****
Process from Point/Station      63.000 to Point/Station      66.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 662.000(Ft.)
Downstream point/station elevation = 661.000(Ft.)
Pipe length = 114.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 179.637(CFS)
Nearest computed pipe diameter = 54.00(In.)
Calculated individual pipe flow = 179.637(CFS)
Normal flow depth in pipe = 43.13(In.)
Flow top width inside pipe = 43.31(In.)
Critical Depth = 46.58(In.)
Pipe flow velocity = 13.20(Ft/s)
Travel time through pipe = 0.14 min.
Time of concentration (TC) = 9.22 min.

```

*****
Process from Point/Station      66.000 to Point/Station      66.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 90.303(Ac.)
Runoff from this stream = 179.637(CFS)
Time of concentration = 9.22 min.
Rainfall intensity = 6.213(In/Hr)

```

*****
Process from Point/Station      26.000 to Point/Station      65.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 262.000(Ft.)
Highest elevation = 673.500(Ft.)
Lowest elevation = 669.000(Ft.)
Elevation difference = 4.500(Ft.) Slope = 1.718 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 80.00 (Ft)
for the top area slope value of 1.72 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.72 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 80.000^0.5)/( 1.718^(1/3))]= 6.72
Rainfall intensity (I) = 7.620(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.960(CFS)
Total initial stream area = 0.210(Ac.)

*****
Process from Point/Station      65.000 to Point/Station      65.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.210(Ac.)
Runoff from this stream = 0.960(CFS)
Time of concentration = 6.72 min.
Rainfall intensity = 7.620(In/Hr)

*****
Process from Point/Station      29.000 to Point/Station      64.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 163.000(Ft.)
Highest elevation = 670.500(Ft.)
Lowest elevation = 668.500(Ft.)
Elevation difference = 2.000(Ft.) Slope = 1.227 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 1.23 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.78 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 65.000^0.5)/( 1.227^(1/3))]= 6.78
Rainfall intensity (I) = 7.579(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.950(CFS)
Total initial stream area = 0.209(Ac.)

```

```

*****
Process from Point/Station      64.000 to Point/Station      66.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 664.000(Ft.)
Downstream point/station elevation = 661.000(Ft.)
Pipe length = 37.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.950(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.950(CFS)
Normal flow depth in pipe = 3.33(In.)
Flow top width inside pipe = 5.96(In.)
Critical Depth = 5.61(In.)
Pipe flow velocity = 8.49(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 6.85 min.

```

```

*****
Process from Point/Station      66.000 to Point/Station      66.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.209(Ac.)
Runoff from this stream = 0.950(CFS)
Time of concentration = 6.85 min.
Rainfall intensity = 7.527(In/Hr)
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	179.637	9.22	6.213
2	0.960	6.72	7.620
3	0.950	6.85	7.527

$Q_{max}(1) = 1.000 * 1.000 * 179.637) + 0.815 * 1.000 * 0.960) + 0.825 * 1.000 * 0.950) + = 181.205$
 $Q_{max}(2) = 1.000 * 0.729 * 179.637) + 1.000 * 1.000 * 0.960) + 1.000 * 0.981 * 0.950) + = 132.810$
 $Q_{max}(3) = 1.000 * 0.743 * 179.637) + 0.988 * 1.000 * 0.960) + 1.000 * 1.000 * 0.950) + = 135.333$

```

Total of 3 streams to confluence:
Flow rates before confluence point:
179.637      0.960      0.950
Maximum flow rates at confluence using above data:
181.205      132.810      135.333
Area of streams before confluence:
90.303      0.210      0.209
Results of confluence:
Total flow rate = 181.205(CFS)
Time of concentration = 9.222 min.
Effective stream area after confluence = 90.722(Ac.)

```

```

*****
Process from Point/Station      66.000 to Point/Station      81.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 661.000(Ft.)
Downstream point/station elevation = 659.680(Ft.)
Pipe length = 132.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 181.205(CFS)
Nearest computed pipe diameter = 54.00(In.)

```

Calculated individual pipe flow = 181.205(CFS)
 Normal flow depth in pipe = 40.88(In.)
 Flow top width inside pipe = 46.32(In.)
 Critical Depth = 46.74(In.)
 Pipe flow velocity = 14.03(Ft/s)
 Travel time through pipe = 0.16 min.
 Time of concentration (TC) = 9.38 min.

 Process from Point/Station 81.000 to Point/Station 81.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 90.722(Ac.)
 Runoff from this stream = 181.205(CFS)
 Time of concentration = 9.38 min.
 Rainfall intensity = 6.146(In/Hr)

 Process from Point/Station 516.000 to Point/Station 524.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 180.000(Ft.)
 Highest elevation = 671.500(Ft.)
 Lowest elevation = 666.000(Ft.)
 Elevation difference = 5.500(Ft.) Slope = 3.056 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 3.06 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.88 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.056^{(1/3)}) = 5.88$
 Rainfall intensity (I) = 8.303(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.126(CFS)
 Total initial stream area = 0.226(Ac.)

 Process from Point/Station 524.000 to Point/Station 81.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.500(Ft.)
 Downstream point/station elevation = 659.680(Ft.)
 Pipe length = 18.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.126(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 1.126(CFS)
 Normal flow depth in pipe = 3.46(In.)
 Flow top width inside pipe = 5.93(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 9.61(Ft/s)
 Travel time through pipe = 0.03 min.
 Time of concentration (TC) = 5.91 min.

 Process from Point/Station 81.000 to Point/Station 81.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.226(Ac.)
Runoff from this stream = 1.126(CFS)
Time of concentration = 5.91 min.
Rainfall intensity = 8.274(In/Hr)

Process from Point/Station 521.000 to Point/Station 538.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 179.000(Ft.)
Highest elevation = 671.500(Ft.)
Lowest elevation = 665.700(Ft.)
Elevation difference = 5.800(Ft.) Slope = 3.240 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.24 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.77 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.240^{(1/3)}) = 5.77$
Rainfall intensity (I) = 8.408(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 1.019(CFS)
Total initial stream area = 0.202(Ac.)

Process from Point/Station 538.000 to Point/Station 81.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.000(Ft.)
Downstream point/station elevation = 659.680(Ft.)
Pipe length = 50.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.019(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.019(CFS)
Normal flow depth in pipe = 3.84(In.)
Flow top width inside pipe = 8.90(In.)
Critical Depth = 5.56(In.)
Pipe flow velocity = 5.66(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 5.92 min.

Process from Point/Station 81.000 to Point/Station 81.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.202(Ac.)
Runoff from this stream = 1.019(CFS)
Time of concentration = 5.92 min.
Rainfall intensity = 8.272(In/Hr)

Process from Point/Station 94.000 to Point/Station 94.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 12.00 min. Rain intensity = 5.24(In/Hr)
 Total area = 12.670(Ac.) Total runoff = 37.580(CFS)

 Process from Point/Station 94.000 to Point/Station 81.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.500(Ft.)
 Downstream point/station elevation = 655.770(Ft.)
 Pipe length = 73.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 37.580(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 37.580(CFS)
 Normal flow depth in pipe = 11.09(In.)
 Flow top width inside pipe = 13.17(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 38.63(Ft/s)
 Travel time through pipe = 0.03 min.
 Time of concentration (TC) = 12.03 min.

 Process from Point/Station 81.000 to Point/Station 81.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4
 Stream flow area = 12.670(Ac.)
 Runoff from this stream = 37.580(CFS)
 Time of concentration = 12.03 min.
 Rainfall intensity = 5.234(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	181.205	9.38	6.146
2	1.126	5.91	8.274
3	1.019	5.92	8.272
4	37.580	12.03	5.234

Qmax(1) =
 1.000 * 1.000 * 181.205) +
 0.743 * 1.000 * 1.126) +
 0.743 * 1.000 * 1.019) +
 1.000 * 0.780 * 37.580) + = 212.094

Qmax(2) =
 1.000 * 0.631 * 181.205) +
 1.000 * 1.000 * 1.126) +
 1.000 * 1.000 * 1.019) +
 1.000 * 0.492 * 37.580) + = 134.894

Qmax(3) =
 1.000 * 0.631 * 181.205) +
 1.000 * 1.000 * 1.126) +
 1.000 * 1.000 * 1.019) +
 1.000 * 0.492 * 37.580) + = 134.946

Qmax(4) =
 0.852 * 1.000 * 181.205) +
 0.633 * 1.000 * 1.126) +
 0.633 * 1.000 * 1.019) +
 1.000 * 1.000 * 37.580) + = 193.252

Total of 4 streams to confluence:
 Flow rates before confluence point:
 181.205 1.126 1.019 37.580
 Maximum flow rates at confluence using above data:
 212.094 134.894 134.946 193.252
 Area of streams before confluence:
 90.722 0.226 0.202 12.670
 Results of confluence:
 Total flow rate = 212.094(CFS)
 Time of concentration = 9.379 min.
 Effective stream area after confluence = 103.820(Ac.)

 Process from Point/Station 81.000 to Point/Station 82.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 655.770(Ft.)
 Downstream point/station elevation = 637.000(Ft.)
 Pipe length = 172.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 212.094(CFS)
 Nearest computed pipe diameter = 36.00(In.)
 Calculated individual pipe flow = 212.094(CFS)
 Normal flow depth in pipe = 28.36(In.)
 Flow top width inside pipe = 29.44(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 35.50(Ft/s)
 Travel time through pipe = 0.08 min.
 Time of concentration (TC) = 9.46 min.
 End of computations, total study area = 103.820 (Ac.)

San Diego County Rational Hydrology Program
CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13

OUTFALL 4 - Las Posas Road: Node 524-543
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052OUTFALL4

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 524.000 to Point/Station 525.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 89.000(Ft.)
Highest elevation = 666.000(Ft.)
Lowest elevation = 664.000(Ft.)
Elevation difference = 2.000(Ft.) Slope = 2.247 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 80.00 (Ft)
for the top area slope value of 2.25 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.15 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (80.000^{.5})] / (2.247^{(1/3)}) = 6.15$
Rainfall intensity (I) = 8.072(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.421(CFS)
Total initial stream area = 0.087(Ac.)

Process from Point/Station 525.000 to Point/Station 526.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 659.500(Ft.)
Downstream point/station elevation = 657.000(Ft.)
Pipe length = 89.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.421(CFS)
Nearest computed pipe diameter = 6.00(In.)

Calculated individual pipe flow = 0.421(CFS)
 Normal flow depth in pipe = 2.82(In.)
 Flow top width inside pipe = 5.99(In.)
 Critical Depth = 3.97(In.)
 Pipe flow velocity = 4.66(Ft/s)
 Travel time through pipe = 0.32 min.
 Time of concentration (TC) = 6.46 min.

 Process from Point/Station 526.000 to Point/Station 526.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.46 min.
 Rainfall intensity = 7.814(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.104
 Subarea runoff = 0.390(CFS) for 0.086(Ac.)
 Total runoff = 0.811(CFS) Total area = 0.173(Ac.)

 Process from Point/Station 526.000 to Point/Station 527.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 657.000(Ft.)
 Downstream point/station elevation = 654.400(Ft.)
 Pipe length = 88.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.811(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.811(CFS)
 Normal flow depth in pipe = 4.21(In.)
 Flow top width inside pipe = 5.49(In.)
 Critical Depth = 5.36(In.)
 Pipe flow velocity = 5.50(Ft/s)
 Travel time through pipe = 0.27 min.
 Time of concentration (TC) = 6.73 min.

 Process from Point/Station 527.000 to Point/Station 527.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.73 min.
 Rainfall intensity = 7.613(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.157
 Subarea runoff = 0.381(CFS) for 0.088(Ac.)
 Total runoff = 1.192(CFS) Total area = 0.261(Ac.)

 Process from Point/Station 527.000 to Point/Station 528.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 654.400(Ft.)
 Downstream point/station elevation = 651.000(Ft.)
 Pipe length = 83.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.192(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.192(CFS)
 Normal flow depth in pipe = 3.71(In.)
 Flow top width inside pipe = 8.86(In.)
 Critical Depth = 6.03(In.)
 Pipe flow velocity = 6.94(Ft/s)
 Travel time through pipe = 0.20 min.
 Time of concentration (TC) = 6.93 min.

 Process from Point/Station 528.000 to Point/Station 528.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.93 min.
 Rainfall intensity = 7.471(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.206
 Subarea runoff = 0.350(CFS) for 0.083(Ac.)
 Total runoff = 1.542(CFS) Total area = 0.344(Ac.)

 Process from Point/Station 528.000 to Point/Station 528.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.344(Ac.)
 Runoff from this stream = 1.542(CFS)
 Time of concentration = 6.93 min.
 Rainfall intensity = 7.471(In/Hr)

 Process from Point/Station 556.000 to Point/Station 526.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 426.000(Ft.)
 Highest elevation = 737.000(Ft.)
 Lowest elevation = 677.000(Ft.)
 Elevation difference = 60.000(Ft.) Slope = 14.085 %
 Top of Initial Area Slope adjusted by User to 12.000 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 12.00 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 4.50 minutes
 (for slope value of 10.00 %)
 Calculated TC of 4.500 minutes is less than 5 minutes,
 resetting TC to 5.0 minutes for rainfall intensity calculations

Rainfall intensity (I) = 9.222(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 10.435(CFS)
 Total initial stream area = 1.886(Ac.)

 Process from Point/Station 526.000 to Point/Station 528.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

!!Warning: Water is above left or right bank elevations
 !!Warning: Water is above left or right bank elevations
 Estimated mean flow rate at midpoint of channel = 10.684(CFS)
 Depth of flow = 0.507(Ft.), Average velocity = 10.379(Ft/s)
 !!Warning: Water is above left or right bank elevations
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	0.50
2	2.00	0.00
3	4.00	0.50

 Manning's 'N' friction factor = 0.014

Sub-Channel flow = 10.684(CFS)
 ' ' flow top width = 4.000(Ft.)
 ' ' velocity = 10.379(Ft/s)
 ' ' area = 1.029(Sq.Ft)
 ' ' Froude number = 3.605

Upstream point elevation = 661.500(Ft.)
 Downstream point elevation = 651.100(Ft.)
 Flow length = 171.000(Ft.)
 Travel time = 0.27 min.
 Time of concentration = 4.77 min.
 Depth of flow = 0.507(Ft.)
 Average velocity = 10.379(Ft/s)
 Total irregular channel flow = 10.684(CFS)
 Irregular channel normal depth above invert elev. = 0.507(Ft.)
 Average velocity of channel(s) = 10.379(Ft/s)
 !!Warning: Water is above left or right bank elevations
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Rainfall intensity = 9.500(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.590 CA = 1.159
 Subarea runoff = 0.571(CFS) for 0.077(Ac.)
 Total runoff = 11.006(CFS) Total area = 1.963(Ac.)
 Depth of flow = 0.512(Ft.), Average velocity = 10.503(Ft/s)
 !!Warning: Water is above left or right bank elevations

 Process from Point/Station 528.000 to Point/Station 528.000
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 1.963(Ac.)
 Runoff from this stream = 11.006(CFS)
 Time of concentration = 4.77 min.
 Rainfall intensity = 9.500(In/Hr)

Process from Point/Station 557.000 to Point/Station 528.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Initial subarea total flow distance = 492.000(Ft.)
 Highest elevation = 737.000(Ft.)
 Lowest elevation = 655.600(Ft.)
 Elevation difference = 81.400(Ft.) Slope = 16.545 %
 Top of Initial Area Slope adjusted by User to 14.000 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 14.00 %, in a development type of
 Permanent Open Space
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 6.90 minutes
 (for slope value of 10.00 %)
 Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
 Subarea runoff = 8.115(CFS)
 Total initial stream area = 3.095(Ac.)

 Process from Point/Station 528.000 to Point/Station 528.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 3.095(Ac.)
 Runoff from this stream = 8.115(CFS)
 Time of concentration = 6.90 min.
 Rainfall intensity = 7.492(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.542	6.93	7.471
2	11.006	4.77	9.500
3	8.115	6.90	7.492
Qmax(1) =			
	1.000 *	1.000 *	1.542) +
	0.786 *	1.000 *	11.006) +
	0.997 *	1.000 *	8.115) + =
			18.290
Qmax(2) =			
	1.000 *	0.689 *	1.542) +
	1.000 *	1.000 *	11.006) +
	1.000 *	0.692 *	8.115) + =
			17.684
Qmax(3) =			
	1.000 *	0.996 *	1.542) +
	0.789 *	1.000 *	11.006) +
	1.000 *	1.000 *	8.115) + =
			18.330

Total of 3 streams to confluence:
 Flow rates before confluence point:
 1.542 11.006 8.115
 Maximum flow rates at confluence using above data:
 18.290 17.684 18.330
 Area of streams before confluence:
 0.344 1.963 3.095
 Results of confluence:
 Total flow rate = 18.330(CFS)
 Time of concentration = 6.900 min.
 Effective stream area after confluence = 5.402(Ac.)

```

*****
Process from Point/Station      528.000 to Point/Station      542.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 651.100(Ft.)
Downstream point/station elevation = 650.500(Ft.)
Pipe length = 65.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 18.330(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 18.330(CFS)
Normal flow depth in pipe = 16.90(In.)
Flow top width inside pipe = 21.91(In.)
Critical Depth = 18.51(In.)
Pipe flow velocity = 7.76(Ft/s)
Travel time through pipe = 0.14 min.
Time of concentration (TC) = 7.04 min.

*****
Process from Point/Station      542.000 to Point/Station      542.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 5.402(Ac.)
Runoff from this stream = 18.330(CFS)
Time of concentration = 7.04 min.
Rainfall intensity = 7.396(In/Hr)

*****
Process from Point/Station      538.000 to Point/Station      539.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 86.000(Ft.)
Highest elevation = 665.700(Ft.)
Lowest elevation = 663.500(Ft.)
Elevation difference = 2.200(Ft.) Slope = 2.558 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 2.56 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.24 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 90.000^0.5)]/( 2.558^(1/3))= 6.24
Rainfall intensity (I) = 7.991(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.479(CFS)
Total initial stream area = 0.100(Ac.)

*****
Process from Point/Station      539.000 to Point/Station      540.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 659.000(Ft.)
Downstream point/station elevation = 656.500(Ft.)
Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.479(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.479(CFS)

```

Normal flow depth in pipe = 3.05(In.)
Flow top width inside pipe = 6.00(In.)
Critical Depth = 4.23(In.)
Pipe flow velocity = 4.79(Ft/s)
Travel time through pipe = 0.31 min.
Time of concentration (TC) = 6.56 min.

Process from Point/Station 540.000 to Point/Station 540.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.56 min.
Rainfall intensity = 7.743(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.125
Subarea runoff = 0.492(CFS) for 0.109(Ac.)
Total runoff = 0.971(CFS) Total area = 0.209(Ac.)

Process from Point/Station 540.000 to Point/Station 541.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 656.500(Ft.)
Downstream point/station elevation = 653.500(Ft.)
Pipe length = 78.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.971(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.971(CFS)
Normal flow depth in pipe = 4.38(In.)
Flow top width inside pipe = 5.33(In.)
Critical Depth = 5.63(In.)
Pipe flow velocity = 6.33(Ft/s)
Travel time through pipe = 0.21 min.
Time of concentration (TC) = 6.76 min.

Process from Point/Station 541.000 to Point/Station 541.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.76 min.
Rainfall intensity = 7.590(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.187
Subarea runoff = 0.445(CFS) for 0.102(Ac.)
Total runoff = 1.416(CFS) Total area = 0.311(Ac.)

Process from Point/Station 541.000 to Point/Station 542.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 653.500(Ft.)

Downstream point/station elevation = 650.500(Ft.)
 Pipe length = 53.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.416(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.416(CFS)
 Normal flow depth in pipe = 3.73(In.)
 Flow top width inside pipe = 8.87(In.)
 Critical Depth = 6.57(In.)
 Pipe flow velocity = 8.18(Ft/s)
 Travel time through pipe = 0.11 min.
 Time of concentration (TC) = 6.87 min.

 Process from Point/Station 542.000 to Point/Station 542.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.87 min.
 Rainfall intensity = 7.513(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.233
 Subarea runoff = 0.333(CFS) for 0.077(Ac.)
 Total runoff = 1.749(CFS) Total area = 0.388(Ac.)

 Process from Point/Station 542.000 to Point/Station 542.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.388(Ac.)
 Runoff from this stream = 1.749(CFS)
 Time of concentration = 6.87 min.
 Rainfall intensity = 7.513(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	18.330	7.04	7.396
2	1.749	6.87	7.513

Qmax(1) =
 1.000 * 1.000 * 18.330) +
 0.984 * 1.000 * 1.749) + = 20.052
 Qmax(2) =
 1.000 * 0.976 * 18.330) +
 1.000 * 1.000 * 1.749) + = 19.636

Total of 2 streams to confluence:
 Flow rates before confluence point:
 18.330 1.749
 Maximum flow rates at confluence using above data:
 20.052 19.636
 Area of streams before confluence:
 5.402 0.388
 Results of confluence:
 Total flow rate = 20.052(CFS)
 Time of concentration = 7.040 min.
 Effective stream area after confluence = 5.790(Ac.)

Process from Point/Station 542.000 to Point/Station 543.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 650.500(Ft.)
Downstream point/station elevation = 630.000(Ft.)
Pipe length = 66.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 20.052(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 20.052(CFS)
Normal flow depth in pipe = 8.00(In.)
Flow top width inside pipe = 14.97(In.)
Critical depth could not be calculated.
Pipe flow velocity = 30.13(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 7.08 min.
End of computations, total study area = 5.790 (Ac.)

San Diego County Rational Hydrology Program
CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13

OUTFALL 5 - Las Posas Road: Node 528-552
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052OUTFALL5

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 528.000 to Point/Station 529.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 86.000(Ft.)
Highest elevation = 655.600(Ft.)
Lowest elevation = 652.100(Ft.)
Elevation difference = 3.500(Ft.) Slope = 4.070 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 4.07 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 5.70 minutes
(for slope value of 5.00 %)
Rainfall intensity (I) = 8.474(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.422(CFS)
Total initial stream area = 0.083(Ac.)

Process from Point/Station 529.000 to Point/Station 530.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 647.600(Ft.)
Downstream point/station elevation = 644.000(Ft.)
Pipe length = 89.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.422(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.422(CFS)

Normal flow depth in pipe = 2.54(In.)
 Flow top width inside pipe = 5.93(In.)
 Critical Depth = 3.97(In.)
 Pipe flow velocity = 5.33(Ft/s)
 Travel time through pipe = 0.28 min.
 Time of concentration (TC) = 5.98 min.

 Process from Point/Station 530.000 to Point/Station 530.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 5.98 min.
 Rainfall intensity = 8.218(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.101
 Subarea runoff = 0.411(CFS) for 0.086(Ac.)
 Total runoff = 0.833(CFS) Total area = 0.169(Ac.)

 Process from Point/Station 530.000 to Point/Station 531.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 644.000(Ft.)
 Downstream point/station elevation = 640.000(Ft.)
 Pipe length = 89.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.833(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.833(CFS)
 Normal flow depth in pipe = 3.70(In.)
 Flow top width inside pipe = 5.83(In.)
 Critical Depth = 5.40(In.)
 Pipe flow velocity = 6.56(Ft/s)
 Travel time through pipe = 0.23 min.
 Time of concentration (TC) = 6.20 min.

 Process from Point/Station 531.000 to Point/Station 531.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.20 min.
 Rainfall intensity = 8.023(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.157
 Subarea runoff = 0.423(CFS) for 0.092(Ac.)
 Total runoff = 1.256(CFS) Total area = 0.261(Ac.)

 Process from Point/Station 531.000 to Point/Station 532.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 640.000(Ft.)

Downstream point/station elevation = 636.000(Ft.)
 Pipe length = 86.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.256(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.256(CFS)
 Normal flow depth in pipe = 3.69(In.)
 Flow top width inside pipe = 8.85(In.)
 Critical Depth = 6.19(In.)
 Pipe flow velocity = 7.37(Ft/s)
 Travel time through pipe = 0.19 min.
 Time of concentration (TC) = 6.40 min.

 Process from Point/Station 532.000 to Point/Station 532.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.40 min.
 Rainfall intensity = 7.865(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.209
 Subarea runoff = 0.386(CFS) for 0.087(Ac.)
 Total runoff = 1.642(CFS) Total area = 0.348(Ac.)

 Process from Point/Station 532.000 to Point/Station 533.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 636.000(Ft.)
 Downstream point/station elevation = 632.000(Ft.)
 Pipe length = 92.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.642(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.642(CFS)
 Normal flow depth in pipe = 4.37(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical Depth = 7.07(In.)
 Pipe flow velocity = 7.71(Ft/s)
 Travel time through pipe = 0.20 min.
 Time of concentration (TC) = 6.60 min.

 Process from Point/Station 533.000 to Point/Station 533.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.60 min.
 Rainfall intensity = 7.711(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.262
 Subarea runoff = 0.380(CFS) for 0.089(Ac.)
 Total runoff = 2.022(CFS) Total area = 0.437(Ac.)

```

*****
Process from Point/Station      533.000 to Point/Station      534.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 632.000(Ft.)
Downstream point/station elevation = 628.200(Ft.)
Pipe length = 89.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.022(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.022(CFS)
Normal flow depth in pipe = 4.98(In.)
Flow top width inside pipe = 8.95(In.)
Critical Depth = 7.74(In.)
Pipe flow velocity = 8.06(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 6.78 min.

*****
Process from Point/Station      534.000 to Point/Station      534.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.78 min.
Rainfall intensity = 7.576(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.316
Subarea runoff = 0.369(CFS) for 0.089(Ac.)
Total runoff = 2.391(CFS) Total area = 0.526(Ac.)

*****
Process from Point/Station      534.000 to Point/Station      535.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 628.200(Ft.)
Downstream point/station elevation = 624.300(Ft.)
Pipe length = 88.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.391(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.391(CFS)
Normal flow depth in pipe = 5.48(In.)
Flow top width inside pipe = 8.78(In.)
Critical Depth = 8.21(In.)
Pipe flow velocity = 8.49(Ft/s)
Travel time through pipe = 0.17 min.
Time of concentration (TC) = 6.95 min.

*****
Process from Point/Station      535.000 to Point/Station      535.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.95 min.
Rainfall intensity = 7.454(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area

```

(Q=KCIA) is C = 0.600 CA = 0.367
 Subarea runoff = 0.346(CFS) for 0.086(Ac.)
 Total runoff = 2.737(CFS) Total area = 0.612(Ac.)

 Process from Point/Station 535.000 to Point/Station 536.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 624.300(Ft.)
 Downstream point/station elevation = 620.300(Ft.)
 Pipe length = 48.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.737(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 2.737(CFS)
 Normal flow depth in pipe = 4.89(In.)
 Flow top width inside pipe = 8.97(In.)
 Critical Depth = 8.49(In.)
 Pipe flow velocity = 11.18(Ft/s)
 Travel time through pipe = 0.07 min.
 Time of concentration (TC) = 7.03 min.

 Process from Point/Station 536.000 to Point/Station 536.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.03 min.
 Rainfall intensity = 7.405(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.419
 Subarea runoff = 0.369(CFS) for 0.087(Ac.)
 Total runoff = 3.106(CFS) Total area = 0.699(Ac.)

 Process from Point/Station 536.000 to Point/Station 536.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.699(Ac.)
 Runoff from this stream = 3.106(CFS)
 Time of concentration = 7.03 min.
 Rainfall intensity = 7.405(In/Hr)

 Process from Point/Station 557.000 to Point/Station 536.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Initial subarea total flow distance = 648.000(Ft.)
 Highest elevation = 737.000(Ft.)
 Lowest elevation = 620.000(Ft.)
 Elevation difference = 117.000(Ft.) Slope = 18.056 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:

The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 18.06 %, in a development type of
 Permanent Open Space
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 6.90 minutes
 (for slope value of 10.00 %)
 Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
 Subarea runoff = 5.349(CFS)
 Total initial stream area = 2.040(Ac.)

 Process from Point/Station 536.000 to Point/Station 536.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Time of concentration = 6.90 min.
 Rainfall intensity = 7.492(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.350 CA = 1.027
 Subarea runoff = 2.342(CFS) for 0.893(Ac.)
 Total runoff = 7.691(CFS) Total area = 2.933(Ac.)

 Process from Point/Station 536.000 to Point/Station 536.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 2.933(Ac.)
 Runoff from this stream = 7.691(CFS)
 Time of concentration = 6.90 min.
 Rainfall intensity = 7.492(In/Hr)

 Process from Point/Station 542.000 to Point/Station 544.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 87.000(Ft.)
 Highest elevation = 650.500(Ft.)
 Lowest elevation = 647.200(Ft.)
 Elevation difference = 3.300(Ft.) Slope = 3.793 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 3.79 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 6.40 minutes
 (for slope value of 3.00 %)
 Rainfall intensity (I) = 7.864(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.486(CFS)
 Total initial stream area = 0.103(Ac.)

```

*****
Process from Point/Station      544.000 to Point/Station      545.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 647.200(Ft.)
Downstream point/station elevation = 643.700(Ft.)
Pipe length = 87.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.486(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.486(CFS)
Normal flow depth in pipe = 2.76(In.)
Flow top width inside pipe = 5.98(In.)
Critical Depth = 4.27(In.)
Pipe flow velocity = 5.52(Ft/s)
Travel time through pipe = 0.26 min.
Time of concentration (TC) = 6.66 min.

```

```

*****
Process from Point/Station      545.000 to Point/Station      545.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.66 min.
Rainfall intensity = 7.663(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.125
Subarea runoff = 0.470(CFS) for 0.105(Ac.)
Total runoff = 0.956(CFS) Total area = 0.208(Ac.)

```

```

*****
Process from Point/Station      545.000 to Point/Station      546.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 643.700(Ft.)
Downstream point/station elevation = 640.300(Ft.)
Pipe length = 89.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.956(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.956(CFS)
Normal flow depth in pipe = 4.34(In.)
Flow top width inside pipe = 5.37(In.)
Critical Depth = 5.61(In.)
Pipe flow velocity = 6.29(Ft/s)
Travel time through pipe = 0.24 min.
Time of concentration (TC) = 6.90 min.

```

```

*****
Process from Point/Station      546.000 to Point/Station      546.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.90 min.
Rainfall intensity = 7.493(In/Hr) for a 100.0 year storm

```


Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.192
 Subarea runoff = 0.482(CFS) for 0.112(Ac.)
 Total runoff = 1.439(CFS) Total area = 0.320(Ac.)

 Process from Point/Station 546.000 to Point/Station 547.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 640.300(Ft.)
 Downstream point/station elevation = 637.000(Ft.)
 Pipe length = 91.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.439(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.439(CFS)
 Normal flow depth in pipe = 4.27(In.)
 Flow top width inside pipe = 8.99(In.)
 Critical Depth = 6.63(In.)
 Pipe flow velocity = 6.97(Ft/s)
 Travel time through pipe = 0.22 min.
 Time of concentration (TC) = 7.12 min.

 Process from Point/Station 547.000 to Point/Station 547.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.12 min.
 Rainfall intensity = 7.344(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.257
 Subarea runoff = 0.447(CFS) for 0.108(Ac.)
 Total runoff = 1.886(CFS) Total area = 0.428(Ac.)

 Process from Point/Station 547.000 to Point/Station 548.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 637.000(Ft.)
 Downstream point/station elevation = 633.300(Ft.)
 Pipe length = 90.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.886(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.886(CFS)
 Normal flow depth in pipe = 4.83(In.)
 Flow top width inside pipe = 8.98(In.)
 Critical Depth = 7.52(In.)
 Pipe flow velocity = 7.81(Ft/s)
 Travel time through pipe = 0.19 min.
 Time of concentration (TC) = 7.31 min.

 Process from Point/Station 548.000 to Point/Station 548.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]

```

(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      7.31 min.
Rainfall intensity =      7.219(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.318
Subarea runoff =      0.410(CFS) for      0.102(Ac.)
Total runoff =      2.296(CFS)      Total area =      0.530(Ac.)

*****
Process from Point/Station      548.000 to Point/Station      549.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 633.300(Ft.)
Downstream point/station elevation = 629.900(Ft.)
Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.296(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.296(CFS)
Normal flow depth in pipe = 5.63(In.)
Flow top width inside pipe = 8.71(In.)
Critical Depth = 8.11(In.)
Pipe flow velocity = 7.91(Ft/s)
Travel time through pipe = 0.19 min.
Time of concentration (TC) = 7.50 min.

*****
Process from Point/Station      549.000 to Point/Station      549.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      7.50 min.
Rainfall intensity =      7.101(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.382
Subarea runoff =      0.418(CFS) for      0.107(Ac.)
Total runoff =      2.714(CFS)      Total area =      0.637(Ac.)

*****
Process from Point/Station      549.000 to Point/Station      550.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 629.900(Ft.)
Downstream point/station elevation = 626.500(Ft.)
Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.714(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.714(CFS)
Normal flow depth in pipe = 6.34(In.)
Flow top width inside pipe = 8.21(In.)
Critical Depth = 8.47(In.)
Pipe flow velocity = 8.16(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 7.68 min.

*****
Process from Point/Station      550.000 to Point/Station      550.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      7.68 min.
Rainfall intensity =      6.991(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.445
Subarea runoff =      0.398(CFS) for      0.105(Ac.)
Total runoff =      3.112(CFS)      Total area =      0.742(Ac.)

*****
Process from Point/Station      550.000 to Point/Station      551.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 626.500(Ft.)
Downstream point/station elevation = 623.000(Ft.)
Pipe length = 115.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow = 3.112(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.112(CFS)
Normal flow depth in pipe = 6.01(In.)
Flow top width inside pipe = 12.00(In.)
Critical Depth = 9.07(In.)
Pipe flow velocity = 7.92(Ft/s)
Travel time through pipe = 0.24 min.
Time of concentration (TC) = 7.92 min.

*****
Process from Point/Station      551.000 to Point/Station      551.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      7.92 min.
Rainfall intensity =      6.852(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.509
Subarea runoff =      0.374(CFS) for      0.106(Ac.)
Total runoff =      3.487(CFS)      Total area =      0.848(Ac.)

*****
Process from Point/Station      551.000 to Point/Station      551.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.848(Ac.)
Runoff from this stream = 3.487(CFS)
Time of concentration = 7.92 min.
Rainfall intensity = 6.852(In/Hr)
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	3.106	7.03	7.405
2	7.691	6.90	7.492

```

3          3.487          7.92          6.852
Qmax(1) =
          1.000 *          1.000 *          3.106) +
          0.988 *          1.000 *          7.691) +
          1.000 *          0.887 *          3.487) + =          13.799
Qmax(2) =
          1.000 *          0.982 *          3.106) +
          1.000 *          1.000 *          7.691) +
          1.000 *          0.871 *          3.487) + =          13.777
Qmax(3) =
          0.925 *          1.000 *          3.106) +
          0.915 *          1.000 *          7.691) +
          1.000 *          1.000 *          3.487) + =          13.395

```

```

Total of 3 streams to confluence:
Flow rates before confluence point:
          3.106          7.691          3.487
Maximum flow rates at confluence using above data:
          13.799          13.777          13.395
Area of streams before confluence:
          0.699          2.933          0.848
Results of confluence:
Total flow rate =          13.799(CFS)
Time of concentration =          7.026 min.
Effective stream area after confluence =          4.480(Ac.)

```

```

*****
Process from Point/Station          551.000 to Point/Station          552.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =          619.000(Ft.)
Downstream point/station elevation =          618.000(Ft.)
Pipe length =          20.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow =          13.799(CFS)
Nearest computed pipe diameter =          15.00(In.)
Calculated individual pipe flow =          13.799(CFS)
Normal flow depth in pipe =          11.74(In.)
Flow top width inside pipe =          12.37(In.)
Critical depth could not be calculated.
Pipe flow velocity =          13.40(Ft/s)
Travel time through pipe =          0.02 min.
Time of concentration (TC) =          7.05 min.
End of computations, total study area =          4.480 (Ac.)

```

San Diego County Rational Hydrology Program
CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13

OUTFALL 6 - Las Posas Road: Node 536-559
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052OUTFALL6

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 536.000 to Point/Station 537.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 84.000(Ft.)
Highest elevation = 624.800(Ft.)
Lowest elevation = 621.700(Ft.)
Elevation difference = 3.100(Ft.) Slope = 3.690 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.69 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.40 minutes
(for slope value of 3.00 %)
Rainfall intensity (I) = 7.864(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.415(CFS)
Total initial stream area = 0.088(Ac.)

Process from Point/Station 537.000 to Point/Station 558.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 621.700(Ft.)
Downstream point/station elevation = 615.500(Ft.)
Pipe length = 117.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.415(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.415(CFS)

Normal flow depth in pipe = 2.34(In.)
Flow top width inside pipe = 5.85(In.)
Critical Depth = 3.93(In.)
Pipe flow velocity = 5.86(Ft/s)
Travel time through pipe = 0.33 min.
Time of concentration (TC) = 6.73 min.

Process from Point/Station 558.000 to Point/Station 558.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.73 min.
Rainfall intensity = 7.611(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.106
Subarea runoff = 0.393(CFS) for 0.089(Ac.)
Total runoff = 0.808(CFS) Total area = 0.177(Ac.)

Process from Point/Station 558.000 to Point/Station 558.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.177(Ac.)
Runoff from this stream = 0.808(CFS)
Time of concentration = 6.73 min.
Rainfall intensity = 7.611(In/Hr)

Process from Point/Station 557.000 to Point/Station 558.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 690.000(Ft.)
Highest elevation = 737.000(Ft.)
Lowest elevation = 615.500(Ft.)
Elevation difference = 121.500(Ft.) Slope = 17.609 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 17.61 %, in a development type of
Permanent Open Space
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.90 minutes
(for slope value of 10.00 %)
Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 10.814(CFS)
Total initial stream area = 4.124(Ac.)

Process from Point/Station 558.000 to Point/Station 558.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 4.124(Ac.)
Runoff from this stream = 10.814(CFS)
Time of concentration = 6.90 min.
Rainfall intensity = 7.492(In/Hr)

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	0.808	6.73	7.611
2	10.814	6.90	7.492

Qmax(1) =
1.000 * 1.000 * 0.808) +
1.000 * 0.976 * 10.814) + = 11.360

Qmax(2) =
0.984 * 1.000 * 0.808) +
1.000 * 1.000 * 10.814) + = 11.609

Total of 2 streams to confluence:

Flow rates before confluence point:

0.808 10.814

Maximum flow rates at confluence using above data:

11.360 11.609

Area of streams before confluence:

0.177 4.124

Results of confluence:

Total flow rate = 11.609(CFS)

Time of concentration = 6.900 min.

Effective stream area after confluence = 4.301(Ac.)

Process from Point/Station 558.000 to Point/Station 555.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 615.500(Ft.)
Downstream point/station elevation = 614.000(Ft.)
Pipe length = 70.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 11.609(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 11.609(CFS)
Normal flow depth in pipe = 11.68(In.)
Flow top width inside pipe = 17.18(In.)
Critical Depth = 15.57(In.)
Pipe flow velocity = 9.56(Ft/s)
Travel time through pipe = 0.12 min.
Time of concentration (TC) = 7.02 min.

Process from Point/Station 555.000 to Point/Station 555.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 4.301(Ac.)
Runoff from this stream = 11.609(CFS)
Time of concentration = 7.02 min.
Rainfall intensity = 7.408(In/Hr)

Process from Point/Station 551.000 to Point/Station 553.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000

```

[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less                    )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 86.000(Ft.)
Highest elevation = 627.500(Ft.)
Lowest elevation = 624.000(Ft.)
Elevation difference = 3.500(Ft.) Slope = 4.070 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 4.07 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.64 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*(100.000^0.5)/(4.070^(1/3))]= 5.64
Rainfall intensity (I) = 8.535(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.553(CFS)
Total initial stream area = 0.108(Ac.)

*****
Process from Point/Station 553.000 to Point/Station 554.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 619.500(Ft.)
Downstream point/station elevation = 616.500(Ft.)
Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.553(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.553(CFS)
Normal flow depth in pipe = 3.14(In.)
Flow top width inside pipe = 5.99(In.)
Critical Depth = 4.55(In.)
Pipe flow velocity = 5.32(Ft/s)
Travel time through pipe = 0.28 min.
Time of concentration (TC) = 5.92 min.

*****
Process from Point/Station 554.000 to Point/Station 554.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less                    )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.92 min.
Rainfall intensity = 8.271(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.130
Subarea runoff = 0.519(CFS) for 0.108(Ac.)
Total runoff = 1.072(CFS) Total area = 0.216(Ac.)

*****
Process from Point/Station 554.000 to Point/Station 555.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 616.500(Ft.)
Downstream point/station elevation = 614.000(Ft.)
Pipe length = 121.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.072(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.072(CFS)
Normal flow depth in pipe = 4.24(In.)

```


Flow top width inside pipe = 8.98(In.)
 Critical Depth = 5.70(In.)
 Pipe flow velocity = 5.24(Ft/s)
 Travel time through pipe = 0.38 min.
 Time of concentration (TC) = 6.30 min.

 Process from Point/Station 555.000 to Point/Station 555.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.30 min.
 Rainfall intensity = 7.941(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.193
 Subarea runoff = 0.462(CFS) for 0.106(Ac.)
 Total runoff = 1.534(CFS) Total area = 0.322(Ac.)

 Process from Point/Station 555.000 to Point/Station 555.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.322(Ac.)
 Runoff from this stream = 1.534(CFS)
 Time of concentration = 6.30 min.
 Rainfall intensity = 7.941(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	11.609	7.02	7.408
2	1.534	6.30	7.941

Qmax(1) =
 1.000 * 1.000 * 11.609) +
 0.933 * 1.000 * 1.534) + = 13.040
 Qmax(2) =
 1.000 * 0.898 * 11.609) +
 1.000 * 1.000 * 1.534) + = 11.956

Total of 2 streams to confluence:
 Flow rates before confluence point:
 11.609 1.534
 Maximum flow rates at confluence using above data:
 13.040 11.956
 Area of streams before confluence:
 4.301 0.322
 Results of confluence:
 Total flow rate = 13.040(CFS)
 Time of concentration = 7.022 min.
 Effective stream area after confluence = 4.623(Ac.)

 Process from Point/Station 555.000 to Point/Station 559.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 614.000(Ft.)
 Downstream point/station elevation = 610.000(Ft.)
 Pipe length = 32.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 13.040(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 13.040(CFS)
Normal flow depth in pipe = 8.12(In.)
Flow top width inside pipe = 14.95(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.22(Ft/s)
Travel time through pipe = 0.03 min.
Time of concentration (TC) = 7.05 min.
End of computations, total study area = 4.623 (Ac.)

San Diego County Rational Hydrology Program
CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/18/13

OUTFALL 7 - Las Posas Road: Node 400-434
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052SESTA

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 400.000 to Point/Station 401.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 100.000(Ft.)
Highest elevation = 1038.000(Ft.)
Lowest elevation = 1027.000(Ft.)
Elevation difference = 11.000(Ft.) Slope = 11.000 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 11.00 %, in a development type of
Permanent Open Space
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.07 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.3500) * (100.000^{.5})] / (11.000^{(1/3)}) = 6.07$
Rainfall intensity (I) = 8.137(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 0.208(CFS)
Total initial stream area = 0.073(Ac.)

Process from Point/Station 401.000 to Point/Station 402.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 9.193(CFS)
Depth of flow = 0.479(Ft.), Average velocity = 6.691(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :

```

Point number      'X' coordinate      'Y' coordinate
      1              0.00              5.00
      2             30.00              0.00
      3             60.00              5.00
Manning's 'N' friction factor =    0.045
-----
Sub-Channel flow =      9.193(CFS)
'      '      flow top width =      5.742(Ft.)
'      '      velocity=      6.691(Ft/s)
'      '      area =      1.374(Sq.Ft)
'      '      Froude number =      2.410

Upstream point elevation = 1027.000(Ft.)
Downstream point elevation = 857.000(Ft.)
Flow length = 604.000(Ft.)
Travel time = 1.50 min.
Time of concentration = 7.57 min.
Depth of flow = 0.479(Ft.)
Average velocity = 6.691(Ft/s)
Total irregular channel flow = 9.193(CFS)
Irregular channel normal depth above invert elev. = 0.479(Ft.)
Average velocity of channel(s) = 6.691(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Rainfall intensity = 7.054(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350 CA = 2.563
Subarea runoff = 17.872(CFS) for 7.250(Ac.)
Total runoff = 18.080(CFS) Total area = 7.323(Ac.)
Depth of flow = 0.617(Ft.), Average velocity = 7.923(Ft/s)

*****
Process from Point/Station 402.000 to Point/Station 403.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****
-----
Depth of flow = 0.874(Ft.), Average velocity = 18.944(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              1.00
      2             1.25              0.00
      3             2.50              1.00
Manning's 'N' friction factor =    0.013
-----
Sub-Channel flow =      18.080(CFS)
'      '      flow top width =      2.185(Ft.)
'      '      velocity=      18.944(Ft/s)
'      '      area =      0.954(Sq.Ft)
'      '      Froude number =      5.051

Upstream point elevation = 857.000(Ft.)
Downstream point elevation = 779.000(Ft.)
Flow length = 677.000(Ft.)
Travel time = 0.60 min.
Time of concentration = 8.17 min.
Depth of flow = 0.874(Ft.)
Average velocity = 18.944(Ft/s)
Total irregular channel flow = 18.080(CFS)
Irregular channel normal depth above invert elev. = 0.874(Ft.)
Average velocity of channel(s) = 18.944(Ft/s)

```

```

*****
Process from Point/Station      403.000 to Point/Station      404.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 774.000(Ft.)
Downstream point/station elevation = 746.000(Ft.)
Pipe length = 200.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 18.080(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 18.080(CFS)
Normal flow depth in pipe = 9.68(In.)
Flow top width inside pipe = 14.35(In.)
Critical depth could not be calculated.
Pipe flow velocity = 21.61(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 8.32 min.

*****
Process from Point/Station      404.000 to Point/Station      404.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 7.323(Ac.)
Runoff from this stream = 18.080(CFS)
Time of concentration = 8.32 min.
Rainfall intensity = 6.637(In/Hr)

*****
Process from Point/Station      405.000 to Point/Station      406.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 99.000(Ft.)
Highest elevation = 837.000(Ft.)
Lowest elevation = 809.000(Ft.)
Elevation difference = 28.000(Ft.) Slope = 28.283 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 28.28 %, in a development type of
Permanent Open Space
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.43 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.350)*( 100.000^0.5)/( 28.283^(1/3))]= 4.43
Rainfall intensity (I) = 9.969(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 0.349(CFS)
Total initial stream area = 0.100(Ac.)

*****
Process from Point/Station      406.000 to Point/Station      407.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.869(CFS)
Depth of flow = 0.139(Ft.), Average velocity = 2.996(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
1                  0.00              2.00
2                 30.00              0.00

```

```

3          60.00          2.00
Manning's 'N' friction factor = 0.045
-----
Sub-Channel flow = 0.869(CFS)
'      ' flow top width = 4.171(Ft.)
'      ' velocity= 2.997(Ft/s)
'      ' area = 0.290(Sq.Ft)
'      ' Froude number = 2.003

Upstream point elevation = 809.000(Ft.)
Downstream point elevation = 770.000(Ft.)
Flow length = 135.000(Ft.)
Travel time = 0.75 min.
Time of concentration = 5.18 min.
Depth of flow = 0.139(Ft.)
Average velocity = 2.996(Ft/s)
Total irregular channel flow = 0.869(CFS)
Irregular channel normal depth above invert elev. = 0.139(Ft.)
Average velocity of channel(s) = 2.996(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Rainfall intensity = 9.012(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350 CA = 0.146
Subarea runoff = 0.969(CFS) for 0.318(Ac.)
Total runoff = 1.318(CFS) Total area = 0.418(Ac.)
Depth of flow = 0.163(Ft.), Average velocity = 3.326(Ft/s)

*****
Process from Point/Station 407.000 to Point/Station 408.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Depth of flow = 0.394(Ft.), Average velocity = 6.794(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 1.00
2 1.25 0.00
3 2.50 1.00
Manning's 'N' friction factor = 0.013
-----
Sub-Channel flow = 1.318(CFS)
'      ' flow top width = 0.985(Ft.)
'      ' velocity= 6.794(Ft/s)
'      ' area = 0.194(Sq.Ft)
'      ' Froude number = 2.697

Upstream point elevation = 770.000(Ft.)
Downstream point elevation = 765.500(Ft.)
Flow length = 105.000(Ft.)
Travel time = 0.26 min.
Time of concentration = 5.44 min.
Depth of flow = 0.394(Ft.)
Average velocity = 6.794(Ft/s)
Total irregular channel flow = 1.318(CFS)
Irregular channel normal depth above invert elev. = 0.394(Ft.)
Average velocity of channel(s) = 6.794(Ft/s)

*****
Process from Point/Station 408.000 to Point/Station 404.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 764.500(Ft.)
 Downstream point/station elevation = 746.000(Ft.)
 Pipe length = 15.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.318(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 1.318(CFS)
 Normal flow depth in pipe = 1.87(In.)
 Flow top width inside pipe = 5.56(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 25.18(Ft/s)
 Travel time through pipe = 0.01 min.
 Time of concentration (TC) = 5.45 min.

 Process from Point/Station 404.000 to Point/Station 404.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.418(Ac.)
 Runoff from this stream = 1.318(CFS)
 Time of concentration = 5.45 min.
 Rainfall intensity = 8.724(In/Hr)

 Process from Point/Station 409.000 to Point/Station 410.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Initial subarea total flow distance = 194.000(Ft.)
 Highest elevation = 835.000(Ft.)
 Lowest elevation = 777.000(Ft.)
 Elevation difference = 58.000(Ft.) Slope = 29.897 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 29.90 %, in a development type of
 Permanent Open Space
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 4.35 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})$
 $TC = [1.8 * (1.1 - 0.3500) * (100.000^{.5})] / (29.897^{(1/3)}) = 4.35$
 Rainfall intensity (I) = 10.089(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
 Subarea runoff = 0.876(CFS)
 Total initial stream area = 0.248(Ac.)

 Process from Point/Station 410.000 to Point/Station 404.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 764.000(Ft.)
 Downstream point/station elevation = 746.000(Ft.)
 Pipe length = 63.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.876(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.876(CFS)
 Normal flow depth in pipe = 2.22(In.)
 Flow top width inside pipe = 5.79(In.)
 Critical Depth = 5.49(In.)
 Pipe flow velocity = 13.25(Ft/s)
 Travel time through pipe = 0.08 min.

Time of concentration (TC) = 4.43 min.

Process from Point/Station 404.000 to Point/Station 404.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 0.248(Ac.)
Runoff from this stream = 0.876(CFS)
Time of concentration = 4.43 min.
Rainfall intensity = 9.972(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	18.080	8.32	6.637
2	1.318	5.45	8.724
3	0.876	4.43	9.972

Qmax(1) =
1.000 * 1.000 * 18.080) +
0.761 * 1.000 * 1.318) +
0.666 * 1.000 * 0.876) + = 19.666

Qmax(2) =
1.000 * 0.655 * 18.080) +
1.000 * 1.000 * 1.318) +
0.875 * 1.000 * 0.876) + = 13.920

Qmax(3) =
1.000 * 0.532 * 18.080) +
1.000 * 0.813 * 1.318) +
1.000 * 1.000 * 0.876) + = 11.566

Total of 3 streams to confluence:

Flow rates before confluence point:

18.080 1.318 0.876

Maximum flow rates at confluence using above data:

19.666 13.920 11.566

Area of streams before confluence:

7.323 0.418 0.248

Results of confluence:

Total flow rate = 19.666(CFS)

Time of concentration = 8.325 min.

Effective stream area after confluence = 7.989(Ac.)

Process from Point/Station 404.000 to Point/Station 411.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 746.000(Ft.)
Downstream point/station elevation = 744.000(Ft.)
Pipe length = 77.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 19.666(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 19.666(CFS)
Normal flow depth in pipe = 13.83(In.)
Flow top width inside pipe = 19.92(In.)
Critical Depth = 19.08(In.)
Pipe flow velocity = 11.71(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 8.43 min.

Process from Point/Station 411.000 to Point/Station 411.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1

Stream flow area = 7.989(Ac.)
 Runoff from this stream = 19.666(CFS)
 Time of concentration = 8.43 min.
 Rainfall intensity = 6.582(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 412.000 to Point/Station 413.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 255.000(Ft.)
 Highest elevation = 853.000(Ft.)
 Lowest elevation = 847.000(Ft.)
 Elevation difference = 6.000(Ft.) Slope = 2.353 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 80.00 (Ft)
 for the top area slope value of 2.35 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.05 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (80.000^{.5})] / (2.353^{(1/3)}) = 6.05$
 Rainfall intensity (I) = 8.153(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.653(CFS)
 Total initial stream area = 0.338(Ac.)

 Process from Point/Station 413.000 to Point/Station 414.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 3.351(CFS)
 Depth of flow = 0.151(Ft.), Average velocity = 7.181(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	0.50
2	20.00	0.00
3	20.50	0.50

 Manning's 'N' friction factor = 0.013

Sub-Channel flow = 3.351(CFS)

'	'	flow top width =	6.186(Ft.)
'	'	velocity =	7.181(Ft/s)
'	'	area =	0.467(Sq.Ft)
'	'	Froude number =	4.607

Upstream point elevation = 847.000(Ft.)
 Downstream point elevation = 759.000(Ft.)
 Flow length = 701.000(Ft.)
 Travel time = 1.63 min.
 Time of concentration = 7.68 min.
 Depth of flow = 0.151(Ft.)
 Average velocity = 7.181(Ft/s)
 Total irregular channel flow = 3.351(CFS)
 Irregular channel normal depth above invert elev. = 0.151(Ft.)
 Average velocity of channel(s) = 7.181(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000

```

Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity =      6.992(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.714
Subarea runoff =      3.339(CFS) for      0.852(Ac.)
Total runoff =      4.992(CFS)      Total area =      1.190(Ac.)
Depth of flow =      0.175(Ft.), Average velocity =      7.933(Ft/s)

*****
Process from Point/Station      414.000 to Point/Station      414.000
**** CONFLUENCE OF MINOR STREAMS ****

-----
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      1.190(Ac.)
Runoff from this stream =      4.992(CFS)
Time of concentration =      7.68 min.
Rainfall intensity =      6.992(In/Hr)

*****
Process from Point/Station      415.000 to Point/Station      416.000
**** INITIAL AREA EVALUATION ****

-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 225.000(Ft.)
Highest elevation = 853.000(Ft.)
Lowest elevation = 847.200(Ft.)
Elevation difference = 5.800(Ft.) Slope = 2.578 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 2.58 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.23 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))]
TC = [1.8*(1.1-0.6000)*( 90.000^0.5)/( 2.578^(1/3))]= 6.23
Rainfall intensity (I) =      8.005(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff =      1.374(CFS)
Total initial stream area =      0.286(Ac.)

*****
Process from Point/Station      416.000 to Point/Station      417.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel =      2.602(CFS)
Depth of flow =      0.138(Ft.), Average velocity =      6.641(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              0.50
      2             20.00              0.00
      3             20.50              0.50
Manning's 'N' friction factor = 0.013

-----
Sub-Channel flow =      2.602(CFS)

```

```

'      '      flow top width =      5.668(Ft.)
'      '      velocity=      6.641(Ft/s)
'      '      area =      0.392(Sq.Ft)
'      '      Froude number =      4.452

Upstream point elevation = 847.200(Ft.)
Downstream point elevation = 759.000(Ft.)
Flow length = 731.000(Ft.)
Travel time = 1.83 min.
Time of concentration = 8.06 min.
Depth of flow = 0.138(Ft.)
Average velocity = 6.641(Ft/s)
Total irregular channel flow = 2.602(CFS)
Irregular channel normal depth above invert elev. = 0.138(Ft.)
Average velocity of channel(s) = 6.641(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 6.777(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.552
Subarea runoff = 2.367(CFS) for 0.634(Ac.)
Total runoff = 3.741(CFS) Total area = 0.920(Ac.)
Depth of flow = 0.158(Ft.), Average velocity = 7.272(Ft/s)

*****
Process from Point/Station 417.000 to Point/Station 414.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 755.500(Ft.)
Downstream point/station elevation = 755.000(Ft.)
Pipe length = 33.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.741(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.741(CFS)
Normal flow depth in pipe = 8.52(In.)
Flow top width inside pipe = 10.89(In.)
Critical Depth = 9.88(In.)
Pipe flow velocity = 6.27(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 8.15 min.

*****
Process from Point/Station 414.000 to Point/Station 414.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
Stream flow area = 0.920(Ac.)
Runoff from this stream = 3.741(CFS)
Time of concentration = 8.15 min.
Rainfall intensity = 6.729(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 4.992 7.68 6.992
2 3.741 8.15 6.729
Qmax(1) =
1.000 * 1.000 * 4.992) +
1.000 * 0.942 * 3.741) + = 8.517
Qmax(2) =

```

```

0.962 * 1.000 * 4.992) +
1.000 * 1.000 * 3.741) + = 8.545

Total of 2 streams to confluence:
Flow rates before confluence point:
4.992 3.741
Maximum flow rates at confluence using above data:
8.517 8.545
Area of streams before confluence:
1.190 0.920
Results of confluence:
Total flow rate = 8.545(CFS)
Time of concentration = 8.149 min.
Effective stream area after confluence = 2.110(Ac.)

*****
Process from Point/Station 414.000 to Point/Station 418.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 755.000(Ft.)
Downstream point/station elevation = 750.500(Ft.)
Pipe length = 24.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 8.545(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 8.545(CFS)
Normal flow depth in pipe = 6.38(In.)
Flow top width inside pipe = 11.98(In.)
Critical depth could not be calculated.
Pipe flow velocity = 20.14(Ft/s)
Travel time through pipe = 0.02 min.
Time of concentration (TC) = 8.17 min.

*****
Process from Point/Station 418.000 to Point/Station 419.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 8.676(CFS)
Depth of flow = 0.121(Ft.), Average velocity = 1.322(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 2.00
2 4.00 0.00
3 58.00 0.00
4 62.00 2.00
Manning's 'N' friction factor = 0.030

-----
Sub-Channel flow = 8.676(CFS)
' ' flow top width = 54.484(Ft.)
' ' velocity = 1.322(Ft/s)
' ' area = 6.561(Sq.Ft)
' ' Froude number = 0.671

Upstream point elevation = 750.500(Ft.)
Downstream point elevation = 750.200(Ft.)
Flow length = 25.000(Ft.)
Travel time = 0.32 min.
Time of concentration = 8.48 min.
Depth of flow = 0.121(Ft.)
Average velocity = 1.322(Ft/s)
Total irregular channel flow = 8.676(CFS)
Irregular channel normal depth above invert elev. = 0.121(Ft.)
Average velocity of channel(s) = 1.322(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000

```

```

[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 6.557(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 1.333
Subarea runoff = 0.196(CFS) for 0.112(Ac.)
Total runoff = 8.742(CFS) Total area = 2.222(Ac.)
Depth of flow = 0.122(Ft.), Average velocity = 1.326(Ft/s)

*****
Process from Point/Station 419.000 to Point/Station 411.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 746.200(Ft.)
Downstream point/station elevation = 744.000(Ft.)
Pipe length = 85.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 8.742(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 8.742(CFS)
Normal flow depth in pipe = 10.54(In.)
Flow top width inside pipe = 13.72(In.)
Critical Depth = 13.75(In.)
Pipe flow velocity = 9.49(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 8.63 min.

*****
Process from Point/Station 411.000 to Point/Station 411.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area = 2.222(Ac.)
Runoff from this stream = 8.742(CFS)
Time of concentration = 8.63 min.
Rainfall intensity = 6.483(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 19.666 8.43 6.582
2 8.742 8.63 6.483
Qmax(1) =
1.000 * 1.000 * 19.666) +
1.000 * 0.977 * 8.742) + = 28.206
Qmax(2) =
0.985 * 1.000 * 19.666) +
1.000 * 1.000 * 8.742) + = 28.114

Total of 2 main streams to confluence:
Flow rates before confluence point:
19.666 8.742
Maximum flow rates at confluence using above data:
28.206 28.114
Area of streams before confluence:
7.989 2.222

Results of confluence:
Total flow rate = 28.206(CFS)
Time of concentration = 8.434 min.
Effective stream area after confluence = 10.211(Ac.)

*****

```

```

Process from Point/Station      411.000 to Point/Station      420.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 744.000(Ft.)
Downstream point/station elevation = 698.500(Ft.)
Pipe length = 424.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 28.206(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 28.206(CFS)
Normal flow depth in pipe = 12.40(In.)
Flow top width inside pipe = 16.67(In.)
Critical depth could not be calculated.
Pipe flow velocity = 21.73(Ft/s)
Travel time through pipe = 0.33 min.
Time of concentration (TC) = 8.76 min.

```

```

*****
Process from Point/Station      420.000 to Point/Station      420.000
**** CONFLUENCE OF MAIN STREAMS ****

```

```

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 10.211(Ac.)
Runoff from this stream = 28.206(CFS)
Time of concentration = 8.76 min.
Rainfall intensity = 6.423(In/Hr)
Program is now starting with Main Stream No. 2

```

```

*****
Process from Point/Station      421.000 to Point/Station      422.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 52.000(Ft.)
Highest elevation = 710.800(Ft.)
Lowest elevation = 710.400(Ft.)
Elevation difference = 0.400(Ft.) Slope = 0.769 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 0.77 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.92 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 65.000^0.5)]/( 0.769^(1/3))= 7.92
Rainfall intensity (I) = 6.854(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.197(CFS)
Total initial stream area = 0.048(Ac.)

```

```

*****
Process from Point/Station      422.000 to Point/Station      423.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

Estimated mean flow rate at midpoint of channel = 0.391(CFS)
Depth of flow = 0.085(Ft.), Average velocity = 2.169(Ft/s)
***** Irregular Channel Data *****

```

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
1                0.00                0.80

```

2	20.00	0.00
3	40.00	0.80

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.391(CFS)
' ' flow top width = 4.244(Ft.)
' ' velocity= 2.169(Ft/s)
' ' area = 0.180(Sq.Ft)
' ' Froude number = 1.856

Upstream point elevation = 710.400(Ft.)
Downstream point elevation = 708.500(Ft.)
Flow length = 78.000(Ft.)
Travel time = 0.60 min.
Time of concentration = 8.52 min.
Depth of flow = 0.085(Ft.)
Average velocity = 2.169(Ft/s)
Total irregular channel flow = 0.391(CFS)
Irregular channel normal depth above invert elev. = 0.085(Ft.)
Average velocity of channel(s) = 2.169(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 6.539(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.085
Subarea runoff = 0.360(CFS) for 0.094(Ac.)
Total runoff = 0.557(CFS) Total area = 0.142(Ac.)
Depth of flow = 0.097(Ft.), Average velocity = 2.371(Ft/s)

Process from Point/Station 423.000 to Point/Station 423.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 0.142(Ac.)
Runoff from this stream = 0.557(CFS)
Time of concentration = 8.52 min.
Rainfall intensity = 6.539(In/Hr)

Process from Point/Station 424.000 to Point/Station 425.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 65.000(Ft.)
Highest elevation = 711.400(Ft.)
Lowest elevation = 710.400(Ft.)
Elevation difference = 1.000(Ft.) Slope = 1.538 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 80.00 (Ft)
for the top area slope value of 1.54 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.97 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))

```

TC = [1.8*(1.1-0.6000)*( 80.000^.5)/(( 1.538^(1/3))]= 6.97
Rainfall intensity (I) = 7.441(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.254(CFS)
Total initial stream area = 0.057(Ac.)

*****
Process from Point/Station 425.000 to Point/Station 426.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel = 0.446(CFS)
Depth of flow = 0.093(Ft.), Average velocity = 2.083(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.80
2 20.00 0.00
3 40.00 0.80
Manning's 'N' friction factor = 0.013
-----
Sub-Channel flow = 0.446(CFS)
' ' flow top width = 4.629(Ft.)
' ' velocity= 2.083(Ft/s)
' ' area = 0.214(Sq.Ft)
' ' Froude number = 1.706

Upstream point elevation = 710.400(Ft.)
Downstream point elevation = 708.500(Ft.)
Flow length = 95.000(Ft.)
Travel time = 0.76 min.
Time of concentration = 7.73 min.
Depth of flow = 0.093(Ft.)
Average velocity = 2.083(Ft/s)
Total irregular channel flow = 0.446(CFS)
Irregular channel normal depth above invert elev. = 0.093(Ft.)
Average velocity of channel(s) = 2.083(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 6.960(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.086
Subarea runoff = 0.343(CFS) for 0.086(Ac.)
Total runoff = 0.597(CFS) Total area = 0.143(Ac.)
Depth of flow = 0.103(Ft.), Average velocity = 2.240(Ft/s)

*****
Process from Point/Station 426.000 to Point/Station 423.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

-----
Upstream point/station elevation = 706.000(Ft.)
Downstream point/station elevation = 705.500(Ft.)
Pipe length = 54.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.597(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.597(CFS)
Normal flow depth in pipe = 3.82(In.)
Flow top width inside pipe = 8.90(In.)
Critical Depth = 4.20(In.)
Pipe flow velocity = 3.35(Ft/s)
Travel time through pipe = 0.27 min.
Time of concentration (TC) = 8.00 min.

```



```

*****
Process from Point/Station      423.000 to Point/Station      423.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 2 in normal stream number 2
Stream flow area =      0.143(Ac.)
Runoff from this stream =      0.597(CFS)
Time of concentration =      8.00 min.
Rainfall intensity =      6.808(In/Hr)
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.557	8.52	6.539
2	0.597	8.00	6.808

Qmax(1) =
 1.000 * 1.000 * 0.557) +
 0.960 * 1.000 * 0.597) + = 1.131
 Qmax(2) =
 1.000 * 0.939 * 0.557) +
 1.000 * 1.000 * 0.597) + = 1.121

```

Total of 2 streams to confluence:
Flow rates before confluence point:
    0.557      0.597
Maximum flow rates at confluence using above data:
    1.131      1.121
Area of streams before confluence:
    0.142      0.143
Results of confluence:
Total flow rate =      1.131(CFS)
Time of concentration =      8.519 min.
Effective stream area after confluence =      0.285(Ac.)

```

```

*****
Process from Point/Station      423.000 to Point/Station      427.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =   705.500(Ft.)
Downstream point/station elevation =   705.300(Ft.)
Pipe length =   16.00(Ft.)   Manning's N = 0.013
No. of pipes = 1   Required pipe flow =   1.131(CFS)
Nearest computed pipe diameter =   9.00(In.)
Calculated individual pipe flow =   1.131(CFS)
Normal flow depth in pipe =   5.09(In.)
Flow top width inside pipe =   8.92(In.)
Critical Depth =   5.87(In.)
Pipe flow velocity =   4.40(Ft/s)
Travel time through pipe =   0.06 min.
Time of concentration (TC) =   8.58 min.

```

```

*****
Process from Point/Station      427.000 to Point/Station      428.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

Estimated mean flow rate at midpoint of channel =   1.210(CFS)
Depth of flow =   0.057(Ft.), Average velocity =   0.966(Ft/s)
***** Irregular Channel Data *****

```

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
    1              0.00              6.50
    2              13.00              0.00
    3              35.00              0.00
    4              40.00              2.50

```

```

Manning's 'N' friction factor = 0.030
-----
Sub-Channel flow = 1.210(CFS)
' ' flow top width = 22.227(Ft.)
' ' velocity = 0.966(Ft/s)
' ' area = 1.252(Sq.Ft)
' ' Froude number = 0.717

Upstream point elevation = 705.300(Ft.)
Downstream point elevation = 705.000(Ft.)
Flow length = 17.000(Ft.)
Travel time = 0.29 min.
Time of concentration = 8.87 min.
Depth of flow = 0.057(Ft.)
Average velocity = 0.966(Ft/s)
Total irregular channel flow = 1.210(CFS)
Irregular channel normal depth above invert elev. = 0.057(Ft.)
Average velocity of channel(s) = 0.966(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 6.370(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.195
Subarea runoff = 0.111(CFS) for 0.040(Ac.)
Total runoff = 1.242(CFS) Total area = 0.325(Ac.)
Depth of flow = 0.058(Ft.), Average velocity = 0.976(Ft/s)

*****
Process from Point/Station 428.000 to Point/Station 420.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 701.000(Ft.)
Downstream point/station elevation = 698.500(Ft.)
Pipe length = 130.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.242(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.242(CFS)
Normal flow depth in pipe = 4.72(In.)
Flow top width inside pipe = 8.99(In.)
Critical Depth = 6.15(In.)
Pipe flow velocity = 5.30(Ft/s)
Travel time through pipe = 0.41 min.
Time of concentration (TC) = 9.28 min.

*****
Process from Point/Station 420.000 to Point/Station 420.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area = 0.325(Ac.)
Runoff from this stream = 1.242(CFS)
Time of concentration = 9.28 min.
Rainfall intensity = 6.187(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 28.206 8.76 6.423
2 1.242 9.28 6.187

```

```

Qmax(1) =
      1.000 *      1.000 *      28.206) +
      1.000 *      0.944 *      1.242) + =      29.378
Qmax(2) =
      0.963 *      1.000 *      28.206) +
      1.000 *      1.000 *      1.242) + =      28.413

```

```

Total of 2 main streams to confluence:
Flow rates before confluence point:
      28.206      1.242
Maximum flow rates at confluence using above data:
      29.378      28.413
Area of streams before confluence:
      10.211      0.325

```

```

Results of confluence:
Total flow rate =      29.378(CFS)
Time of concentration =      8.759 min.
Effective stream area after confluence =      10.536(Ac.)

```

```

*****
Process from Point/Station      420.000 to Point/Station      429.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      698.500(Ft.)
Downstream point/station elevation =      642.300(Ft.)
Pipe length =      365.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      29.378(CFS)
Nearest computed pipe diameter =      18.00(In.)
Calculated individual pipe flow =      29.378(CFS)
Normal flow depth in pipe =      11.23(In.)
Flow top width inside pipe =      17.44(In.)
Critical depth could not be calculated.
Pipe flow velocity =      25.33(Ft/s)
Travel time through pipe =      0.24 min.
Time of concentration (TC) =      9.00 min.

```

```

*****
Process from Point/Station      429.000 to Point/Station      430.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      642.300(Ft.)
Downstream point/station elevation =      641.300(Ft.)
Pipe length =      47.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      29.378(CFS)
Nearest computed pipe diameter =      24.00(In.)
Calculated individual pipe flow =      29.378(CFS)
Normal flow depth in pipe =      17.65(In.)
Flow top width inside pipe =      21.17(In.)
Critical Depth =      22.22(In.)
Pipe flow velocity =      11.87(Ft/s)
Travel time through pipe =      0.07 min.
Time of concentration (TC) =      9.07 min.

```

```

*****
Process from Point/Station      430.000 to Point/Station      430.000
**** CONFLUENCE OF MAIN STREAMS ****

```

```

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =      10.536(Ac.)
Runoff from this stream =      29.378(CFS)
Time of concentration =      9.07 min.
Rainfall intensity =      6.282(In/Hr)
Program is now starting with Main Stream No. 2

```

```

*****
Process from Point/Station      431.000 to Point/Station      432.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 99.000(Ft.)
Highest elevation = 765.000(Ft.)
Lowest elevation = 752.500(Ft.)
Elevation difference = 12.500(Ft.) Slope = 12.626 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 12.63 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.87 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.600)*(100.000^0.5)/(12.626^(1/3))]= 3.87
Rainfall intensity (I) = 10.887(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.261(CFS)
Total initial stream area = 0.040(Ac.)

*****
Process from Point/Station      432.000 to Point/Station      433.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 2.147(CFS)
Depth of flow = 0.134(Ft.), Average velocity = 5.875(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              0.50
      2             20.00              0.00
      3             20.50              0.50
Manning's 'N' friction factor = 0.013
-----
Sub-Channel flow = 2.147(CFS)
'      ' flow top width = 5.475(Ft.)
'      ' velocity= 5.875(Ft/s)
'      ' area = 0.365(Sq.Ft)
'      ' Froude number = 4.007

Upstream point elevation = 752.500(Ft.)
Downstream point elevation = 663.800(Ft.)
Flow length = 897.000(Ft.)
Travel time = 2.54 min.
Time of concentration = 6.41 min.
Depth of flow = 0.134(Ft.)
Average velocity = 5.875(Ft/s)
Total irregular channel flow = 2.147(CFS)
Irregular channel normal depth above invert elev. = 0.134(Ft.)
Average velocity of channel(s) = 5.875(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 7.856(In/Hr) for a 100.0 year storm

```

```

Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA = 0.506
Subarea runoff = 3.712(CFS) for 0.803(Ac.)
Total runoff = 3.974(CFS) Total area = 0.843(Ac.)
Depth of flow = 0.168(Ft.), Average velocity = 6.852(Ft/s)

*****
Process from Point/Station 433.000 to Point/Station 434.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 659.800(Ft.)
Downstream point/station elevation = 659.000(Ft.)
Pipe length = 3.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.974(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 3.974(CFS)
Normal flow depth in pipe = 4.31(In.)
Flow top width inside pipe = 8.99(In.)
Critical depth could not be calculated.
Pipe flow velocity = 18.98(Ft/s)
Travel time through pipe = 0.00 min.
Time of concentration (TC) = 6.41 min.

*****
Process from Point/Station 434.000 to Point/Station 434.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 0.843(Ac.)
Runoff from this stream = 3.974(CFS)
Time of concentration = 6.41 min.
Rainfall intensity = 7.854(In/Hr)

*****
Process from Point/Station 431.000 to Point/Station 435.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 95.000(Ft.)
Highest elevation = 765.000(Ft.)
Lowest elevation = 752.500(Ft.)
Elevation difference = 12.500(Ft.) Slope = 13.158 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 13.16 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.81 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*(100.000^0.5)/(13.158^(1/3))]= 3.81
Rainfall intensity (I) = 10.985(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.250(CFS)
Total initial stream area = 0.038(Ac.)

*****
Process from Point/Station 435.000 to Point/Station 436.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 2.611(CFS)

```

Depth of flow = 0.143(Ft.), Average velocity = 6.235(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.50
2 20.00 0.00
3 20.50 0.50
Manning's 'N' friction factor = 0.013

Sub-Channel flow = 2.611(CFS)
' ' flow top width = 5.860(Ft.)
' ' velocity = 6.235(Ft/s)
' ' area = 0.419(Sq.Ft)
' ' Froude number = 4.110

Upstream point elevation = 752.500(Ft.)
Downstream point elevation = 663.800(Ft.)
Flow length = 872.000(Ft.)
Travel time = 2.33 min.
Time of concentration = 6.14 min.
Depth of flow = 0.143(Ft.)
Average velocity = 6.235(Ft/s)
Total irregular channel flow = 2.611(CFS)
Irregular channel normal depth above invert elev. = 0.143(Ft.)
Average velocity of channel(s) = 6.235(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 8.075(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.607
Subarea runoff = 4.652(CFS) for 0.974(Ac.)
Total runoff = 4.903(CFS) Total area = 1.012(Ac.)
Depth of flow = 0.181(Ft.), Average velocity = 7.299(Ft/s)

Process from Point/Station 436.000 to Point/Station 434.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 659.800(Ft.)
Downstream point/station elevation = 659.000(Ft.)
Pipe length = 33.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 4.903(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 4.903(CFS)
Normal flow depth in pipe = 8.77(In.)
Flow top width inside pipe = 10.65(In.)
Critical Depth = 10.94(In.)
Pipe flow velocity = 7.97(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 6.21 min.

Process from Point/Station 434.000 to Point/Station 434.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
Stream flow area = 1.012(Ac.)
Runoff from this stream = 4.903(CFS)
Time of concentration = 6.21 min.
Rainfall intensity = 8.017(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	3.974	6.41	7.854
2	4.903	6.21	8.017

Qmax(1) =
 1.000 * 1.000 * 3.974) +
 0.980 * 1.000 * 4.903) + = 8.777
 Qmax(2) =
 1.000 * 0.969 * 3.974) +
 1.000 * 1.000 * 4.903) + = 8.753

Total of 2 streams to confluence:
 Flow rates before confluence point:
 3.974 4.903
 Maximum flow rates at confluence using above data:
 8.777 8.753
 Area of streams before confluence:
 0.843 1.012
 Results of confluence:
 Total flow rate = 8.777(CFS)
 Time of concentration = 6.412 min.
 Effective stream area after confluence = 1.855(Ac.)

 Process from Point/Station 434.000 to Point/Station 430.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 659.000(Ft.)
 Downstream point/station elevation = 641.300(Ft.)
 Pipe length = 65.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 8.777(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 8.777(CFS)
 Normal flow depth in pipe = 5.80(In.)
 Flow top width inside pipe = 11.99(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 23.33(Ft/s)
 Travel time through pipe = 0.05 min.
 Time of concentration (TC) = 6.46 min.

 Process from Point/Station 430.000 to Point/Station 430.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 1.855(Ac.)
 Runoff from this stream = 8.777(CFS)
 Time of concentration = 6.46 min.
 Rainfall intensity = 7.818(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	29.378	9.07	6.282
2	8.777	6.46	7.818

Qmax(1) =
 1.000 * 1.000 * 29.378) +
 0.804 * 1.000 * 8.777) + = 36.432
 Qmax(2) =
 1.000 * 0.712 * 29.378) +
 1.000 * 1.000 * 8.777) + = 29.708

Total of 2 main streams to confluence:

Flow rates before confluence point:
29.378 8.777
Maximum flow rates at confluence using above data:
36.432 29.708
Area of streams before confluence:
10.536 1.855

Results of confluence:
Total flow rate = 36.432(CFS)
Time of concentration = 9.066 min.
Effective stream area after confluence = 12.391(Ac.)
End of computations, total study area = 12.391 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/18/13

OUTFALL 8 - Las Posas Road: Node 600-648
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052WQG

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 600.000 to Point/Station 601.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 96.000(Ft.)
Highest elevation = 853.000(Ft.)
Lowest elevation = 852.000(Ft.)
Elevation difference = 1.000(Ft.) Slope = 1.042 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 1.04 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.16 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5})] / (1.042^{(1/3)}) = 7.16$
Rainfall intensity (I) = 7.317(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.847(CFS)
Total initial stream area = 0.193(Ac.)

Process from Point/Station 601.000 to Point/Station 602.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 850.000(Ft.)
Downstream point/station elevation = 849.000(Ft.)
Pipe length = 83.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.847(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.847(CFS)
Normal flow depth in pipe = 4.32(In.)

Flow top width inside pipe = 8.99(In.)
Critical Depth = 5.05(In.)
Pipe flow velocity = 4.04(Ft/s)
Travel time through pipe = 0.34 min.
Time of concentration (TC) = 7.50 min.

Process from Point/Station 602.000 to Point/Station 602.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.50 min.
Rainfall intensity = 7.100(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.376
Subarea runoff = 1.824(CFS) for 0.434(Ac.)
Total runoff = 2.671(CFS) Total area = 0.627(Ac.)

Process from Point/Station 602.000 to Point/Station 603.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 849.000(Ft.)
Downstream point/station elevation = 847.000(Ft.)
Pipe length = 151.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.671(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 2.671(CFS)
Normal flow depth in pipe = 7.05(In.)
Flow top width inside pipe = 11.81(In.)
Critical Depth = 8.41(In.)
Pipe flow velocity = 5.56(Ft/s)
Travel time through pipe = 0.45 min.
Time of concentration (TC) = 7.95 min.

Process from Point/Station 603.000 to Point/Station 603.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.95 min.
Rainfall intensity = 6.836(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.725
Subarea runoff = 2.284(CFS) for 0.581(Ac.)
Total runoff = 4.955(CFS) Total area = 1.208(Ac.)

Process from Point/Station 603.000 to Point/Station 604.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 847.000(Ft.)
Downstream point/station elevation = 841.000(Ft.)
Pipe length = 72.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 4.955(CFS)

Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 4.955(CFS)
 Normal flow depth in pipe = 5.87(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical Depth = 10.98(In.)
 Pipe flow velocity = 12.97(Ft/s)
 Travel time through pipe = 0.09 min.
 Time of concentration (TC) = 8.04 min.

 Process from Point/Station 604.000 to Point/Station 604.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Stream flow area = 1.208(Ac.)
 Runoff from this stream = 4.955(CFS)
 Time of concentration = 8.04 min.
 Rainfall intensity = 6.786(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 605.000 to Point/Station 606.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 87.000(Ft.)
 Highest elevation = 853.000(Ft.)
 Lowest elevation = 852.000(Ft.)
 Elevation difference = 1.000(Ft.) Slope = 1.149 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 65.00 (Ft)
 for the top area slope value of 1.15 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.93 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5})] / (1.149^{(1/3)}) = 6.93$
 Rainfall intensity (I) = 7.472(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.628(CFS)
 Total initial stream area = 0.140(Ac.)

 Process from Point/Station 606.000 to Point/Station 607.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 850.000(Ft.)
 Downstream point/station elevation = 848.000(Ft.)
 Pipe length = 122.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.628(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.628(CFS)
 Normal flow depth in pipe = 4.35(In.)
 Flow top width inside pipe = 5.36(In.)
 Critical Depth = 4.83(In.)
 Pipe flow velocity = 4.13(Ft/s)
 Travel time through pipe = 0.49 min.
 Time of concentration (TC) = 7.42 min.

 Process from Point/Station 607.000 to Point/Station 607.000

**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.42 min.
 Rainfall intensity = 7.148(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.243
 Subarea runoff = 1.109(CFS) for 0.265(Ac.)
 Total runoff = 1.737(CFS) Total area = 0.405(Ac.)

 Process from Point/Station 607.000 to Point/Station 608.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 848.000(Ft.)
 Downstream point/station elevation = 847.000(Ft.)
 Pipe length = 25.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.737(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.737(CFS)
 Normal flow depth in pipe = 4.63(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical Depth = 7.26(In.)
 Pipe flow velocity = 7.58(Ft/s)
 Travel time through pipe = 0.05 min.
 Time of concentration (TC) = 7.48 min.

 Process from Point/Station 608.000 to Point/Station 608.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 0.405(Ac.)
 Runoff from this stream = 1.737(CFS)
 Time of concentration = 7.48 min.
 Rainfall intensity = 7.114(In/Hr)

 Process from Point/Station 609.000 to Point/Station 610.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 114.000(Ft.)
 Highest elevation = 853.000(Ft.)
 Lowest elevation = 852.000(Ft.)
 Elevation difference = 1.000(Ft.) Slope = 0.877 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 65.00 (Ft)
 for the top area slope value of 0.88 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 7.58 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5})] / (0.877^{(1/3)}) = 7.58$
 Rainfall intensity (I) = 7.051(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600

Subarea runoff = 1.134(CFS)
 Total initial stream area = 0.268(Ac.)

 Process from Point/Station 610.000 to Point/Station 608.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 850.000(Ft.)
 Downstream point/station elevation = 847.000(Ft.)
 Pipe length = 100.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.134(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.134(CFS)
 Normal flow depth in pipe = 3.93(In.)
 Flow top width inside pipe = 8.93(In.)
 Critical Depth = 5.87(In.)
 Pipe flow velocity = 6.11(Ft/s)
 Travel time through pipe = 0.27 min.
 Time of concentration (TC) = 7.85 min.

 Process from Point/Station 608.000 to Point/Station 608.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.85 min.
 Rainfall intensity = 6.892(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.327
 Subarea runoff = 1.120(CFS) for 0.277(Ac.)
 Total runoff = 2.254(CFS) Total area = 0.545(Ac.)

 Process from Point/Station 608.000 to Point/Station 608.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.545(Ac.)
 Runoff from this stream = 2.254(CFS)
 Time of concentration = 7.85 min.
 Rainfall intensity = 6.892(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.737	7.48	7.114
2	2.254	7.85	6.892

Qmax(1) =
 1.000 * 1.000 * 1.737) +
 1.000 * 0.952 * 2.254) + = 3.882

Qmax(2) =
 0.969 * 1.000 * 1.737) +
 1.000 * 1.000 * 2.254) + = 3.936

Total of 2 streams to confluence:
 Flow rates before confluence point:
 1.737 2.254
 Maximum flow rates at confluence using above data:
 3.882 3.936
 Area of streams before confluence:
 0.405 0.545

Results of confluence:

Total flow rate = 3.936(CFS)
 Time of concentration = 7.853 min.
 Effective stream area after confluence = 0.950(Ac.)

 Process from Point/Station 608.000 to Point/Station 604.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 847.000(Ft.)
 Downstream point/station elevation = 841.000(Ft.)
 Pipe length = 65.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 3.936(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 3.936(CFS)
 Normal flow depth in pipe = 6.00(In.)
 Flow top width inside pipe = 8.49(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 12.59(Ft/s)
 Travel time through pipe = 0.09 min.
 Time of concentration (TC) = 7.94 min.

 Process from Point/Station 604.000 to Point/Station 604.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 0.950(Ac.)
 Runoff from this stream = 3.936(CFS)
 Time of concentration = 7.94 min.
 Rainfall intensity = 6.843(In/Hr)
 Program is now starting with Main Stream No. 3

 Process from Point/Station 611.000 to Point/Station 612.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 130.000(Ft.)
 Highest elevation = 853.000(Ft.)
 Lowest elevation = 852.000(Ft.)
 Elevation difference = 1.000(Ft.) Slope = 0.769 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 65.00 (Ft)
 for the top area slope value of 0.77 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 7.92 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5})] / (0.769^{(1/3)}) = 7.92$
 Rainfall intensity (I) = 6.854(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.172(CFS)
 Total initial stream area = 0.285(Ac.)

 Process from Point/Station 612.000 to Point/Station 613.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 850.000(Ft.)
 Downstream point/station elevation = 848.000(Ft.)

```

Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.172(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.172(CFS)
Normal flow depth in pipe = 4.37(In.)
Flow top width inside pipe = 9.00(In.)
Critical Depth = 5.98(In.)
Pipe flow velocity = 5.51(Ft/s)
Travel time through pipe = 0.27 min.
Time of concentration (TC) = 8.19 min.

*****
Process from Point/Station 613.000 to Point/Station 613.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.19 min.
Rainfall intensity = 6.707(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.490
Subarea runoff = 2.111(CFS) for 0.531(Ac.)
Total runoff = 3.284(CFS) Total area = 0.816(Ac.)

*****
Process from Point/Station 613.000 to Point/Station 614.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 848.000(Ft.)
Downstream point/station elevation = 847.000(Ft.)
Pipe length = 102.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.284(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.284(CFS)
Normal flow depth in pipe = 9.16(In.)
Flow top width inside pipe = 10.20(In.)
Critical Depth = 9.31(In.)
Pipe flow velocity = 5.10(Ft/s)
Travel time through pipe = 0.33 min.
Time of concentration (TC) = 8.53 min.

*****
Process from Point/Station 614.000 to Point/Station 614.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.53 min.
Rainfall intensity = 6.536(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.671
Subarea runoff = 1.105(CFS) for 0.303(Ac.)
Total runoff = 4.388(CFS) Total area = 1.119(Ac.)

*****
Process from Point/Station 614.000 to Point/Station 604.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 847.000(Ft.)
 Downstream point/station elevation = 841.000(Ft.)
 Pipe length = 20.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 4.388(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 4.388(CFS)
 Normal flow depth in pipe = 4.42(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 20.35(Ft/s)
 Travel time through pipe = 0.02 min.
 Time of concentration (TC) = 8.54 min.

++++++
 Process from Point/Station 604.000 to Point/Station 604.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 3
 Stream flow area = 1.119(Ac.)
 Runoff from this stream = 4.388(CFS)
 Time of concentration = 8.54 min.
 Rainfall intensity = 6.528(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	4.955	8.04	6.786
2	3.936	7.94	6.843
3	4.388	8.54	6.528

Qmax(1) =
 1.000 * 1.000 * 4.955) +
 0.992 * 1.000 * 3.936) +
 1.000 * 0.942 * 4.388) + = 12.991
 Qmax(2) =
 1.000 * 0.987 * 4.955) +
 1.000 * 1.000 * 3.936) +
 1.000 * 0.929 * 4.388) + = 12.905
 Qmax(3) =
 0.962 * 1.000 * 4.955) +
 0.954 * 1.000 * 3.936) +
 1.000 * 1.000 * 4.388) + = 12.910

Total of 3 main streams to confluence:

Flow rates before confluence point:

4.955 3.936 4.388

Maximum flow rates at confluence using above data:

12.991 12.905 12.910

Area of streams before confluence:

1.208 0.950 1.119

Results of confluence:

Total flow rate = 12.991(CFS)

Time of concentration = 8.045 min.

Effective stream area after confluence = 3.277(Ac.)

++++++
 Process from Point/Station 604.000 to Point/Station 615.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 841.000(Ft.)
 Downstream point/station elevation = 820.000(Ft.)
 Pipe length = 220.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 12.991(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 12.991(CFS)
 Normal flow depth in pipe = 8.81(In.)

Flow top width inside pipe = 14.77(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 17.32(Ft/s)
 Travel time through pipe = 0.21 min.
 Time of concentration (TC) = 8.26 min.

 Process from Point/Station 615.000 to Point/Station 615.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 3.277(Ac.)
 Runoff from this stream = 12.991(CFS)
 Time of concentration = 8.26 min.
 Rainfall intensity = 6.673(In/Hr)

 Process from Point/Station 616.000 to Point/Station 617.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 100.000(Ft.)
 Highest elevation = 835.000(Ft.)
 Lowest elevation = 834.000(Ft.)
 Elevation difference = 1.000(Ft.) Slope = 1.000 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 65.00 (Ft)
 for the top area slope value of 1.00 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 7.26 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5})] / (1.000^{(1/3)}) = 7.26$
 Rainfall intensity (I) = 7.253(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.249(CFS)
 Total initial stream area = 0.287(Ac.)

 Process from Point/Station 617.000 to Point/Station 618.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 832.000(Ft.)
 Downstream point/station elevation = 828.000(Ft.)
 Pipe length = 123.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.249(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.249(CFS)
 Normal flow depth in pipe = 4.06(In.)
 Flow top width inside pipe = 8.96(In.)
 Critical Depth = 6.17(In.)
 Pipe flow velocity = 6.45(Ft/s)
 Travel time through pipe = 0.32 min.
 Time of concentration (TC) = 7.57 min.

 Process from Point/Station 618.000 to Point/Station 618.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000

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Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.57 min.
Rainfall intensity = 7.055(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.423
Subarea runoff = 1.735(CFS) for 0.418(Ac.)
Total runoff = 2.984(CFS) Total area = 0.705(Ac.)

*****
Process from Point/Station 618.000 to Point/Station 615.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 828.000(Ft.)
Downstream point/station elevation = 820.000(Ft.)
Pipe length = 107.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.984(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.984(CFS)
Normal flow depth in pipe = 5.34(In.)
Flow top width inside pipe = 8.84(In.)
Critical depth could not be calculated.
Pipe flow velocity = 10.94(Ft/s)
Travel time through pipe = 0.16 min.
Time of concentration (TC) = 7.74 min.

*****
Process from Point/Station 615.000 to Point/Station 615.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.705(Ac.)
Runoff from this stream = 2.984(CFS)
Time of concentration = 7.74 min.
Rainfall intensity = 6.959(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 12.991 8.26 6.673
2 2.984 7.74 6.959
Qmax(1) =
1.000 * 1.000 * 12.991) +
0.959 * 1.000 * 2.984) + = 15.853
Qmax(2) =
1.000 * 0.937 * 12.991) +
1.000 * 1.000 * 2.984) + = 15.158

Total of 2 streams to confluence:
Flow rates before confluence point:
12.991 2.984
Maximum flow rates at confluence using above data:
15.853 15.158
Area of streams before confluence:
3.277 0.705
Results of confluence:
Total flow rate = 15.853(CFS)
Time of concentration = 8.256 min.
Effective stream area after confluence = 3.982(Ac.)

*****
Process from Point/Station 615.000 to Point/Station 619.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 820.000(Ft.)

```

Downstream point/station elevation = 810.000(Ft.)
 Pipe length = 81.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 15.853(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 15.853(CFS)
 Normal flow depth in pipe = 9.23(In.)
 Flow top width inside pipe = 14.59(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 20.00(Ft/s)
 Travel time through pipe = 0.07 min.
 Time of concentration (TC) = 8.32 min.

 Process from Point/Station 619.000 to Point/Station 619.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.32 min.
 Rainfall intensity = 6.638(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 2.704
 Subarea runoff = 2.097(CFS) for 0.525(Ac.)
 Total runoff = 17.950(CFS) Total area = 4.507(Ac.)

 Process from Point/Station 619.000 to Point/Station 620.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 810.000(Ft.)
 Downstream point/station elevation = 791.000(Ft.)
 Pipe length = 140.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 17.950(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 17.950(CFS)
 Normal flow depth in pipe = 9.73(In.)
 Flow top width inside pipe = 14.32(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 21.30(Ft/s)
 Travel time through pipe = 0.11 min.
 Time of concentration (TC) = 8.43 min.

 Process from Point/Station 620.000 to Point/Station 620.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.43 min.
 Rainfall intensity = 6.582(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 2.937
 Subarea runoff = 1.382(CFS) for 0.388(Ac.)
 Total runoff = 19.332(CFS) Total area = 4.895(Ac.)

 Process from Point/Station 620.000 to Point/Station 621.000

**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 791.000(Ft.)
 Downstream point/station elevation = 766.000(Ft.)
 Pipe length = 206.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 19.332(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 19.332(CFS)
 Normal flow depth in pipe = 10.71(In.)
 Flow top width inside pipe = 13.56(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 20.62(Ft/s)
 Travel time through pipe = 0.17 min.
 Time of concentration (TC) = 8.60 min.

 Process from Point/Station 621.000 to Point/Station 621.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.60 min.
 Rainfall intensity = 6.500(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 3.250
 Subarea runoff = 1.790(CFS) for 0.521(Ac.)
 Total runoff = 21.121(CFS) Total area = 5.416(Ac.)

 Process from Point/Station 621.000 to Point/Station 622.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 766.000(Ft.)
 Downstream point/station elevation = 737.000(Ft.)
 Pipe length = 264.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 21.121(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 21.121(CFS)
 Normal flow depth in pipe = 12.12(In.)
 Flow top width inside pipe = 11.82(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 19.89(Ft/s)
 Travel time through pipe = 0.22 min.
 Time of concentration (TC) = 8.82 min.

 Process from Point/Station 622.000 to Point/Station 622.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.82 min.
 Rainfall intensity = 6.394(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 3.428
 Subarea runoff = 0.800(CFS) for 0.298(Ac.)
 Total runoff = 21.921(CFS) Total area = 5.714(Ac.)

```

*****
Process from Point/Station      622.000 to Point/Station      623.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 737.000(Ft.)
Downstream point/station elevation = 720.000(Ft.)
Pipe length = 135.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 21.921(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 21.921(CFS)
Normal flow depth in pipe = 11.74(In.)
Flow top width inside pipe = 12.37(In.)
Critical depth could not be calculated.
Pipe flow velocity = 21.27(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 8.93 min.

*****
Process from Point/Station      623.000 to Point/Station      623.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.93 min.
Rainfall intensity = 6.345(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 3.682
Subarea runoff = 1.442(CFS) for 0.423(Ac.)
Total runoff = 23.364(CFS) Total area = 6.137(Ac.)

*****
Process from Point/Station      623.000 to Point/Station      624.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 720.000(Ft.)
Downstream point/station elevation = 702.000(Ft.)
Pipe length = 125.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 23.364(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 23.364(CFS)
Normal flow depth in pipe = 11.71(In.)
Flow top width inside pipe = 12.42(In.)
Critical depth could not be calculated.
Pipe flow velocity = 22.74(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 9.02 min.

*****
Process from Point/Station      624.000 to Point/Station      624.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 6.137(Ac.)
Runoff from this stream = 23.364(CFS)
Time of concentration = 9.02 min.
Rainfall intensity = 6.303(In/Hr)

*****
Process from Point/Station      625.000 to Point/Station      626.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000

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Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 123.000(Ft.)
Highest elevation = 714.500(Ft.)
Lowest elevation = 713.500(Ft.)
Elevation difference = 1.000(Ft.) Slope = 0.813 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 0.81 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.77 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 65.000^.5)/( 0.813^(1/3))]= 7.77
Rainfall intensity (I) = 6.937(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.687(CFS)
Total initial stream area = 0.165(Ac.)

*****
Process from Point/Station 626.000 to Point/Station 627.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 711.000(Ft.)
Downstream point/station elevation = 710.000(Ft.)
Pipe length = 87.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.687(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.687(CFS)
Normal flow depth in pipe = 3.88(In.)
Flow top width inside pipe = 8.92(In.)
Critical Depth = 4.52(In.)
Pipe flow velocity = 3.76(Ft/s)
Travel time through pipe = 0.39 min.
Time of concentration (TC) = 8.16 min.

*****
Process from Point/Station 627.000 to Point/Station 627.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.16 min.
Rainfall intensity = 6.723(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.314
Subarea runoff = 1.427(CFS) for 0.359(Ac.)
Total runoff = 2.114(CFS) Total area = 0.524(Ac.)

*****
Process from Point/Station 627.000 to Point/Station 624.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 710.000(Ft.)
Downstream point/station elevation = 702.000(Ft.)
Pipe length = 156.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.114(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.114(CFS)

```

Normal flow depth in pipe = 4.84(In.)
 Flow top width inside pipe = 8.97(In.)
 Critical Depth = 7.87(In.)
 Pipe flow velocity = 8.74(Ft/s)
 Travel time through pipe = 0.30 min.
 Time of concentration (TC) = 8.46 min.

 Process from Point/Station 624.000 to Point/Station 624.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.46 min.
 Rainfall intensity = 6.570(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.589
 Subarea runoff = 1.753(CFS) for 0.457(Ac.)
 Total runoff = 3.867(CFS) Total area = 0.981(Ac.)

 Process from Point/Station 624.000 to Point/Station 624.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 0.981(Ac.)
 Runoff from this stream = 3.867(CFS)
 Time of concentration = 8.46 min.
 Rainfall intensity = 6.570(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	23.364	9.02	6.303
2	3.867	8.46	6.570

Qmax(1) =
 1.000 * 1.000 * 23.364) +
 0.959 * 1.000 * 3.867) + = 27.074
 Qmax(2) =
 1.000 * 0.938 * 23.364) +
 1.000 * 1.000 * 3.867) + = 25.778

Total of 2 streams to confluence:

Flow rates before confluence point:

23.364 3.867

Maximum flow rates at confluence using above data:

27.074 25.778

Area of streams before confluence:

6.137 0.981

Results of confluence:

Total flow rate = 27.074(CFS)

Time of concentration = 9.019 min.

Effective stream area after confluence = 7.118(Ac.)

 Process from Point/Station 624.000 to Point/Station 628.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 702.000(Ft.)
 Downstream point/station elevation = 696.000(Ft.)
 Pipe length = 274.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 27.074(CFS)

Nearest computed pipe diameter = 24.00(In.)
 Calculated individual pipe flow = 27.074(CFS)
 Normal flow depth in pipe = 16.36(In.)
 Flow top width inside pipe = 22.36(In.)
 Critical Depth = 21.73(In.)
 Pipe flow velocity = 11.86(Ft/s)
 Travel time through pipe = 0.39 min.
 Time of concentration (TC) = 9.40 min.

 Process from Point/Station 628.000 to Point/Station 628.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 9.40 min.
 Rainfall intensity = 6.136(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 4.585
 Subarea runoff = 1.059(CFS) for 0.524(Ac.)
 Total runoff = 28.133(CFS) Total area = 7.642(Ac.)

 Process from Point/Station 628.000 to Point/Station 629.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 696.000(Ft.)
 Downstream point/station elevation = 692.000(Ft.)
 Pipe length = 168.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 28.133(CFS)
 Nearest computed pipe diameter = 24.00(In.)
 Calculated individual pipe flow = 28.133(CFS)
 Normal flow depth in pipe = 16.34(In.)
 Flow top width inside pipe = 22.38(In.)
 Critical Depth = 21.96(In.)
 Pipe flow velocity = 12.36(Ft/s)
 Travel time through pipe = 0.23 min.
 Time of concentration (TC) = 9.63 min.

 Process from Point/Station 629.000 to Point/Station 629.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 9.63 min.
 Rainfall intensity = 6.042(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 4.837
 Subarea runoff = 1.094(CFS) for 0.420(Ac.)
 Total runoff = 29.227(CFS) Total area = 8.062(Ac.)

 Process from Point/Station 629.000 to Point/Station 629.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000


```

Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN          ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Time of concentration =      9.63 min.
Rainfall intensity =      6.042(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.578  CA =      5.115
Subarea runoff =      1.679(CFS) for      0.794(Ac.)
Total runoff =      30.906(CFS)      Total area =      8.856(Ac.)

*****
Process from Point/Station      629.000 to Point/Station      630.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 692.000(Ft.)
Downstream point/station elevation = 691.000(Ft.)
Pipe length = 65.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 30.906(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 30.906(CFS)
Normal flow depth in pipe = 18.35(In.)
Flow top width inside pipe = 25.20(In.)
Critical Depth = 23.06(In.)
Pipe flow velocity = 10.75(Ft/s)
Travel time through pipe = 0.10 min.
Time of concentration (TC) = 9.73 min.

*****
Process from Point/Station      630.000 to Point/Station      630.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 8.856(Ac.)
Runoff from this stream = 30.906(CFS)
Time of concentration = 9.73 min.
Rainfall intensity = 6.002(In/Hr)
Program is now starting with Main Stream No. 2

*****
Process from Point/Station      631.000 to Point/Station      632.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 106.000(Ft.)
Highest elevation = 702.000(Ft.)
Lowest elevation = 701.000(Ft.)
Elevation difference = 1.000(Ft.) Slope = 0.943 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 0.94 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.40 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 65.000^0.5)/( 0.943^(1/3))]= 7.40
Rainfall intensity (I) = 7.162(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.584(CFS)

```

Total initial stream area = 0.136(Ac.)

Process from Point/Station 632.000 to Point/Station 633.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 699.000(Ft.)
Downstream point/station elevation = 694.000(Ft.)
Pipe length = 212.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.584(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.584(CFS)
Normal flow depth in pipe = 3.62(In.)
Flow top width inside pipe = 5.87(In.)
Critical Depth = 4.67(In.)
Pipe flow velocity = 4.72(Ft/s)
Travel time through pipe = 0.75 min.
Time of concentration (TC) = 8.15 min.

Process from Point/Station 633.000 to Point/Station 633.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.15 min.
Rainfall intensity = 6.730(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.424
Subarea runoff = 2.266(CFS) for 0.570(Ac.)
Total runoff = 2.851(CFS) Total area = 0.706(Ac.)

Process from Point/Station 633.000 to Point/Station 630.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 694.000(Ft.)
Downstream point/station elevation = 691.000(Ft.)
Pipe length = 122.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.851(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 2.851(CFS)
Normal flow depth in pipe = 6.07(In.)
Flow top width inside pipe = 12.00(In.)
Critical Depth = 8.69(In.)
Pipe flow velocity = 7.15(Ft/s)
Travel time through pipe = 0.28 min.
Time of concentration (TC) = 8.43 min.

Process from Point/Station 630.000 to Point/Station 630.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area = 0.706(Ac.)
Runoff from this stream = 2.851(CFS)
Time of concentration = 8.43 min.
Rainfall intensity = 6.582(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

```

1      30.906      9.73      6.002
2      2.851      8.43      6.582
Qmax(1) =
      1.000 *      1.000 *      30.906) +
      0.912 *      1.000 *      2.851) + =      33.506
Qmax(2) =
      1.000 *      0.867 *      30.906) +
      1.000 *      1.000 *      2.851) + =      29.635

```

```

Total of 2 main streams to confluence:
Flow rates before confluence point:
      30.906      2.851
Maximum flow rates at confluence using above data:
      33.506      29.635
Area of streams before confluence:
      8.856      0.706

```

```

Results of confluence:
Total flow rate =      33.506(CFS)
Time of concentration =      9.731 min.
Effective stream area after confluence =      9.562(Ac.)

```

```

*****
Process from Point/Station      630.000 to Point/Station      634.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      691.000(Ft.)
Downstream point/station elevation =      690.000(Ft.)
Pipe length =      78.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow =      33.506(CFS)
Nearest computed pipe diameter =      27.00(In.)
Calculated individual pipe flow =      33.506(CFS)
Normal flow depth in pipe =      21.14(In.)
Flow top width inside pipe =      22.26(In.)
Critical Depth =      23.77(In.)
Pipe flow velocity =      10.04(Ft/s)
Travel time through pipe =      0.13 min.
Time of concentration (TC) =      9.86 min.

```

```

*****
Process from Point/Station      634.000 to Point/Station      634.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      9.86 min.
Rainfall intensity =      5.951(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.580 CA =      5.880
Subarea runoff =      1.486(CFS) for      0.569(Ac.)
Total runoff =      34.991(CFS)      Total area =      10.131(Ac.)

```

```

*****
Process from Point/Station      634.000 to Point/Station      635.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      690.000(Ft.)
Downstream point/station elevation =      687.000(Ft.)
Pipe length =      138.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow =      34.991(CFS)
Nearest computed pipe diameter =      27.00(In.)

```

Calculated individual pipe flow = 34.991(CFS)
 Normal flow depth in pipe = 17.72(In.)
 Flow top width inside pipe = 25.65(In.)
 Critical Depth = 24.13(In.)
 Pipe flow velocity = 12.66(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 10.04 min.

 Process from Point/Station 635.000 to Point/Station 635.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Stream flow area = 10.131(Ac.)
 Runoff from this stream = 34.991(CFS)
 Time of concentration = 10.04 min.
 Rainfall intensity = 5.881(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 636.000 to Point/Station 637.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 96.000(Ft.)
 Highest elevation = 751.500(Ft.)
 Lowest elevation = 750.500(Ft.)
 Elevation difference = 1.000(Ft.) Slope = 1.042 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 65.00 (Ft)
 for the top area slope value of 1.04 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 7.16 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5})] / (1.042^{(1/3)}) = 7.16$
 Rainfall intensity (I) = 7.317(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.509(CFS)
 Total initial stream area = 0.116(Ac.)

 Process from Point/Station 637.000 to Point/Station 638.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 748.000(Ft.)
 Downstream point/station elevation = 736.000(Ft.)
 Pipe length = 215.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.509(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.509(CFS)
 Normal flow depth in pipe = 2.58(In.)
 Flow top width inside pipe = 5.94(In.)
 Critical Depth = 4.36(In.)
 Pipe flow velocity = 6.31(Ft/s)
 Travel time through pipe = 0.57 min.
 Time of concentration (TC) = 7.72 min.

 Process from Point/Station 638.000 to Point/Station 638.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.72 min.
 Rainfall intensity = 6.965(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.377
 Subarea runoff = 2.115(CFS) for 0.512(Ac.)
 Total runoff = 2.625(CFS) Total area = 0.628(Ac.)

 Process from Point/Station 638.000 to Point/Station 639.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 736.000(Ft.)
 Downstream point/station elevation = 726.000(Ft.)
 Pipe length = 100.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.625(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 2.625(CFS)
 Normal flow depth in pipe = 4.51(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical Depth = 8.41(In.)
 Pipe flow velocity = 11.85(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 7.87 min.

 Process from Point/Station 639.000 to Point/Station 639.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.87 min.
 Rainfall intensity = 6.885(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.669
 Subarea runoff = 1.981(CFS) for 0.487(Ac.)
 Total runoff = 4.606(CFS) Total area = 1.115(Ac.)

 Process from Point/Station 639.000 to Point/Station 640.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 726.000(Ft.)
 Downstream point/station elevation = 715.000(Ft.)
 Pipe length = 114.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 4.606(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 4.606(CFS)
 Normal flow depth in pipe = 6.66(In.)
 Flow top width inside pipe = 7.90(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 13.16(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 8.01 min.

```

*****
Process from Point/Station      640.000 to Point/Station      640.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      8.01 min.
Rainfall intensity =      6.805(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.980
Subarea runoff =      2.061(CFS) for      0.518(Ac.)
Total runoff =      6.667(CFS)      Total area =      1.633(Ac.)

*****
Process from Point/Station      640.000 to Point/Station      641.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 715.000(Ft.)
Downstream point/station elevation = 696.000(Ft.)
Pipe length = 170.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow = 6.667(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 6.667(CFS)
Normal flow depth in pipe = 6.42(In.)
Flow top width inside pipe = 11.97(In.)
Critical depth could not be calculated.
Pipe flow velocity = 15.59(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 8.19 min.

*****
Process from Point/Station      641.000 to Point/Station      641.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.19 min.
Rainfall intensity = 6.707(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA = 1.253
Subarea runoff = 1.735(CFS) for 0.455(Ac.)
Total runoff = 8.402(CFS)      Total area = 2.088(Ac.)

*****
Process from Point/Station      641.000 to Point/Station      642.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 696.000(Ft.)
Downstream point/station elevation = 688.000(Ft.)
Pipe length = 78.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow = 8.402(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 8.402(CFS)
Normal flow depth in pipe = 7.65(In.)
Flow top width inside pipe = 11.54(In.)
Critical depth could not be calculated.
Pipe flow velocity = 15.88(Ft/s)
Travel time through pipe = 0.08 min.

```

Time of concentration (TC) = 8.27 min.

Process from Point/Station 642.000 to Point/Station 642.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.27 min.
Rainfall intensity = 6.664(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 1.492
Subarea runoff = 1.542(CFS) for 0.399(Ac.)
Total runoff = 9.944(CFS) Total area = 2.487(Ac.)

Process from Point/Station 642.000 to Point/Station 642.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 2.487(Ac.)
Runoff from this stream = 9.944(CFS)
Time of concentration = 8.27 min.
Rainfall intensity = 6.664(In/Hr)

Process from Point/Station 643.000 to Point/Station 644.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 114.000(Ft.)
Highest elevation = 751.500(Ft.)
Lowest elevation = 750.500(Ft.)
Elevation difference = 1.000(Ft.) Slope = 0.877 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 0.88 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.58 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5}) / (0.877^{(1/3)})] = 7.58$
Rainfall intensity (I) = 7.051(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.673(CFS)
Total initial stream area = 0.159(Ac.)

Process from Point/Station 644.000 to Point/Station 645.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 748.500(Ft.)
Downstream point/station elevation = 741.000(Ft.)
Pipe length = 166.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.673(CFS)
Nearest computed pipe diameter = 6.00(In.)

Calculated individual pipe flow = 0.673(CFS)
 Normal flow depth in pipe = 3.22(In.)
 Flow top width inside pipe = 5.98(In.)
 Critical Depth = 4.98(In.)
 Pipe flow velocity = 6.26(Ft/s)
 Travel time through pipe = 0.44 min.
 Time of concentration (TC) = 8.02 min.

 Process from Point/Station 645.000 to Point/Station 645.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.02 min.
 Rainfall intensity = 6.798(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.377
 Subarea runoff = 1.889(CFS) for 0.469(Ac.)
 Total runoff = 2.561(CFS) Total area = 0.628(Ac.)

 Process from Point/Station 645.000 to Point/Station 646.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 741.000(Ft.)
 Downstream point/station elevation = 709.000(Ft.)
 Pipe length = 236.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.561(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 2.561(CFS)
 Normal flow depth in pipe = 4.07(In.)
 Flow top width inside pipe = 8.96(In.)
 Critical Depth = 8.36(In.)
 Pipe flow velocity = 13.19(Ft/s)
 Travel time through pipe = 0.30 min.
 Time of concentration (TC) = 8.32 min.

 Process from Point/Station 646.000 to Point/Station 646.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.32 min.
 Rainfall intensity = 6.639(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.634
 Subarea runoff = 1.649(CFS) for 0.429(Ac.)
 Total runoff = 4.211(CFS) Total area = 1.057(Ac.)

 Process from Point/Station 646.000 to Point/Station 647.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 709.000(Ft.)
 Downstream point/station elevation = 689.000(Ft.)

Pipe length = 192.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 4.211(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 4.211(CFS)
 Normal flow depth in pipe = 6.02(In.)
 Flow top width inside pipe = 8.47(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 13.39(Ft/s)
 Travel time through pipe = 0.24 min.
 Time of concentration (TC) = 8.56 min.

 Process from Point/Station 647.000 to Point/Station 647.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.56 min.
 Rainfall intensity = 6.519(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.892
 Subarea runoff = 1.606(CFS) for 0.430(Ac.)
 Total runoff = 5.816(CFS) Total area = 1.487(Ac.)

 Process from Point/Station 647.000 to Point/Station 642.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 689.000(Ft.)
 Downstream point/station elevation = 688.000(Ft.)
 Pipe length = 72.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 5.816(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 5.816(CFS)
 Normal flow depth in pipe = 9.82(In.)
 Flow top width inside pipe = 14.26(In.)
 Critical Depth = 11.71(In.)
 Pipe flow velocity = 6.83(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 8.74 min.

 Process from Point/Station 642.000 to Point/Station 642.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 1.487(Ac.)
 Runoff from this stream = 5.816(CFS)
 Time of concentration = 8.74 min.
 Rainfall intensity = 6.434(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	9.944	8.27	6.664
2	5.816	8.74	6.434
Qmax(1) =			
	1.000 *	1.000 *	9.944) +
	1.000 *	0.947 *	5.816) + = 15.453
Qmax(2) =			
	0.966 *	1.000 *	9.944) +
	1.000 *	1.000 *	5.816) + = 15.418

Total of 2 streams to confluence:
Flow rates before confluence point:
9.944 5.816
Maximum flow rates at confluence using above data:
15.453 15.418
Area of streams before confluence:
2.487 1.487
Results of confluence:
Total flow rate = 15.453(CFS)
Time of concentration = 8.274 min.
Effective stream area after confluence = 3.974(Ac.)

Process from Point/Station 642.000 to Point/Station 635.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
Downstream point/station elevation = 687.000(Ft.)
Pipe length = 104.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 15.453(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 15.453(CFS)
Normal flow depth in pipe = 17.11(In.)
Flow top width inside pipe = 16.32(In.)
Critical Depth = 17.44(In.)
Pipe flow velocity = 7.36(Ft/s)
Travel time through pipe = 0.24 min.
Time of concentration (TC) = 8.51 min.

Process from Point/Station 635.000 to Point/Station 635.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 3.974(Ac.)
Runoff from this stream = 15.453(CFS)
Time of concentration = 8.51 min.
Rainfall intensity = 6.544(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	34.991	10.04	5.881
2	15.453	8.51	6.544
Qmax(1) =			
	1.000 *	1.000 *	34.991) +
	0.899 *	1.000 *	15.453) + = 48.878
Qmax(2) =			
	1.000 *	0.847 *	34.991) +
	1.000 *	1.000 *	15.453) + = 45.102

Total of 2 main streams to confluence:
Flow rates before confluence point:
34.991 15.453
Maximum flow rates at confluence using above data:
48.878 45.102
Area of streams before confluence:
10.131 3.974

Results of confluence:
Total flow rate = 48.878(CFS)
Time of concentration = 10.042 min.
Effective stream area after confluence = 14.105(Ac.)

```

*****
Process from Point/Station      635.000 to Point/Station      648.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 687.000(Ft.)
Downstream point/station elevation = 652.000(Ft.)
Pipe length = 536.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 48.878(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 48.878(CFS)
Normal flow depth in pipe = 16.92(In.)
Flow top width inside pipe = 21.89(In.)
Critical depth could not be calculated.
Pipe flow velocity = 20.64(Ft/s)
Travel time through pipe = 0.43 min.
Time of concentration (TC) = 10.48 min.

```

```

*****
Process from Point/Station      648.000 to Point/Station      648.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Time of concentration = 10.48 min.
Rainfall intensity = 5.723(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.567 CA = 8.684
Subarea runoff = 0.825(CFS) for 1.200(Ac.)
Total runoff = 49.703(CFS) Total area = 15.305(Ac.)
End of computations, total study area = 15.305 (Ac.)

```

San Diego County Rational Hydrology Program
CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/18/13

OUTFALL 9 - Las Posas Road: 200-243
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052STEUNDET

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 200.000 to Point/Station 201.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 90.000(Ft.)
Highest elevation = 701.000(Ft.)
Lowest elevation = 698.000(Ft.)
Elevation difference = 3.000(Ft.) Slope = 3.333 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.33 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.72 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.330^{(1/3)}) = 5.72$
Rainfall intensity (I) = 8.457(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.345(CFS)
Total initial stream area = 0.068(Ac.)

Process from Point/Station 201.000 to Point/Station 202.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 694.000(Ft.)
Downstream point/station elevation = 689.000(Ft.)
Pipe length = 106.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.345(CFS)
Nearest computed pipe diameter = 6.00(In.)

Calculated individual pipe flow = 0.345(CFS)
 Normal flow depth in pipe = 2.18(In.)
 Flow top width inside pipe = 5.77(In.)
 Critical Depth = 3.58(In.)
 Pipe flow velocity = 5.34(Ft/s)
 Travel time through pipe = 0.33 min.
 Time of concentration (TC) = 6.05 min.

 Process from Point/Station 201.000 to Point/Station 202.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.05 min.
 Rainfall intensity = 8.156(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.089
 Subarea runoff = 0.379(CFS) for 0.080(Ac.)
 Total runoff = 0.724(CFS) Total area = 0.148(Ac.)

 Process from Point/Station 202.000 to Point/Station 203.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 689.000(Ft.)
 Downstream point/station elevation = 687.000(Ft.)
 Pipe length = 106.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.724(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.724(CFS)
 Normal flow depth in pipe = 4.62(In.)
 Flow top width inside pipe = 5.05(In.)
 Critical Depth = 5.13(In.)
 Pipe flow velocity = 4.46(Ft/s)
 Travel time through pipe = 0.40 min.
 Time of concentration (TC) = 6.44 min.

 Process from Point/Station 202.000 to Point/Station 203.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.44 min.
 Rainfall intensity = 7.829(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.136
 Subarea runoff = 0.337(CFS) for 0.078(Ac.)
 Total runoff = 1.062(CFS) Total area = 0.226(Ac.)

 Process from Point/Station 203.000 to Point/Station 204.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
 Downstream point/station elevation = 686.680(Ft.)
 Pipe length = 31.75(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.062(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.062(CFS)
 Normal flow depth in pipe = 5.23(In.)
 Flow top width inside pipe = 8.88(In.)
 Critical Depth = 5.67(In.)
 Pipe flow velocity = 3.99(Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 6.58 min.

 Process from Point/Station 204.000 to Point/Station 204.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.226(Ac.)
 Runoff from this stream = 1.062(CFS)
 Time of concentration = 6.58 min.
 Rainfall intensity = 7.727(In/Hr)

 Process from Point/Station 205.000 to Point/Station 206.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 90.000(Ft.)
 Highest elevation = 701.000(Ft.)
 Lowest elevation = 698.000(Ft.)
 Elevation difference = 3.000(Ft.) Slope = 3.333 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 3.33 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.72 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.330^{(1/3)}) = 5.72$
 Rainfall intensity (I) = 8.457(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.406(CFS)
 Total initial stream area = 0.080(Ac.)

 Process from Point/Station 206.000 to Point/Station 207.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 694.000(Ft.)
 Downstream point/station elevation = 688.500(Ft.)
 Pipe length = 106.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.406(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.406(CFS)
 Normal flow depth in pipe = 2.33(In.)
 Flow top width inside pipe = 5.85(In.)
 Critical Depth = 3.89(In.)
 Pipe flow velocity = 5.78(Ft/s)
 Travel time through pipe = 0.31 min.
 Time of concentration (TC) = 6.02 min.

```

*****
Process from Point/Station      206.000 to Point/Station      207.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      6.02 min.
Rainfall intensity =      8.178(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.103
Subarea runoff =      0.433(CFS) for      0.091(Ac.)
Total runoff =      0.839(CFS)      Total area =      0.171(Ac.)

```

```

*****
Process from Point/Station      207.000 to Point/Station      208.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 688.500(Ft.)
Downstream point/station elevation = 687.000(Ft.)
Pipe length = 106.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.839(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.839(CFS)
Normal flow depth in pipe = 4.10(In.)
Flow top width inside pipe = 8.96(In.)
Critical Depth = 5.03(In.)
Pipe flow velocity = 4.28(Ft/s)
Travel time through pipe = 0.41 min.
Time of concentration (TC) = 6.44 min.

```

```

*****
Process from Point/Station      207.000 to Point/Station      208.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.44 min.
Rainfall intensity = 7.835(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA = 0.152
Subarea runoff = 0.350(CFS) for 0.082(Ac.)
Total runoff = 1.189(CFS)      Total area = 0.253(Ac.)

```

```

*****
Process from Point/Station      208.000 to Point/Station      204.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 687.000(Ft.)
Downstream point/station elevation = 686.680(Ft.)
Pipe length = 5.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.189(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.189(CFS)
Normal flow depth in pipe = 4.20(In.)

```

Flow top width inside pipe = 5.50(In.)
Critical depth could not be calculated.
Pipe flow velocity = 8.10(Ft/s)
Travel time through pipe = 0.01 min.
Time of concentration (TC) = 6.45 min.

Process from Point/Station 204.000 to Point/Station 204.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.253(Ac.)
Runoff from this stream = 1.189(CFS)
Time of concentration = 6.45 min.
Rainfall intensity = 7.827(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.062	6.58	7.727
2	1.189	6.45	7.827

Qmax(1) =
1.000 * 1.000 * 1.062) +
0.987 * 1.000 * 1.189) + = 2.236

Qmax(2) =
1.000 * 0.980 * 1.062) +
1.000 * 1.000 * 1.189) + = 2.230

Total of 2 streams to confluence:
Flow rates before confluence point:
1.062 1.189
Maximum flow rates at confluence using above data:
2.236 2.230
Area of streams before confluence:
0.226 0.253
Results of confluence:
Total flow rate = 2.236(CFS)
Time of concentration = 6.577 min.
Effective stream area after confluence = 0.479(Ac.)

Process from Point/Station 204.000 to Point/Station 211.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.680(Ft.)
Downstream point/station elevation = 684.500(Ft.)
Pipe length = 95.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.236(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.236(CFS)
Normal flow depth in pipe = 6.62(In.)
Flow top width inside pipe = 7.94(In.)
Critical Depth = 8.04(In.)
Pipe flow velocity = 6.41(Ft/s)
Travel time through pipe = 0.25 min.
Time of concentration (TC) = 6.82 min.

Process from Point/Station 211.000 to Point/Station 211.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.479(Ac.)
Runoff from this stream = 2.236(CFS)
Time of concentration = 6.82 min.
Rainfall intensity = 7.545(In/Hr)


```

*****
Process from Point/Station      203.000 to Point/Station      210.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 101.000(Ft.)
Highest elevation = 693.000(Ft.)
Lowest elevation = 691.000(Ft.)
Elevation difference = 2.000(Ft.) Slope = 1.980 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 80.00 (Ft)
for the top area slope value of 1.98 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.41 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 80.000^0.5)/( 1.980^(1/3))]= 6.41
Rainfall intensity (I) = 7.856(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.401(CFS)
Total initial stream area = 0.085(Ac.)

```

```

*****
Process from Point/Station      210.000 to Point/Station      211.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 685.000(Ft.)
Downstream point/station elevation = 684.500(Ft.)
Pipe length = 36.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.401(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.401(CFS)
Normal flow depth in pipe = 3.38(In.)
Flow top width inside pipe = 5.95(In.)
Critical Depth = 3.86(In.)
Pipe flow velocity = 3.53(Ft/s)
Travel time through pipe = 0.17 min.
Time of concentration (TC) = 6.58 min.

```

```

*****
Process from Point/Station      211.000 to Point/Station      211.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.085(Ac.)
Runoff from this stream = 0.401(CFS)
Time of concentration = 6.58 min.
Rainfall intensity = 7.724(In/Hr)

```

```

*****
Process from Point/Station      208.000 to Point/Station      209.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
)
]

```

```

Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 101.000(Ft.)
Highest elevation = 693.000(Ft.)
Lowest elevation = 691.000(Ft.)
Elevation difference = 2.000(Ft.) Slope = 1.980 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 80.00 (Ft)
for the top area slope value of 1.98 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.41 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 80.000^0.5)]/( 1.980^(1/3))= 6.41
Rainfall intensity (I) = 7.856(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.372(CFS)
Total initial stream area = 0.079(Ac.)

*****
Process from Point/Station 209.000 to Point/Station 211.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.000(Ft.)
Downstream point/station elevation = 684.500(Ft.)
Pipe length = 10.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.372(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.372(CFS)
Normal flow depth in pipe = 2.24(In.)
Flow top width inside pipe = 5.81(In.)
Critical Depth = 3.72(In.)
Pipe flow velocity = 5.57(Ft/s)
Travel time through pipe = 0.03 min.
Time of concentration (TC) = 6.44 min.

*****
Process from Point/Station 211.000 to Point/Station 211.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.079(Ac.)
Runoff from this stream = 0.372(CFS)
Time of concentration = 6.44 min.
Rainfall intensity = 7.832(In/Hr)
Summary of stream data:

Stream No. Flow rate (CFS) TC (min) Rainfall Intensity (In/Hr)

1 2.236 6.82 7.545
2 0.401 6.58 7.724
3 0.372 6.44 7.832
Qmax(1) =
1.000 * 1.000 * 2.236) +
0.977 * 1.000 * 0.401) +
0.963 * 1.000 * 0.372) + = 2.986
Qmax(2) =
1.000 * 0.964 * 2.236) +
1.000 * 1.000 * 0.401) +
0.986 * 1.000 * 0.372) + = 2.924
Qmax(3) =
1.000 * 0.944 * 2.236) +
1.000 * 0.979 * 0.401) +
1.000 * 1.000 * 0.372) + = 2.875

Total of 3 streams to confluence:
Flow rates before confluence point:

```



```

*****
Process from Point/Station      219.000 to Point/Station      220.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel =      0.712(CFS)
Depth of flow =      0.102(Ft.), Average velocity =      3.342(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              0.50
      2             20.00              0.00
      3             20.50              0.50
Manning's 'N' friction factor =      0.013

-----
Sub-Channel flow =      0.712(CFS)
'      '      flow top width =      4.179(Ft.)
'      '      velocity=      3.342(Ft/s)
'      '      area =      0.213(Sq.Ft)
'      '      Froude number =      2.609

Upstream point elevation =      746.000(Ft.)
Downstream point elevation =      741.000(Ft.)
Flow length =      109.000(Ft.)
Travel time =      0.54 min.
Time of concentration =      4.52 min.
Depth of flow =      0.102(Ft.)
Average velocity =      3.342(Ft/s)
Total irregular channel flow =      0.712(CFS)
Irregular channel normal depth above invert elev. =      0.102(Ft.)
Average velocity of channel(s) =      3.342(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity =      9.839(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600      CA =      0.091
Subarea runoff =      0.436(CFS) for      0.080(Ac.)
Total runoff =      0.891(CFS)      Total area =      0.151(Ac.)
Depth of flow =      0.111(Ft.), Average velocity =      3.536(Ft/s)

*****
Process from Point/Station      220.000 to Point/Station      213.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel =      1.095(CFS)
Depth of flow =      0.101(Ft.), Average velocity =      5.267(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              0.50
      2             20.00              0.00
      3             20.50              0.50
Manning's 'N' friction factor =      0.013

-----
Sub-Channel flow =      1.095(CFS)
'      '      flow top width =      4.129(Ft.)
'      '      velocity=      5.267(Ft/s)
'      '      area =      0.208(Sq.Ft)
'      '      Froude number =      4.137

Upstream point elevation =      741.000(Ft.)
Downstream point elevation =      730.000(Ft.)

```

```

Flow length = 95.000(Ft.)
Travel time = 0.30 min.
Time of concentration = 4.82 min.
Depth of flow = 0.101(Ft.)
Average velocity = 5.267(Ft/s)
Total irregular channel flow = 1.095(CFS)
Irregular channel normal depth above invert elev. = 0.101(Ft.)
Average velocity of channel(s) = 5.267(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 9.439(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.132
Subarea runoff = 0.355(CFS) for 0.069(Ac.)
Total runoff = 1.246(CFS) Total area = 0.220(Ac.)
Depth of flow = 0.106(Ft.), Average velocity = 5.440(Ft/s)

*****
Process from Point/Station 213.000 to Point/Station 214.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel = 2.217(CFS)
Depth of flow = 0.134(Ft.), Average velocity = 6.041(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.50
2 20.00 0.00
3 20.50 0.50
Manning's 'N' friction factor = 0.013

-----
Sub-Channel flow = 2.217(CFS)
' ' flow top width = 5.486(Ft.)
' ' velocity = 6.041(Ft/s)
' ' area = 0.367(Sq.Ft)
' ' Froude number = 4.116

Upstream point elevation = 730.000(Ft.)
Downstream point elevation = 688.500(Ft.)
Flow length = 398.000(Ft.)
Travel time = 1.10 min.
Time of concentration = 5.92 min.
Depth of flow = 0.134(Ft.)
Average velocity = 6.041(Ft/s)
Total irregular channel flow = 2.217(CFS)
Irregular channel normal depth above invert elev. = 0.134(Ft.)
Average velocity of channel(s) = 6.041(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 8.269(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.379
Subarea runoff = 1.885(CFS) for 0.411(Ac.)
Total runoff = 3.131(CFS) Total area = 0.631(Ac.)
Depth of flow = 0.152(Ft.), Average velocity = 6.585(Ft/s)

```

```

*****
Process from Point/Station      214.000 to Point/Station      215.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.500(Ft.)
Downstream point/station elevation = 686.000(Ft.)
Pipe length = 25.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.131(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.131(CFS)
Normal flow depth in pipe = 6.84(In.)
Flow top width inside pipe = 11.88(In.)
Critical Depth = 9.10(In.)
Pipe flow velocity = 6.76(Ft/s)
Travel time through pipe = 0.06 min.
Time of concentration (TC) = 5.98 min.

*****
Process from Point/Station      215.000 to Point/Station      216.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 3.268(CFS)
Depth of flow = 0.158(Ft.), Average velocity = 1.163(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
1                  0.00                3.75
2                  7.50                0.00
3                 25.00                0.00
4                 38.00                6.50
Manning's 'N' friction factor = 0.030

-----
Sub-Channel flow = 3.268(CFS)
'      ' flow top width = 18.131(Ft.)
'      ' velocity = 1.163(Ft/s)
'      ' area = 2.809(Sq.Ft)
'      ' Froude number = 0.521

Upstream point elevation = 686.000(Ft.)
Downstream point elevation = 685.800(Ft.)
Flow length = 30.000(Ft.)
Travel time = 0.43 min.
Time of concentration = 6.41 min.
Depth of flow = 0.158(Ft.)
Average velocity = 1.163(Ft/s)
Total irregular channel flow = 3.268(CFS)
Irregular channel normal depth above invert elev. = 0.158(Ft.)
Average velocity of channel(s) = 1.163(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 7.855(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.422
Subarea runoff = 0.187(CFS) for 0.073(Ac.)
Total runoff = 3.318(CFS) Total area = 0.704(Ac.)
Depth of flow = 0.159(Ft.), Average velocity = 1.170(Ft/s)

*****
Process from Point/Station      216.000 to Point/Station      212.000

```

**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 684.000(Ft.)
 Downstream point/station elevation = 683.000(Ft.)
 Pipe length = 31.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 3.318(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 3.318(CFS)
 Normal flow depth in pipe = 6.13(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical Depth = 9.36(In.)
 Pipe flow velocity = 8.22(Ft/s)
 Travel time through pipe = 0.06 min.
 Time of concentration (TC) = 6.47 min.

Process from Point/Station 212.000 to Point/Station 212.000

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.704(Ac.)
 Runoff from this stream = 3.318(CFS)
 Time of concentration = 6.47 min.
 Rainfall intensity = 7.806(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.986	7.02	7.408
2	3.318	6.47	7.806

Qmax(1) =
 1.000 * 1.000 * 2.986) +
 0.949 * 1.000 * 3.318) + = 6.135

Qmax(2) =
 1.000 * 0.922 * 2.986) +
 1.000 * 1.000 * 3.318) + = 6.071

Total of 2 streams to confluence:

Flow rates before confluence point:

2.986 3.318

Maximum flow rates at confluence using above data:

6.135 6.071

Area of streams before confluence:

0.643 0.704

Results of confluence:

Total flow rate = 6.135(CFS)

Time of concentration = 7.021 min.

Effective stream area after confluence = 1.347(Ac.)

Process from Point/Station 212.000 to Point/Station 217.000

**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 683.000(Ft.)
 Downstream point/station elevation = 682.000(Ft.)
 Pipe length = 80.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 6.135(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 6.135(CFS)
 Normal flow depth in pipe = 10.62(In.)
 Flow top width inside pipe = 13.64(In.)
 Critical Depth = 12.01(In.)
 Pipe flow velocity = 6.61(Ft/s)
 Travel time through pipe = 0.20 min.
 Time of concentration (TC) = 7.22 min.

```

*****
Process from Point/Station      217.000 to Point/Station      217.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =          1.347(Ac.)
Runoff from this stream =          6.135(CFS)
Time of concentration =          7.22 min.
Rainfall intensity =          7.274(In/Hr)
Program is now starting with Main Stream No. 2

*****
Process from Point/Station      226.000 to Point/Station      227.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN          ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 100.000(Ft.)
Highest elevation = 1030.000(Ft.)
Lowest elevation = 1010.000(Ft.)
Elevation difference = 20.000(Ft.) Slope = 20.000 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 20.00 %, in a development type of
Permanent Open Space
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.97 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3)]
TC = [1.8*(1.1-0.3500)*( 100.000^.5)/( 20.000^(1/3))]= 4.97
Rainfall intensity (I) = 9.253(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 0.408(CFS)
Total initial stream area = 0.126(Ac.)

*****
Process from Point/Station      227.000 to Point/Station      228.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 5.664(CFS)
Depth of flow = 0.436(Ft.), Average velocity = 6.488(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
1                  0.00                6.00
2                  25.00                0.00
3                  55.00                6.00
Manning's 'N' friction factor = 0.045
-----
Sub-Channel flow = 5.664(CFS)
'      '      flow top width = 4.001(Ft.)
'      '      velocity= 6.488(Ft/s)
'      '      area = 0.873(Sq.Ft)
'      '      Froude number = 2.448

Upstream point elevation = 1010.000(Ft.)
Downstream point elevation = 732.000(Ft.)
Flow length = 917.000(Ft.)
Travel time = 2.36 min.
Time of concentration = 7.33 min.
Depth of flow = 0.436(Ft.)
Average velocity = 6.488(Ft/s)

```



```

Total irregular channel flow =      5.664(CFS)
Irregular channel normal depth above invert elev. =    0.436(Ft.)
Average velocity of channel(s) =    6.488(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN          ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Rainfall intensity =      7.206(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350 CA =      1.507
Subarea runoff =      10.452(CFS) for      4.180(Ac.)
Total runoff =      10.860(CFS)      Total area =      4.306(Ac.)
Depth of flow =      0.557(Ft.), Average velocity =    7.635(Ft/s)

*****
Process from Point/Station      228.000 to Point/Station      229.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation =    726.000(Ft.)
Downstream point/station elevation =    716.800(Ft.)
Pipe length =    218.00(Ft.) Manning's N = 0.013
No. of pipes = 2 Required pipe flow =    10.860(CFS)
Nearest computed pipe diameter =     12.00(In.)
Calculated individual pipe flow =     5.430(CFS)
Normal flow depth in pipe =     7.70(In.)
Flow top width inside pipe =    11.51(In.)
Critical Depth =    11.24(In.)
Pipe flow velocity =     10.21(Ft/s)
Travel time through pipe =     0.36 min.
Time of concentration (TC) =     7.69 min.

*****
Process from Point/Station      229.000 to Point/Station      229.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area =      4.306(Ac.)
Runoff from this stream =    10.860(CFS)
Time of concentration =     7.69 min.
Rainfall intensity =     6.989(In/Hr)

*****
Process from Point/Station      230.000 to Point/Station      231.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN          ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance =    97.000(Ft.)
Highest elevation =    880.000(Ft.)
Lowest elevation =    858.000(Ft.)
Elevation difference =    22.000(Ft.) Slope = 22.680 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 22.68 %, in a development type of
Permanent Open Space
In Accordance With Figure 3-3
Initial Area Time of Concentration =    4.77 minutes

```

```

TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.3500)*( 100.000^.5)/( 22.680^(1/3))]= 4.77
Rainfall intensity (I) = 9.507(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 0.223(CFS)
Total initial stream area = 0.067(Ac.)

*****
Process from Point/Station 231.000 to Point/Station 232.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel = 2.044(CFS)
Depth of flow = 0.224(Ft.), Average velocity = 3.707(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 2.00
2 17.00 0.00
3 44.00 2.00
Manning's 'N' friction factor = 0.045
-----
Sub-Channel flow = 2.044(CFS)
' ' flow top width = 4.925(Ft.)
' ' velocity= 3.707(Ft/s)
' ' area = 0.551(Sq.Ft)
' ' Froude number = 1.953

Upstream point elevation = 858.000(Ft.)
Downstream point elevation = 717.000(Ft.)
Flow length = 600.000(Ft.)
Travel time = 2.70 min.
Time of concentration = 7.47 min.
Depth of flow = 0.224(Ft.)
Average velocity = 3.707(Ft/s)
Total irregular channel flow = 2.044(CFS)
Irregular channel normal depth above invert elev. = 0.224(Ft.)
Average velocity of channel(s) = 3.707(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Rainfall intensity = 7.120(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350 CA = 0.530
Subarea runoff = 3.550(CFS) for 1.447(Ac.)
Total runoff = 3.773(CFS) Total area = 1.514(Ac.)
Depth of flow = 0.282(Ft.), Average velocity = 4.321(Ft/s)

*****
Process from Point/Station 232.000 to Point/Station 229.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

-----
Upstream point/station elevation = 717.000(Ft.)
Downstream point/station elevation = 716.800(Ft.)
Pipe length = 15.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.773(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.773(CFS)
Normal flow depth in pipe = 9.05(In.)
Flow top width inside pipe = 10.34(In.)
Critical Depth = 9.92(In.)
Pipe flow velocity = 5.94(Ft/s)
Travel time through pipe = 0.04 min.

```

Time of concentration (TC) = 7.51 min.

Process from Point/Station 229.000 to Point/Station 229.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2

Stream flow area = 1.514(Ac.)
Runoff from this stream = 3.773(CFS)
Time of concentration = 7.51 min.
Rainfall intensity = 7.094(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	10.860	7.69	6.989
2	3.773	7.51	7.094

Qmax(1) =
1.000 * 1.000 * 10.860) +
0.985 * 1.000 * 3.773) + = 14.577

Qmax(2) =
1.000 * 0.977 * 10.860) +
1.000 * 1.000 * 3.773) + = 14.384

Total of 2 streams to confluence:

Flow rates before confluence point:

10.860 3.773

Maximum flow rates at confluence using above data:

14.577 14.384

Area of streams before confluence:

4.306 1.514

Results of confluence:

Total flow rate = 14.577(CFS)

Time of concentration = 7.685 min.

Effective stream area after confluence = 5.820(Ac.)

Process from Point/Station 229.000 to Point/Station 225.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 716.800(Ft.)

Downstream point/station elevation = 715.000(Ft.)

Pipe length = 192.00(Ft.) Manning's N = 0.013

No. of pipes = 2 Required pipe flow = 14.577(CFS)

Nearest computed pipe diameter = 18.00(In.)

Calculated individual pipe flow = 7.288(CFS)

Normal flow depth in pipe = 11.27(In.)

Flow top width inside pipe = 17.42(In.)

Critical Depth = 12.54(In.)

Pipe flow velocity = 6.26(Ft/s)

Travel time through pipe = 0.51 min.

Time of concentration (TC) = 8.20 min.

Process from Point/Station 225.000 to Point/Station 225.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1

Stream flow area = 5.820(Ac.)

Runoff from this stream = 14.577(CFS)

Time of concentration = 8.20 min.

Rainfall intensity = 6.704(In/Hr)

Process from Point/Station 222.000 to Point/Station 223.000

**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 98.000(Ft.)
 Highest elevation = 750.000(Ft.)
 Lowest elevation = 746.000(Ft.)
 Elevation difference = 4.000(Ft.) Slope = 4.082 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 4.08 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.63 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (100.000^{.5})] / (4.080^{(1/3)}) = 5.63$
 Rainfall intensity (I) = 8.540(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.379(CFS)
 Total initial stream area = 0.074(Ac.)

 Process from Point/Station 223.000 to Point/Station 224.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.576(CFS)
 Depth of flow = 0.095(Ft.), Average velocity = 3.091(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	0.50
2	20.00	0.00
3	20.50	0.50

 Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.576(CFS)
 ' ' flow top width = 3.911(Ft.)
 ' ' velocity = 3.091(Ft/s)
 ' ' area = 0.187(Sq.Ft)
 ' ' Froude number = 2.494

Upstream point elevation = 746.000(Ft.)
 Downstream point elevation = 741.500(Ft.)
 Flow length = 105.000(Ft.)
 Travel time = 0.57 min.
 Time of concentration = 6.20 min.
 Depth of flow = 0.095(Ft.)
 Average velocity = 3.091(Ft/s)
 Total irregular channel flow = 0.576(CFS)
 Irregular channel normal depth above invert elev. = 0.095(Ft.)
 Average velocity of channel(s) = 3.091(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity = 8.028(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.091

Subarea runoff = 0.348(CFS) for 0.077(Ac.)
 Total runoff = 0.727(CFS) Total area = 0.151(Ac.)
 Depth of flow = 0.104(Ft.), Average velocity = 3.276(Ft/s)

 Process from Point/Station 224.000 to Point/Station 225.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 737.500(Ft.)
 Downstream point/station elevation = 715.000(Ft.)
 Pipe length = 200.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.727(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.727(CFS)
 Normal flow depth in pipe = 2.59(In.)
 Flow top width inside pipe = 5.94(In.)
 Critical Depth = 5.14(In.)
 Pipe flow velocity = 8.97(Ft/s)
 Travel time through pipe = 0.37 min.
 Time of concentration (TC) = 6.57 min.

 Process from Point/Station 225.000 to Point/Station 225.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.151(Ac.)
 Runoff from this stream = 0.727(CFS)
 Time of concentration = 6.57 min.
 Rainfall intensity = 7.732(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	14.577	8.20	6.704
2	0.727	6.57	7.732

Qmax(1) =
 1.000 * 1.000 * 14.577) +
 0.867 * 1.000 * 0.727) + = 15.207

Qmax(2) =
 1.000 * 0.802 * 14.577) +
 1.000 * 1.000 * 0.727) + = 12.412

Total of 2 streams to confluence:
 Flow rates before confluence point:
 14.577 0.727
 Maximum flow rates at confluence using above data:
 15.207 12.412
 Area of streams before confluence:
 5.820 0.151
 Results of confluence:
 Total flow rate = 15.207(CFS)
 Time of concentration = 8.196 min.
 Effective stream area after confluence = 5.971(Ac.)

 Process from Point/Station 225.000 to Point/Station 217.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 715.000(Ft.)
 Downstream point/station elevation = 682.000(Ft.)
 Pipe length = 350.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 15.207(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 15.207(CFS)
 Normal flow depth in pipe = 9.84(In.)

Flow top width inside pipe = 14.25(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 17.82(Ft/s)
 Travel time through pipe = 0.33 min.
 Time of concentration (TC) = 8.52 min.

 Process from Point/Station 217.000 to Point/Station 217.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 5.971(Ac.)
 Runoff from this stream = 15.207(CFS)
 Time of concentration = 8.52 min.
 Rainfall intensity = 6.537(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	6.135	7.22	7.274
2	15.207	8.52	6.537

Qmax(1) =
 1.000 * 1.000 * 6.135) +
 1.000 * 0.847 * 15.207) + = 19.021

Qmax(2) =
 0.899 * 1.000 * 6.135) +
 1.000 * 1.000 * 15.207) + = 20.721

Total of 2 main streams to confluence:

Flow rates before confluence point:

6.135 15.207

Maximum flow rates at confluence using above data:

19.021 20.721

Area of streams before confluence:

1.347 5.971

Results of confluence:

Total flow rate = 20.721(CFS)

Time of concentration = 8.524 min.

Effective stream area after confluence = 7.318(Ac.)

 Process from Point/Station 217.000 to Point/Station 233.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 682.000(Ft.)
 Downstream point/station elevation = 679.000(Ft.)
 Pipe length = 125.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 20.721(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 20.721(CFS)
 Normal flow depth in pipe = 14.79(In.)
 Flow top width inside pipe = 19.17(In.)
 Critical Depth = 19.38(In.)
 Pipe flow velocity = 11.44(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 8.71 min.

 Process from Point/Station 233.000 to Point/Station 233.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 7.318(Ac.)

Runoff from this stream = 20.721(CFS)
 Time of concentration = 8.71 min.
 Rainfall intensity = 6.449(In/Hr)

 Process from Point/Station 224.000 to Point/Station 234.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 100.000(Ft.)
 Highest elevation = 741.500(Ft.)
 Lowest elevation = 732.000(Ft.)
 Elevation difference = 9.500(Ft.) Slope = 9.500 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 9.50 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 4.25 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (100.000^{.5})] / (9.500^{(1/3)}) = 4.25$
 Rainfall intensity (I) = 10.242(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.430(CFS)
 Total initial stream area = 0.070(Ac.)

 Process from Point/Station 234.000 to Point/Station 235.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 1.997(CFS)
 Depth of flow = 0.132(Ft.), Average velocity = 5.630(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	0.50
2	20.00	0.00
3	20.50	0.50

 Manning's 'N' friction factor = 0.013

Sub-Channel flow = 1.997(CFS)

'	'	flow top width = 5.393(Ft.)
'	'	velocity = 5.630(Ft/s)
'	'	area = 0.355(Sq.Ft)
'	'	Froude number = 3.868

Upstream point elevation = 732.000(Ft.)
 Downstream point elevation = 688.000(Ft.)
 Flow length = 475.000(Ft.)
 Travel time = 1.41 min.
 Time of concentration = 5.66 min.
 Depth of flow = 0.132(Ft.)
 Average velocity = 5.630(Ft/s)
 Total irregular channel flow = 1.997(CFS)
 Irregular channel normal depth above invert elev. = 0.132(Ft.)
 Average velocity of channel(s) = 5.630(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000

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[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 8.517(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.407
Subarea runoff = 3.040(CFS) for 0.609(Ac.)
Total runoff = 3.470(CFS) Total area = 0.679(Ac.)
Depth of flow = 0.162(Ft.), Average velocity = 6.463(Ft/s)

*****
Process from Point/Station 235.000 to Point/Station 236.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.000(Ft.)
Downstream point/station elevation = 684.000(Ft.)
Pipe length = 71.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.470(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.470(CFS)
Normal flow depth in pipe = 8.27(In.)
Flow top width inside pipe = 11.11(In.)
Critical Depth = 9.55(In.)
Pipe flow velocity = 6.01(Ft/s)
Travel time through pipe = 0.20 min.
Time of concentration (TC) = 5.85 min.

*****
Process from Point/Station 236.000 to Point/Station 237.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 3.616(CFS)
Depth of flow = 0.130(Ft.), Average velocity = 1.616(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 3.50
2 7.50 0.00
3 24.50 0.00
4 40.00 7.50
Manning's 'N' friction factor = 0.030

-----
Sub-Channel flow = 3.616(CFS)
' ' flow top width = 17.545(Ft.)
' ' velocity = 1.616(Ft/s)
' ' area = 2.237(Sq.Ft)
' ' Froude number = 0.798

Upstream point elevation = 684.000(Ft.)
Downstream point elevation = 683.500(Ft.)
Flow length = 30.000(Ft.)
Travel time = 0.31 min.
Time of concentration = 6.16 min.
Depth of flow = 0.130(Ft.)
Average velocity = 1.616(Ft/s)
Total irregular channel flow = 3.616(CFS)
Irregular channel normal depth above invert elev. = 0.130(Ft.)
Average velocity of channel(s) = 1.616(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600

```


Rainfall intensity = 8.059(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.460
 Subarea runoff = 0.239(CFS) for 0.088(Ac.)
 Total runoff = 3.709(CFS) Total area = 0.767(Ac.)
 Depth of flow = 0.131(Ft.), Average velocity = 1.632(Ft/s)

 Process from Point/Station 237.000 to Point/Station 233.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 679.500(Ft.)
 Downstream point/station elevation = 679.000(Ft.)
 Pipe length = 40.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 3.709(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 3.709(CFS)
 Normal flow depth in pipe = 9.16(In.)
 Flow top width inside pipe = 10.20(In.)
 Critical Depth = 9.84(In.)
 Pipe flow velocity = 5.76(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 6.28 min.

 Process from Point/Station 233.000 to Point/Station 233.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.767(Ac.)
 Runoff from this stream = 3.709(CFS)
 Time of concentration = 6.28 min.
 Rainfall intensity = 7.963(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	20.721	8.71	6.449
2	3.709	6.28	7.963
Qmax(1) =			
	1.000 *	1.000 *	20.721) +
	0.810 *	1.000 *	3.709) + =
			23.724
Qmax(2) =			
	1.000 *	0.721 *	20.721) +
	1.000 *	1.000 *	3.709) + =
			18.650

Total of 2 streams to confluence:
 Flow rates before confluence point:
 20.721 3.709
 Maximum flow rates at confluence using above data:
 23.724 18.650
 Area of streams before confluence:
 7.318 0.767
 Results of confluence:
 Total flow rate = 23.724(CFS)
 Time of concentration = 8.706 min.
 Effective stream area after confluence = 8.085(Ac.)

 Process from Point/Station 233.000 to Point/Station 238.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 679.000(Ft.)
 Downstream point/station elevation = 678.000(Ft.)
 Pipe length = 47.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 23.724(CFS)

Nearest computed pipe diameter = 24.00(In.)
 Calculated individual pipe flow = 23.724(CFS)
 Normal flow depth in pipe = 15.07(In.)
 Flow top width inside pipe = 23.20(In.)
 Critical Depth = 20.72(In.)
 Pipe flow velocity = 11.43(Ft/s)
 Travel time through pipe = 0.07 min.
 Time of concentration (TC) = 8.77 min.

 Process from Point/Station 238.000 to Point/Station 238.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 8.085(Ac.)
 Runoff from this stream = 23.724(CFS)
 Time of concentration = 8.77 min.
 Rainfall intensity = 6.416(In/Hr)

 Process from Point/Station 239.000 to Point/Station 240.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Initial subarea total flow distance = 98.000(Ft.)
 Highest elevation = 740.000(Ft.)
 Lowest elevation = 723.000(Ft.)
 Elevation difference = 17.000(Ft.) Slope = 17.347 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 17.35 %, in a development type of
 Permanent Open Space
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.22 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.3500) * (100.000^{.5})] / (17.347^{(1/3)}) = 5.22$
 Rainfall intensity (I) = 8.974(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
 Subarea runoff = 0.195(CFS)
 Total initial stream area = 0.062(Ac.)

 Process from Point/Station 240.000 to Point/Station 241.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.400(CFS)
 Depth of flow = 0.232(Ft.), Average velocity = 1.819(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	5.00
2	27.00	0.00
3	45.00	6.50

 Manning's 'N' friction factor = 0.045

 Sub-Channel flow = 0.400(CFS)

'	'	flow top width = 1.897(Ft.)
'	'	velocity = 1.819(Ft/s)
'	'	area = 0.220(Sq.Ft)
'	'	Froude number = 0.941

Upstream point elevation = 723.000(Ft.)
 Downstream point elevation = 715.000(Ft.)
 Flow length = 143.000(Ft.)
 Travel time = 1.31 min.
 Time of concentration = 6.53 min.
 Depth of flow = 0.232(Ft.)
 Average velocity = 1.819(Ft/s)
 Total irregular channel flow = 0.400(CFS)
 Irregular channel normal depth above invert elev. = 0.232(Ft.)
 Average velocity of channel(s) = 1.819(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Rainfall intensity = 7.767(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.350 CA = 0.068
 Subarea runoff = 0.330(CFS) for 0.131(Ac.)
 Total runoff = 0.525(CFS) Total area = 0.193(Ac.)
 Depth of flow = 0.257(Ft.), Average velocity = 1.946(Ft/s)

 Process from Point/Station 241.000 to Point/Station 242.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 0.245(Ft.), Average velocity = 6.971(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 1.00
 2 1.25 0.00
 3 2.50 1.00
 Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.525(CFS)
 ' ' flow top width = 0.613(Ft.)
 ' ' velocity = 6.971(Ft/s)
 ' ' area = 0.075(Sq.Ft)
 ' ' Froude number = 3.507

Upstream point elevation = 715.000(Ft.)
 Downstream point elevation = 687.000(Ft.)
 Flow length = 330.000(Ft.)
 Travel time = 0.79 min.
 Time of concentration = 7.31 min.
 Depth of flow = 0.245(Ft.)
 Average velocity = 6.971(Ft/s)
 Total irregular channel flow = 0.525(CFS)
 Irregular channel normal depth above invert elev. = 0.245(Ft.)
 Average velocity of channel(s) = 6.971(Ft/s)

 Process from Point/Station 242.000 to Point/Station 238.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

 Upstream point/station elevation = 681.000(Ft.)
 Downstream point/station elevation = 678.000(Ft.)
 Pipe length = 40.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.525(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.525(CFS)
 Normal flow depth in pipe = 2.42(In.)

Flow top width inside pipe = 5.89(In.)
 Critical Depth = 4.43(In.)
 Pipe flow velocity = 7.09(Ft/s)
 Travel time through pipe = 0.09 min.
 Time of concentration (TC) = 7.41 min.

 Process from Point/Station 238.000 to Point/Station 238.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.193(Ac.)
 Runoff from this stream = 0.525(CFS)
 Time of concentration = 7.41 min.
 Rainfall intensity = 7.156(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	23.724	8.77	6.416
2	0.525	7.41	7.156

Qmax(1) =
 1.000 * 1.000 * 23.724) +
 0.897 * 1.000 * 0.525) + = 24.195
 Qmax(2) =
 1.000 * 0.844 * 23.724) +
 1.000 * 1.000 * 0.525) + = 20.555

Total of 2 streams to confluence:
 Flow rates before confluence point:
 23.724 0.525
 Maximum flow rates at confluence using above data:
 24.195 20.555
 Area of streams before confluence:
 8.085 0.193
 Results of confluence:
 Total flow rate = 24.195(CFS)
 Time of concentration = 8.774 min.
 Effective stream area after confluence = 8.278(Ac.)

 Process from Point/Station 238.000 to Point/Station 243.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 678.000(Ft.)
 Downstream point/station elevation = 662.000(Ft.)
 Pipe length = 83.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 24.195(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 24.195(CFS)
 Normal flow depth in pipe = 10.65(In.)
 Flow top width inside pipe = 13.61(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 25.96(Ft/s)
 Travel time through pipe = 0.05 min.
 Time of concentration (TC) = 8.83 min.
 End of computations, total study area = 8.278 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/19/13

FINAL OUTFALL 10 - Las Posas Road: Node 1 TO 6
POST DEVELOPMENT BEFORE DETENTION
100 Year Storm Event
File Name: 12052POSTOVERALL.RD3

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL]
(1.0 DU/A or Less)
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Initial subarea total flow distance = 1012.000(Ft.)
Highest elevation = 1140.000(Ft.)
Lowest elevation = 900.000(Ft.)
Elevation difference = 240.000(Ft.) Slope = 23.715 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 23.72 %, in a development type of
1.0 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.32 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.4100) * (100.000^{.5})] / (23.715^{(1/3)}) = 4.32$
The initial area total distance of 1012.00 (Ft.) entered leaves a
remaining distance of 912.00 (Ft.)
Using Figure 3-4, the travel time for this distance is 2.58 minutes
for a distance of 912.00 (Ft.) and a slope of 23.72 %
with an elevation difference of 216.28(Ft.) from the end of the top area
 $Tt = [11.9 * length(Mi)^3] / (elevation change(Ft.))^{.385} * 60(min/hr)$
= 2.585 Minutes
 $Tt = [(11.9 * 0.1727^3) / (216.28)]^{.385} = 2.58$
Total initial area Ti = 4.32 minutes from Figure 3-3 formula plus
2.58 minutes from the Figure 3-4 formula = 6.91 minutes
Rainfall intensity (I) = 7.486(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.410
Subarea runoff = 45.998(CFS)
Total initial stream area = 14.986(Ac.)

Process from Point/Station 2.000 to Point/Station 3.000

**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 148.425(CFS)
 Depth of flow = 1.083(Ft.), Average velocity = 12.664(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 10.00
 2 100.00 0.00
 3 200.00 10.00
 Manning's 'N' friction factor = 0.020

Sub-Channel flow = 148.425(CFS)
 flow top width = 21.652(Ft.)
 velocity= 12.664(Ft/s)
 area = 11.720(Sq.Ft)
 Froude number = 3.033

Upstream point elevation = 900.000(Ft.)
 Downstream point elevation = 721.000(Ft.)
 Flow length = 2700.000(Ft.)
 Travel time = 3.55 min.
 Time of concentration = 10.46 min.
 Depth of flow = 1.083(Ft.)
 Average velocity = 12.664(Ft/s)
 Total irregular channel flow = 148.425(CFS)
 Irregular channel normal depth above invert elev. = 1.083(Ft.)
 Average velocity of channel(s) = 12.664(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [LOW DENSITY RESIDENTIAL]
 (1.0 DU/A or Less)
 Impervious value, Ai = 0.100
 Sub-Area C Value = 0.410
 Rainfall intensity = 5.728(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.410 CA = 43.782
 Subarea runoff = 204.795(CFS) for 91.800(Ac.)
 Total runoff = 250.793(CFS) Total area = 106.786(Ac.)
 Depth of flow = 1.318(Ft.), Average velocity = 14.439(Ft/s)

 Process from Point/Station 3.000 to Point/Station 4.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 307.673(CFS)
 Depth of flow = 1.722(Ft.), Average velocity = 10.375(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 100.00 0.00
 3 100.00 5.00
 Manning's 'N' friction factor = 0.023

Sub-Channel flow = 307.673(CFS)
 flow top width = 34.441(Ft.)
 velocity= 10.375(Ft/s)
 area = 29.655(Sq.Ft)
 Froude number = 1.970

Upstream point elevation = 721.000(Ft.)
 Downstream point elevation = 668.000(Ft.)
 Flow length = 1575.000(Ft.)
 Travel time = 2.53 min.
 Time of concentration = 12.99 min.
 Depth of flow = 1.722(Ft.)
 Average velocity = 10.375(Ft/s)

```

Total irregular channel flow = 307.673(CFS)
Irregular channel normal depth above invert elev. = 1.722(Ft.)
Average velocity of channel(s) = 10.375(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL ]
(1.0 DU/A or Less )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Rainfall intensity = 4.981(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.410 CA = 73.172
Subarea runoff = 113.696(CFS) for 71.682(Ac.)
Total runoff = 364.490(CFS) Total area = 178.468(Ac.)
Depth of flow = 1.835(Ft.), Average velocity = 10.824(Ft/s)

+++++
Process from Point/Station 4.000 to Point/Station 4.000
**** CONFLUENCE OF MINOR STREAMS ****

-----
Along Main Stream number: 1 in normal stream number 1
Stream flow area = 178.468(Ac.)
Runoff from this stream = 364.490(CFS)
Time of concentration = 12.99 min.
Rainfall intensity = 4.981(In/Hr)

+++++
Process from Point/Station 9.000 to Point/Station 10.000
**** INITIAL AREA EVALUATION ****

-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL ]
(1.0 DU/A or Less )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Initial subarea total flow distance = 1909.000(Ft.)
Highest elevation = 1302.000(Ft.)
Lowest elevation = 820.000(Ft.)
Elevation difference = 482.000(Ft.) Slope = 25.249 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 25.25 %, in a development type of
1.0 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.23 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.4100)*( 100.000^0.5)/( 25.249^(1/3))]= 4.23
The initial area total distance of 1909.00 (Ft.) entered leaves a
remaining distance of 1809.00 (Ft.)
Using Figure 3-4, the travel time for this distance is 4.28 minutes
for a distance of 1809.00 (Ft.) and a slope of 25.25 %
with an elevation difference of 456.75(Ft.) from the end of the top area
Tt = [11.9*length(Mi)^3]/(elevation change(Ft.))^0.385 *60(min/hr)
= 4.275 Minutes
Tt=[(11.9*0.3426^3)/(456.75)]^0.385= 4.28
Total initial area Ti = 4.23 minutes from Figure 3-3 formula plus
4.28 minutes from the Figure 3-4 formula = 8.51 minutes
Rainfall intensity (I) = 6.544(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.410
Subarea runoff = 60.081(CFS)
Total initial stream area = 22.391(Ac.)

+++++
Process from Point/Station 10.000 to Point/Station 4.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

Estimated mean flow rate at midpoint of channel = 194.618(CFS)
Depth of flow = 0.918(Ft.), Average velocity = 11.540(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              5.00
      2             100.00              0.00
      3             200.00              5.00
Manning's 'N' friction factor = 0.020
-----
Sub-Channel flow = 194.618(CFS)
      '      '      flow top width = 36.731(Ft.)
      '      '      velocity= 11.540(Ft/s)
      '      '      area = 16.864(Sq.Ft)
      '      '      Froude number = 3.001

Upstream point elevation = 820.000(Ft.)
Downstream point elevation = 668.000(Ft.)
Flow length = 2228.000(Ft.)
Travel time = 3.22 min.
Time of concentration = 11.73 min.
Depth of flow = 0.918(Ft.)
Average velocity = 11.540(Ft/s)
Total irregular channel flow = 194.618(CFS)
Irregular channel normal depth above invert elev. = 0.918(Ft.)
Average velocity of channel(s) = 11.540(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL ]
(1.0 DU/A or Less )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Rainfall intensity = 5.321(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.410 CA = 61.845
Subarea runoff = 269.022(CFS) for 128.450(Ac.)
Total runoff = 329.102(CFS) Total area = 150.841(Ac.)
Depth of flow = 1.118(Ft.), Average velocity = 13.160(Ft/s)

+++++
Process from Point/Station 4.000 to Point/Station 4.000
**** CONFLUENCE OF MINOR STREAMS ****
-----
Along Main Stream number: 1 in normal stream number 2
Stream flow area = 150.841(Ac.)
Runoff from this stream = 329.102(CFS)
Time of concentration = 11.73 min.
Rainfall intensity = 5.321(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 364.490 12.99 4.981
2 329.102 11.73 5.321
Qmax(1) =
1.000 * 1.000 * 364.490) +
0.936 * 1.000 * 329.102) + = 672.557
Qmax(2) =
1.000 * 0.903 * 364.490) +
1.000 * 1.000 * 329.102) + = 658.114

Total of 2 streams to confluence:
Flow rates before confluence point:
364.490 329.102
Maximum flow rates at confluence using above data:
672.557 658.114

```



```

Area of streams before confluence:
    178.468    150.841
Results of confluence:
Total flow rate =    672.557(CFS)
Time of concentration =    12.991 min.
Effective stream area after confluence =    329.309(Ac.)

+++++
Process from Point/Station    4.000 to Point/Station    4.200
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Depth of flow =    3.950(Ft.), Average velocity =    6.898(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number    'X' coordinate    'Y' coordinate
    1            0.00            16.00
    2           100.00            0.00
    3           200.00           16.00
Manning's 'N' friction factor =    0.045
-----
Sub-Channel flow =    672.556(CFS)
'    '    flow top width =    49.371(Ft.)
'    '    velocity =    6.898(Ft/s)
'    '    area =    97.500(Sq.Ft)
'    '    Froude number =    0.865

Upstream point elevation =    668.000(Ft.)
Downstream point elevation =    656.000(Ft.)
Flow length =    670.000(Ft.)
Travel time =    1.62 min.
Time of concentration =    14.61 min.
Depth of flow =    3.950(Ft.)
Average velocity =    6.898(Ft/s)
Total irregular channel flow =    672.557(CFS)
Irregular channel normal depth above invert elev. =    3.950(Ft.)
Average velocity of channel(s) =    6.898(Ft/s)

+++++
Process from Point/Station    4.200 to Point/Station    4.200
**** CONFLUENCE OF MINOR STREAMS ****

-----
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    329.309(Ac.)
Runoff from this stream =    672.557(CFS)
Time of concentration =    14.61 min.
Rainfall intensity =    4.618(In/Hr)

+++++
Process from Point/Station    4.100 to Point/Station    4.200
**** INITIAL AREA EVALUATION ****

-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN    ]
(Permanent Open Space    )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 887.000(Ft.)
Highest elevation = 835.000(Ft.)
Lowest elevation = 656.000(Ft.)
Elevation difference = 179.000(Ft.) Slope = 20.180 %
Top of Initial Area Slope adjusted by User to 30.000 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 30.00 %, in a development type of
Permanent Open Space
In Accordance With Table 3-2
Initial Area Time of Concentration =    6.90 minutes

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(for slope value of 10.00 %)
Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 48.850(CFS)
Total initial stream area = 18.630(Ac.)

+++++
Process from Point/Station 4.200 to Point/Station 4.200
**** CONFLUENCE OF MINOR STREAMS ****

-----
Along Main Stream number: 1 in normal stream number 2
Stream flow area = 18.630(Ac.)
Runoff from this stream = 48.850(CFS)
Time of concentration = 6.90 min.
Rainfall intensity = 7.492(In/Hr)

+++++
Process from Point/Station 511.000 to Point/Station 4.200
**** USER DEFINED FLOW INFORMATION AT A POINT ****

-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 9.00 min. Rain intensity = 6.31(In/Hr)
Total area = 0.944(Ac.) Total runoff = 3.650(CFS)

+++++
Process from Point/Station 4.200 to Point/Station 4.200
**** CONFLUENCE OF MINOR STREAMS ****

-----
Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.944(Ac.)
Runoff from this stream = 3.650(CFS)
Time of concentration = 9.00 min.
Rainfall intensity = 6.312(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 672.557 14.61 4.618
2 48.850 6.90 7.492
3 3.650 9.00 6.312
Qmax(1) =
1.000 * 1.000 * 672.557) +
0.616 * 1.000 * 48.850) +
0.732 * 1.000 * 3.650) + = 705.338
Qmax(2) =
1.000 * 0.472 * 672.557) +
1.000 * 1.000 * 48.850) +
1.000 * 0.767 * 3.650) + = 369.286
Qmax(3) =
1.000 * 0.616 * 672.557) +
0.843 * 1.000 * 48.850) +
1.000 * 1.000 * 3.650) + = 459.117

Total of 3 streams to confluence:
Flow rates before confluence point:
672.557 48.850 3.650
Maximum flow rates at confluence using above data:
705.338 369.286 459.117
Area of streams before confluence:
329.309 18.630 0.944

```

Results of confluence:

Total flow rate = 705.338(CFS)
 Time of concentration = 14.610 min.
 Effective stream area after confluence = 348.883(Ac.)

 Process from Point/Station 4.200 to Point/Station 4.300
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 4.839(Ft.), Average velocity = 4.819(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 16.00
 2 100.00 0.00
 3 200.00 16.00

Manning's 'N' friction factor = 0.045

 Sub-Channel flow = 705.338(CFS)
 ' ' flow top width = 60.492(Ft.)
 ' ' velocity = 4.819(Ft/s)
 ' ' area = 146.372(Sq.Ft)
 ' ' Froude number = 0.546

Upstream point elevation = 656.000(Ft.)
 Downstream point elevation = 654.000(Ft.)
 Flow length = 300.000(Ft.)
 Travel time = 1.04 min.
 Time of concentration = 15.65 min.
 Depth of flow = 4.839(Ft.)
 Average velocity = 4.819(Ft/s)
 Total irregular channel flow = 705.338(CFS)
 Irregular channel normal depth above invert elev. = 4.839(Ft.)
 Average velocity of channel(s) = 4.819(Ft/s)

 Process from Point/Station 4.300 to Point/Station 4.300
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 348.883(Ac.)
 Runoff from this stream = 705.338(CFS)
 Time of concentration = 15.65 min.
 Rainfall intensity = 4.418(In/Hr)

 Process from Point/Station 523.000 to Point/Station 4.300
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 8.198(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 6.00 min. Rain intensity = 8.20(In/Hr)
 Total area = 0.860(Ac.) Total runoff = 4.100(CFS)

 Process from Point/Station 4.300 to Point/Station 4.300
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.860(Ac.)
 Runoff from this stream = 4.100(CFS)

Time of concentration = 6.00 min.
 Rainfall intensity = 8.198(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	705.338	15.65	4.418
2	4.100	6.00	8.198

Qmax(1) =
 1.000 * 1.000 * 705.338) +
 0.539 * 1.000 * 4.100) + = 707.547
 Qmax(2) =
 1.000 * 0.383 * 705.338) +
 1.000 * 1.000 * 4.100) + = 274.561

Total of 2 streams to confluence:
 Flow rates before confluence point:
 705.338 4.100
 Maximum flow rates at confluence using above data:
 707.547 274.561
 Area of streams before confluence:
 348.883 0.860
 Results of confluence:
 Total flow rate = 707.547(CFS)
 Time of concentration = 15.647 min.
 Effective stream area after confluence = 349.743(Ac.)

 Process from Point/Station 4.300 to Point/Station 430.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 647.000(Ft.)
 Downstream point/station elevation = 641.300(Ft.)
 Pipe length = 83.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 707.547(CFS)
 Nearest computed pipe diameter = 63.00(In.)
 Calculated individual pipe flow = 707.547(CFS)
 Normal flow depth in pipe = 47.16(In.)
 Flow top width inside pipe = 54.67(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 40.69(Ft/s)
 Travel time through pipe = 0.03 min.
 Time of concentration (TC) = 15.68 min.

 Process from Point/Station 430.000 to Point/Station 430.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 349.743(Ac.)
 Runoff from this stream = 707.547(CFS)
 Time of concentration = 15.68 min.
 Rainfall intensity = 4.412(In/Hr)

 Process from Point/Station 434.000 to Point/Station 430.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 8.198(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 6.00 min. Rain intensity = 8.20(In/Hr)

Total area = 1.850(Ac.) Total runoff = 8.780(CFS)

Process from Point/Station 430.000 to Point/Station 430.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 1.850(Ac.)
Runoff from this stream = 8.780(CFS)
Time of concentration = 6.00 min.
Rainfall intensity = 8.198(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	707.547	15.68	4.412
2	8.780	6.00	8.198

Qmax(1) =
1.000 * 1.000 * 707.547) +
0.538 * 1.000 * 8.780) + = 712.272
Qmax(2) =
1.000 * 0.383 * 707.547) +
1.000 * 1.000 * 8.780) + = 279.500

Total of 2 streams to confluence:
Flow rates before confluence point:
707.547 8.780
Maximum flow rates at confluence using above data:
712.272 279.500
Area of streams before confluence:
349.743 1.850
Results of confluence:
Total flow rate = 712.272(CFS)
Time of concentration = 15.681 min.
Effective stream area after confluence = 351.593(Ac.)

Process from Point/Station 430.000 to Point/Station 5.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 0.355(Ft.), Average velocity = 3.337(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 25.00
2 60.00 0.00
3 660.00 0.00
4 720.00 20.00

Manning's 'N' friction factor = 0.045

Sub-Channel flow = 712.278(CFS)
' ' flow top width = 601.918(Ft.)
' ' velocity = 3.337(Ft/s)
' ' area = 213.424(Sq.Ft)
' ' Froude number = 0.988

Upstream point elevation = 641.300(Ft.)
Downstream point elevation = 631.000(Ft.)
Flow length = 253.000(Ft.)
Travel time = 1.26 min.
Time of concentration = 16.94 min.
Depth of flow = 0.355(Ft.)
Average velocity = 3.337(Ft/s)
Total irregular channel flow = 712.272(CFS)
Irregular channel normal depth above invert elev. = 0.355(Ft.)
Average velocity of channel(s) = 3.337(Ft/s)

Process from Point/Station 5.000 to Point/Station 5.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 351.593(Ac.)
 Runoff from this stream = 712.272(CFS)
 Time of concentration = 16.94 min.
 Rainfall intensity = 4.197(In/Hr)

 Process from Point/Station 82.000 to Point/Station 5.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 9.00 min. Rain intensity = 6.31(In/Hr)
 Total area = 103.820(Ac.) Total runoff = 212.100(CFS)

 Process from Point/Station 5.000 to Point/Station 5.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 103.820(Ac.)
 Runoff from this stream = 212.100(CFS)
 Time of concentration = 9.00 min.
 Rainfall intensity = 6.312(In/Hr)

 Process from Point/Station 648.000 to Point/Station 5.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 5.897(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 10.00 min. Rain intensity = 5.90(In/Hr)
 Total area = 15.310(Ac.) Total runoff = 49.700(CFS)

 Process from Point/Station 5.000 to Point/Station 5.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 15.310(Ac.)
 Runoff from this stream = 49.700(CFS)
 Time of concentration = 10.00 min.
 Rainfall intensity = 5.897(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	712.272	16.94	4.197
2	212.100	9.00	6.312

```

3          49.700      10.00      5.897
Qmax(1) =
      1.000 *      1.000 * 712.272) +
      0.665 *      1.000 * 212.100) +
      0.712 *      1.000 * 49.700) + =      888.667
Qmax(2) =
      1.000 *      0.531 * 712.272) +
      1.000 *      1.000 * 212.100) +
      1.000 *      0.900 * 49.700) + =      635.141
Qmax(3) =
      1.000 *      0.590 * 712.272) +
      0.934 *      1.000 * 212.100) +
      1.000 *      1.000 * 49.700) + =      668.211

Total of 3 streams to confluence:
Flow rates before confluence point:
      712.272      212.100      49.700
Maximum flow rates at confluence using above data:
      888.667      635.141      668.211
Area of streams before confluence:
      351.593      103.820      15.310
Results of confluence:
Total flow rate =      888.667(CFS)
Time of concentration =      16.945 min.
Effective stream area after confluence =      470.723(Ac.)

+++++
Process from Point/Station      5.000 to Point/Station      543.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Depth of flow =      0.420(Ft.), Average velocity =      3.524(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              25.00
      2             60.00              0.00
      3            660.00              0.00
      4            720.00             20.00
Manning's 'N' friction factor =      0.045

-----
Sub-Channel flow =      888.667(CFS)
'      '      flow top width =      602.265(Ft.)
'      '      velocity=      3.524(Ft/s)
'      '      area =      252.185(Sq.Ft)
'      '      Froude number =      0.960

Upstream point elevation =      631.000(Ft.)
Downstream point elevation =      627.000(Ft.)
Flow length =      110.000(Ft.)
Travel time =      0.52 min.
Time of concentration =      17.47 min.
Depth of flow =      0.420(Ft.)
Average velocity =      3.524(Ft/s)
Total irregular channel flow =      888.667(CFS)
Irregular channel normal depth above invert elev. =      0.420(Ft.)
Average velocity of channel(s) =      3.524(Ft/s)

+++++
Process from Point/Station      543.000 to Point/Station      543.000
**** CONFLUENCE OF MINOR STREAMS ****

-----
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      470.723(Ac.)
Runoff from this stream =      888.667(CFS)
Time of concentration =      17.47 min.
Rainfall intensity =      4.116(In/Hr)

+++++
Process from Point/Station      543.000 to Point/Station      543.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 7.423(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 7.00 min. Rain intensity = 7.42(In/Hr)
Total area = 5.790(Ac.) Total runoff = 20.100(CFS)

*****
Process from Point/Station 543.000 to Point/Station 543.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 5.790(Ac.)
Runoff from this stream = 20.100(CFS)
Time of concentration = 7.00 min.
Rainfall intensity = 7.423(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 888.667 17.47 4.116
2 20.100 7.00 7.423
Qmax(1) =
1.000 * 1.000 * 888.667) +
0.554 * 1.000 * 20.100) + = 899.812
Qmax(2) =
1.000 * 0.401 * 888.667) +
1.000 * 1.000 * 20.100) + = 376.276

Total of 2 streams to confluence:
Flow rates before confluence point:
888.667 20.100
Maximum flow rates at confluence using above data:
899.812 376.276
Area of streams before confluence:
470.723 5.790
Results of confluence:
Total flow rate = 899.812(CFS)
Time of concentration = 17.465 min.
Effective stream area after confluence = 476.513(Ac.)

*****
Process from Point/Station 543.000 to Point/Station 5.100
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 5.232(Ft.), Average velocity = 9.745(Ft/s)
***** Irregular Channel Data *****

-----
Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 24.00
2 85.00 0.00
3 226.00 44.00
Manning's 'N' friction factor = 0.045

-----
Sub-Channel flow = 899.812(CFS)
' ' flow top width = 35.297(Ft.)
' ' velocity= 9.745(Ft/s)
' ' area = 92.340(Sq.Ft)
' ' Froude number = 1.062

Upstream point elevation = 627.000(Ft.)
Downstream point elevation = 604.000(Ft.)

```


Flow length = 900.000(Ft.)
 Travel time = 1.54 min.
 Time of concentration = 19.00 min.
 Depth of flow = 5.232(Ft.)
 Average velocity = 9.745(Ft/s)
 Total irregular channel flow = 899.812(CFS)
 Irregular channel normal depth above invert elev. = 5.232(Ft.)
 Average velocity of channel(s) = 9.745(Ft/s)

 Process from Point/Station 5.100 to Point/Station 5.100
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 476.513(Ac.)
 Runoff from this stream = 899.812(CFS)
 Time of concentration = 19.00 min.
 Rainfall intensity = 3.897(In/Hr)

 Process from Point/Station 243.000 to Point/Station 5.100
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 9.00 min. Rain intensity = 6.31(In/Hr)
 Total area = 8.280(Ac.) Total runoff = 24.200(CFS)

 Process from Point/Station 5.100 to Point/Station 5.100
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 8.280(Ac.)
 Runoff from this stream = 24.200(CFS)
 Time of concentration = 9.00 min.
 Rainfall intensity = 6.312(In/Hr)

 Process from Point/Station 552.000 to Point/Station 5.100
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 7.423(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 7.00 min. Rain intensity = 7.42(In/Hr)
 Total area = 4.450(Ac.) Total runoff = 13.800(CFS)

 Process from Point/Station 5.100 to Point/Station 5.100
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 4.450(Ac.)

Runoff from this stream = 13.800(CFS)
 Time of concentration = 7.00 min.
 Rainfall intensity = 7.423(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	899.812	19.00	3.897
2	24.200	9.00	6.312
3	13.800	7.00	7.423

Qmax(1) =
 1.000 * 1.000 * 899.812) +
 0.617 * 1.000 * 24.200) +
 0.525 * 1.000 * 13.800) + = 922.001

Qmax(2) =
 1.000 * 0.474 * 899.812) +
 1.000 * 1.000 * 24.200) +
 0.850 * 1.000 * 13.800) + = 462.061

Qmax(3) =
 1.000 * 0.368 * 899.812) +
 1.000 * 0.778 * 24.200) +
 1.000 * 1.000 * 13.800) + = 364.053

Total of 3 streams to confluence:

Flow rates before confluence point:

899.812 24.200 13.800

Maximum flow rates at confluence using above data:

922.001 462.061 364.053

Area of streams before confluence:

476.513 8.280 4.450

Results of confluence:

Total flow rate = 922.001(CFS)

Time of concentration = 19.004 min.

Effective stream area after confluence = 489.243(Ac.)

 Process from Point/Station 5.100 to Point/Station 5.200
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 5.072(Ft.), Average velocity = 10.624(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	24.00
2	85.00	0.00
3	226.00	44.00

Manning's 'N' friction factor = 0.045

Sub-Channel flow = 922.001(CFS)
 ' ' flow top width = 34.218(Ft.)
 ' ' velocity = 10.624(Ft/s)
 ' ' area = 86.782(Sq.Ft)
 ' ' Froude number = 1.176

Upstream point elevation = 604.000(Ft.)

Downstream point elevation = 592.000(Ft.)

Flow length = 379.000(Ft.)

Travel time = 0.59 min.

Time of concentration = 19.60 min.

Depth of flow = 5.072(Ft.)

Average velocity = 10.624(Ft/s)

Total irregular channel flow = 922.001(CFS)

Irregular channel normal depth above invert elev. = 5.072(Ft.)

Average velocity of channel(s) = 10.624(Ft/s)

 Process from Point/Station 5.200 to Point/Station 5.200
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 489.243(Ac.)
Runoff from this stream = 922.001(CFS)
Time of concentration = 19.60 min.
Rainfall intensity = 3.821(In/Hr)

Process from Point/Station 559.000 to Point/Station 5.200
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 7.423(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 7.00 min. Rain intensity = 7.42(In/Hr)
Total area = 4.620(Ac.) Total runoff = 13.000(CFS)

Process from Point/Station 5.200 to Point/Station 5.200
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 4.620(Ac.)
Runoff from this stream = 13.000(CFS)
Time of concentration = 7.00 min.
Rainfall intensity = 7.423(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	922.001	19.60	3.821
2	13.000	7.00	7.423

Qmax(1) =
1.000 * 1.000 * 922.001) +
0.515 * 1.000 * 13.000) + = 928.693

Qmax(2) =
1.000 * 0.357 * 922.001) +
1.000 * 1.000 * 13.000) + = 342.302

Total of 2 streams to confluence:
Flow rates before confluence point:
922.001 13.000
Maximum flow rates at confluence using above data:
928.693 342.302
Area of streams before confluence:
489.243 4.620
Results of confluence:
Total flow rate = 928.693(CFS)
Time of concentration = 19.599 min.
Effective stream area after confluence = 493.863(Ac.)

```

+++++
Process from Point/Station      5.200 to Point/Station      6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel =    948.916(CFS)
Depth of flow =    5.649(Ft.), Average velocity =    8.817(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              24.00
      2             85.00              0.00
      3            226.00             44.00
Manning's 'N' friction factor =    0.045
-----
Sub-Channel flow =    948.916(CFS)
'      '      flow top width =    38.107(Ft.)
'      '      velocity=    8.817(Ft/s)
'      '      area =    107.629(Sq.Ft)
'      '      Froude number =    0.925

Upstream point elevation =    592.000(Ft.)
Downstream point elevation =    575.000(Ft.)
Flow length =    900.000(Ft.)
Travel time =    1.70 min.
Time of concentration =    21.30 min.
Depth of flow =    5.649(Ft.)
Average velocity =    8.817(Ft/s)
Total irregular channel flow =    948.916(CFS)
Irregular channel normal depth above invert elev. =    5.649(Ft.)
Average velocity of channel(s) =    8.817(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL                      ]
(2.0 DU/A or Less                          )
Impervious value, Ai = 0.200
Sub-Area C Value = 0.460
Rainfall intensity =    3.621(In/Hr) for a    100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.463  CA =    267.626
Subarea runoff =    40.386(CFS) for    83.770(Ac.)
Total runoff =    969.079(CFS)      Total area =    577.633(Ac.)
Depth of flow =    5.693(Ft.), Average velocity =    8.863(Ft/s)
End of computations, total study area =    577.633 (Ac.)

```

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/18/13

***** Hydrology Study Control Information *****

File: 12052POSTB.RD3

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 30.000 to Point/Station 31.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 92.000(Ft.)
Highest elevation = 706.000(Ft.)
Lowest elevation = 703.000(Ft.)
Elevation difference = 3.000(Ft.) Slope = 3.261 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.26 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.76 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.261^{(1/3)})] = 5.76$
Rainfall intensity (I) = 8.419(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.364(CFS)
Total initial stream area = 0.072(Ac.)

Process from Point/Station 31.000 to Point/Station 32.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 698.500(Ft.)
Downstream point/station elevation = 693.300(Ft.)
Pipe length = 85.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.364(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.364(CFS)
Normal flow depth in pipe = 2.10(In.)
Flow top width inside pipe = 5.72(In.)
Critical Depth = 3.68(In.)
Pipe flow velocity = 5.95(Ft/s)
Travel time through pipe = 0.24 min.
Time of concentration (TC) = 6.00 min.

Street B – Before Detention

```

+++++
Process from Point/Station      32.000 to Point/Station      32.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      6.00 min.
Rainfall intensity =      8.202(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA =      0.097
Subarea runoff =      0.434(CFS) for      0.090(Ac.)
Total runoff =      0.797(CFS)      Total area =      0.162(Ac.)

+++++
Process from Point/Station      32.000 to Point/Station      33.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 693.300(Ft.)
Downstream point/station elevation = 691.300(Ft.)
Pipe length = 85.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.797(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.797(CFS)
Normal flow depth in pipe = 4.56(In.)
Flow top width inside pipe = 5.13(In.)
Critical Depth = 5.32(In.)
Pipe flow velocity = 4.98(Ft/s)
Travel time through pipe = 0.28 min.
Time of concentration (TC) = 6.28 min.

+++++
Process from Point/Station      33.000 to Point/Station      33.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.28 min.
Rainfall intensity = 7.961(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.136
Subarea runoff = 0.287(CFS) for 0.065(Ac.)
Total runoff = 1.084(CFS)      Total area = 0.227(Ac.)

+++++
Process from Point/Station      33.000 to Point/Station      34.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.300(Ft.)
Downstream point/station elevation = 690.800(Ft.)
Pipe length = 43.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.084(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.084(CFS)
Normal flow depth in pipe = 5.06(In.)
Flow top width inside pipe = 8.93(In.)
Critical Depth = 5.74(In.)
Pipe flow velocity = 4.23(Ft/s)
Travel time through pipe = 0.17 min.
Time of concentration (TC) = 6.45 min.

```

Street B – Before Detention

```

+++++
Process from Point/Station      34.000 to Point/Station      34.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      6.45 min.
Rainfall intensity =      7.825(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA =      0.159
Subarea runoff =      0.160(CFS) for      0.038(Ac.)
Total runoff =      1.244(CFS)      Total area =      0.265(Ac.)

```

```

+++++
Process from Point/Station      34.000 to Point/Station      39.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 690.800(Ft.)
Downstream point/station elevation = 688.000(Ft.)
Pipe length = 3.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.244(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.244(CFS)
Normal flow depth in pipe = 1.96(In.)
Flow top width inside pipe = 5.62(In.)
Critical depth could not be calculated.
Pipe flow velocity = 22.41(Ft/s)
Travel time through pipe = 0.00 min.
Time of concentration (TC) = 6.45 min.

```

```

+++++
Process from Point/Station      39.000 to Point/Station      39.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.265(Ac.)
Runoff from this stream = 1.244(CFS)
Time of concentration = 6.45 min.
Rainfall intensity = 7.823(In/Hr)

```

```

+++++
Process from Point/Station      30.100 to Point/Station      35.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 96.000(Ft.)
Highest elevation = 706.000(Ft.)
Lowest elevation = 703.000(Ft.)
Elevation difference = 3.000(Ft.) Slope = 3.125 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.13 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.84 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3))

```

Street B – Before Detention

```

TC = [1.8*(1.1-0.6000)*( 90.000^.5)/( 3.125^(1/3))]= 5.84
Rainfall intensity (I) = 8.343(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.365(CFS)
Total initial stream area = 0.073(Ac.)

+++++
Process from Point/Station 35.000 to Point/Station 36.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 698.500(Ft.)
Downstream point/station elevation = 695.000(Ft.)
Pipe length = 88.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.365(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.365(CFS)
Normal flow depth in pipe = 2.36(In.)
Flow top width inside pipe = 5.86(In.)
Critical Depth = 3.68(In.)
Pipe flow velocity = 5.10(Ft/s)
Travel time through pipe = 0.29 min.
Time of concentration (TC) = 6.13 min.

+++++
Process from Point/Station 36.000 to Point/Station 36.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.13 min.
Rainfall intensity = 8.088(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.085
Subarea runoff = 0.319(CFS) for 0.068(Ac.)
Total runoff = 0.684(CFS) Total area = 0.141(Ac.)

+++++
Process from Point/Station 36.000 to Point/Station 37.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 695.000(Ft.)
Downstream point/station elevation = 691.300(Ft.)
Pipe length = 84.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.684(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.684(CFS)
Normal flow depth in pipe = 3.28(In.)
Flow top width inside pipe = 5.97(In.)
Critical Depth = 5.02(In.)
Pipe flow velocity = 6.22(Ft/s)
Travel time through pipe = 0.23 min.
Time of concentration (TC) = 6.35 min.

+++++
Process from Point/Station 37.000 to Point/Station 37.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450

```

Street B – Before Detention

Sub-Area C Value = 0.600
 Time of concentration = 6.35 min.
 Rainfall intensity = 7.902(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.121
 Subarea runoff = 0.273(CFS) for 0.061(Ac.)
 Total runoff = 0.958(CFS) Total area = 0.202(Ac.)

 Process from Point/Station 37.000 to Point/Station 38.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.300(Ft.)
 Downstream point/station elevation = 689.300(Ft.)
 Pipe length = 84.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.958(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 0.958(CFS)
 Normal flow depth in pipe = 3.82(In.)
 Flow top width inside pipe = 8.90(In.)
 Critical Depth = 5.38(In.)
 Pipe flow velocity = 5.37(Ft/s)
 Travel time through pipe = 0.26 min.
 Time of concentration (TC) = 6.61 min.

 Process from Point/Station 38.000 to Point/Station 38.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.61 min.
 Rainfall intensity = 7.699(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.145
 Subarea runoff = 0.160(CFS) for 0.040(Ac.)
 Total runoff = 1.118(CFS) Total area = 0.242(Ac.)

 Process from Point/Station 38.000 to Point/Station 39.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 689.300(Ft.)
 Downstream point/station elevation = 688.000(Ft.)
 Pipe length = 33.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.118(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.118(CFS)
 Normal flow depth in pipe = 3.62(In.)
 Flow top width inside pipe = 8.83(In.)
 Critical Depth = 5.83(In.)
 Pipe flow velocity = 6.72(Ft/s)
 Travel time through pipe = 0.08 min.
 Time of concentration (TC) = 6.70 min.

 Process from Point/Station 39.000 to Point/Station 39.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.242(Ac.)
 Runoff from this stream = 1.118(CFS)
 Time of concentration = 6.70 min.
 Rainfall intensity = 7.639(In/Hr)

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	1.244	6.45	7.823
2	1.118	6.70	7.639
Qmax(1) =			
	1.000 *	1.000 *	1.244) +
	1.000 *	0.964 *	1.118) + = 2.321
Qmax(2) =			
	0.976 *	1.000 *	1.244) +
	1.000 *	1.000 *	1.118) + = 2.333

Total of 2 streams to confluence:

Flow rates before confluence point:

1.244 1.118

Maximum flow rates at confluence using above data:

2.321 2.333

Area of streams before confluence:

0.265 0.242

Results of confluence:

Total flow rate = 2.333(CFS)

Time of concentration = 6.695 min.

Effective stream area after confluence = 0.507(Ac.)

 Process from Point/Station 39.000 to Point/Station 130.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
 Downstream point/station elevation = 685.700(Ft.)
 Pipe length = 128.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.333(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 2.333(CFS)
 Normal flow depth in pipe = 5.92(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical Depth = 7.85(In.)
 Pipe flow velocity = 6.05(Ft/s)
 Travel time through pipe = 0.35 min.
 Time of concentration (TC) = 7.05 min.

 Process from Point/Station 130.000 to Point/Station 130.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.507(Ac.)
 Runoff from this stream = 2.333(CFS)
 Time of concentration = 7.05 min.
 Rainfall intensity = 7.390(In/Hr)

 Process from Point/Station 139.000 to Point/Station 139.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 9.00 min. Rain intensity = 6.31(In/Hr)
 Total area = 1.640(Ac.) Total runoff = 6.100(CFS)

Street B – Before Detention

Process from Point/Station 139.000 to Point/Station 130.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 689.900(Ft.)
Downstream point/station elevation = 685.700(Ft.)
Pipe length = 75.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 6.100(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 6.100(CFS)
Normal flow depth in pipe = 7.56(In.)
Flow top width inside pipe = 11.58(In.)
Critical depth could not be calculated.
Pipe flow velocity = 11.70(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 9.11 min.

Process from Point/Station 130.000 to Point/Station 130.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 1.640(Ac.)
Runoff from this stream = 6.100(CFS)
Time of concentration = 9.11 min.
Rainfall intensity = 6.264(In/Hr)

Process from Point/Station 129.000 to Point/Station 129.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 9.00 min. Rain intensity = 6.31(In/Hr)
Total area = 1.340(Ac.) Total runoff = 5.000(CFS)

Process from Point/Station 129.000 to Point/Station 130.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
Downstream point/station elevation = 685.700(Ft.)
Pipe length = 123.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 5.000(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 5.000(CFS)
Normal flow depth in pipe = 9.71(In.)
Flow top width inside pipe = 14.33(In.)
Critical Depth = 10.89(In.)
Pipe flow velocity = 5.94(Ft/s)
Travel time through pipe = 0.34 min.
Time of concentration (TC) = 9.34 min.

Process from Point/Station 130.000 to Point/Station 130.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 1.340(Ac.)
Runoff from this stream = 5.000(CFS)
Time of concentration = 9.34 min.

Rainfall intensity = 6.161(In/Hr)

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.333	7.05	7.390
2	6.100	9.11	6.264
3	5.000	9.34	6.161

Qmax(1) =

1.000 *	1.000 *	2.333) +	
1.000 *	0.774 *	6.100) +	
1.000 *	0.754 *	5.000) + =	10.825

Qmax(2) =

0.848 *	1.000 *	2.333) +	
1.000 *	1.000 *	6.100) +	
1.000 *	0.975 *	5.000) + =	12.950

Qmax(3) =

0.834 *	1.000 *	2.333) +	
0.983 *	1.000 *	6.100) +	
1.000 *	1.000 *	5.000) + =	12.944

Total of 3 streams to confluence:

Flow rates before confluence point:

2.333 6.100 5.000

Maximum flow rates at confluence using above data:

10.825 12.950 12.944

Area of streams before confluence:

0.507 1.640 1.340

Results of confluence:

Total flow rate = 12.950(CFS)

Time of concentration = 9.107 min.

Effective stream area after confluence = 3.487(Ac.)

Process from Point/Station 130.000 to Point/Station 42.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.700(Ft.)
Downstream point/station elevation = 684.700(Ft.)
Pipe length = 92.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 12.950(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 12.950(CFS)
Normal flow depth in pipe = 13.99(In.)
Flow top width inside pipe = 19.80(In.)
Critical Depth = 16.08(In.)
Pipe flow velocity = 7.60(Ft/s)
Travel time through pipe = 0.20 min.
Time of concentration (TC) = 9.31 min.

Process from Point/Station 42.000 to Point/Station 42.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 3.487(Ac.)
Runoff from this stream = 12.950(CFS)
Time of concentration = 9.31 min.
Rainfall intensity = 6.176(In/Hr)

Process from Point/Station 34.000 to Point/Station 40.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]

Street B – Before Detention

(10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 220.000(Ft.)
 Highest elevation = 696.000(Ft.)
 Lowest elevation = 690.000(Ft.)
 Elevation difference = 6.000(Ft.) Slope = 2.727 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 2.73 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.11 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (2.727^{(1/3)}) = 6.11$
 Rainfall intensity (I) = 8.102(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.841(CFS)
 Total initial stream area = 0.173(Ac.)

 Process from Point/Station 40.000 to Point/Station 42.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.500(Ft.)
 Downstream point/station elevation = 684.700(Ft.)
 Pipe length = 12.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.841(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.841(CFS)
 Normal flow depth in pipe = 3.28(In.)
 Flow top width inside pipe = 5.97(In.)
 Critical Depth = 5.42(In.)
 Pipe flow velocity = 7.65(Ft/s)
 Travel time through pipe = 0.03 min.
 Time of concentration (TC) = 6.14 min.

 Process from Point/Station 42.000 to Point/Station 42.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.173(Ac.)
 Runoff from this stream = 0.841(CFS)
 Time of concentration = 6.14 min.
 Rainfall intensity = 8.080(In/Hr)

 Process from Point/Station 38.000 to Point/Station 41.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 241.000(Ft.)
 Highest elevation = 696.000(Ft.)
 Lowest elevation = 690.000(Ft.)
 Elevation difference = 6.000(Ft.) Slope = 2.490 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 80.00 (Ft)
 for the top area slope value of 2.49 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.94 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (80.000^{.5})] / (2.490^{(1/3)}) = 5.94$

Rainfall intensity (I) = 8.253(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.867(CFS)
 Total initial stream area = 0.175(Ac.)

 Process from Point/Station 41.000 to Point/Station 42.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.500(Ft.)
 Downstream point/station elevation = 684.700(Ft.)
 Pipe length = 38.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.867(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 0.867(CFS)
 Normal flow depth in pipe = 3.74(In.)
 Flow top width inside pipe = 8.87(In.)
 Critical Depth = 5.11(In.)
 Pipe flow velocity = 4.99(Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 6.07 min.

 Process from Point/Station 42.000 to Point/Station 42.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 0.175(Ac.)
 Runoff from this stream = 0.867(CFS)
 Time of concentration = 6.07 min.
 Rainfall intensity = 8.141(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	12.950	9.31	6.176
2	0.841	6.14	8.080
3	0.867	6.07	8.141

Qmax(1) =
 1.000 * 1.000 * 12.950) +
 0.764 * 1.000 * 0.841) +
 0.759 * 1.000 * 0.867) + = 14.250

Qmax(2) =
 1.000 * 0.659 * 12.950) +
 1.000 * 1.000 * 0.841) +
 0.992 * 1.000 * 0.867) + = 10.239

Qmax(3) =
 1.000 * 0.652 * 12.950) +
 1.000 * 0.988 * 0.841) +
 1.000 * 1.000 * 0.867) + = 10.137

Total of 3 streams to confluence:
 Flow rates before confluence point:
 12.950 0.841 0.867
 Maximum flow rates at confluence using above data:
 14.250 10.239 10.137
 Area of streams before confluence:
 3.487 0.173 0.175
 Results of confluence:
 Total flow rate = 14.250(CFS)
 Time of concentration = 9.309 min.
 Effective stream area after confluence = 3.835(Ac.)

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*****
Process from Point/Station      42.000 to Point/Station      43.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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Upstream point/station elevation = 684.700(Ft.)
Downstream point/station elevation = 684.000(Ft.)
Pipe length = 52.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 14.250(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 14.250(CFS)
Normal flow depth in pipe = 13.89(In.)
Flow top width inside pipe = 19.88(In.)
Critical Depth = 16.82(In.)
Pipe flow velocity = 8.44(Ft/s)
Travel time through pipe = 0.10 min.
Time of concentration (TC) = 9.41 min.
End of computations, total study area = 3.835 (Ac.)

```

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 01/31/13

***** Hydrology Study Control Information *****

FILE: 12052WQE.RD3

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 123.000 to Point/Station 124.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 99.890(Ft.)
Highest elevation = 707.500(Ft.)
Lowest elevation = 706.500(Ft.)
Elevation difference = 1.000(Ft.) Slope = 1.001 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 1.00 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.25 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5} / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5}) / (1.001^{(1/3)})] = 7.25$
Rainfall intensity (I) = 7.254(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.514(CFS)
Total initial stream area = 0.118(Ac.)

Process from Point/Station 124.000 to Point/Station 125.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 704.500(Ft.)
Downstream point/station elevation = 702.000(Ft.)
Pipe length = 125.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.514(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.514(CFS)
Normal flow depth in pipe = 3.52(In.)
Flow top width inside pipe = 5.91(In.)
Critical Depth = 4.38(In.)
Pipe flow velocity = 4.30(Ft/s)

Flow rate for Pond E

Travel time through pipe = 0.48 min.
Time of concentration (TC) = 7.74 min.

Process from Point/Station 125.000 to Point/Station 125.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.74 min.
Rainfall intensity = 6.958(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.268
Subarea runoff = 1.352(CFS) for 0.329(Ac.)
Total runoff = 1.866(CFS) Total area = 0.447(Ac.)

Process from Point/Station 125.000 to Point/Station 126.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 702.000(Ft.)
Downstream point/station elevation = 696.600(Ft.)
Pipe length = 172.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.866(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.866(CFS)
Normal flow depth in pipe = 5.21(In.)
Flow top width inside pipe = 8.89(In.)
Critical Depth = 7.49(In.)
Pipe flow velocity = 7.03(Ft/s)
Travel time through pipe = 0.41 min.
Time of concentration (TC) = 8.15 min.

Process from Point/Station 126.000 to Point/Station 126.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.15 min.
Rainfall intensity = 6.731(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.499
Subarea runoff = 1.490(CFS) for 0.384(Ac.)
Total runoff = 3.356(CFS) Total area = 0.831(Ac.)

Process from Point/Station 126.000 to Point/Station 127.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 696.600(Ft.)
Downstream point/station elevation = 691.500(Ft.)
Pipe length = 157.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.356(CFS)
Nearest computed pipe diameter = 12.00(In.)

Flow rate for Pond E

Calculated individual pipe flow = 3.356(CFS)
 Normal flow depth in pipe = 6.16(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical Depth = 9.40(In.)
 Pipe flow velocity = 8.27(Ft/s)
 Travel time through pipe = 0.32 min.
 Time of concentration (TC) = 8.46 min.

 Process from Point/Station 127.000 to Point/Station 127.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.46 min.
 Rainfall intensity = 6.568(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.754
 Subarea runoff = 1.593(CFS) for 0.425(Ac.)
 Total runoff = 4.949(CFS) Total area = 1.256(Ac.)

 Process from Point/Station 127.000 to Point/Station 128.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.500(Ft.)
 Downstream point/station elevation = 691.000(Ft.)
 Pipe length = 34.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 4.949(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 4.949(CFS)
 Normal flow depth in pipe = 8.65(In.)
 Flow top width inside pipe = 14.82(In.)
 Critical Depth = 10.82(In.)
 Pipe flow velocity = 6.75(Ft/s)
 Travel time through pipe = 0.08 min.
 Time of concentration (TC) = 8.55 min.

 Process from Point/Station 128.000 to Point/Station 129.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 5.004(CFS)
 Depth of flow = 0.173(Ft.), Average velocity = 1.421(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	2.50
2	5.00	0.00
3	25.00	0.00
4	30.00	2.50

 Manning's 'N' friction factor = 0.030

Sub-Channel flow = 5.004(CFS)
 ' ' flow top width = 20.692(Ft.)
 ' ' velocity = 1.421(Ft/s)
 ' ' area = 3.521(Sq.Ft)
 ' ' Froude number = 0.607

Upstream point elevation = 691.000(Ft.)
 Downstream point elevation = 690.500(Ft.)

Flow rate for Pond E

```

Flow length =      57.000(Ft.)
Travel time =      0.67 min.
Time of concentration =      9.22 min.
Depth of flow =      0.173(Ft.)
Average velocity =      1.421(Ft/s)
Total irregular channel flow =      5.004(CFS)
Irregular channel normal depth above invert elev. =      0.173(Ft.)
Average velocity of channel(s) =      1.421(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL                                ]
(10.9 DU/A or Less                                         )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity =      6.216(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA =      0.802
Subarea runoff =      0.038(CFS) for      0.081(Ac.)
Total runoff =      4.987(CFS)      Total area =      1.337(Ac.)
Depth of flow =      0.173(Ft.), Average velocity =      1.419(Ft/s)

+++++
Process from Point/Station      129.000 to Point/Station      130.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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Upstream point/station elevation =      690.500(Ft.)
Downstream point/station elevation =      689.000(Ft.)
Pipe length =      134.00(Ft.)      Manning's N = 0.013
No. of pipes = 1      Required pipe flow =      4.987(CFS)
Nearest computed pipe diameter =      15.00(In.)
Calculated individual pipe flow =      4.987(CFS)
Normal flow depth in pipe =      9.52(In.)
Flow top width inside pipe =      14.45(In.)
Critical Depth =      10.86(In.)
Pipe flow velocity =      6.08(Ft/s)
Travel time through pipe =      0.37 min.
Time of concentration (TC) =      9.58 min.
End of computations, total study area =      1.337 (Ac.)

```

Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 8:37 AM

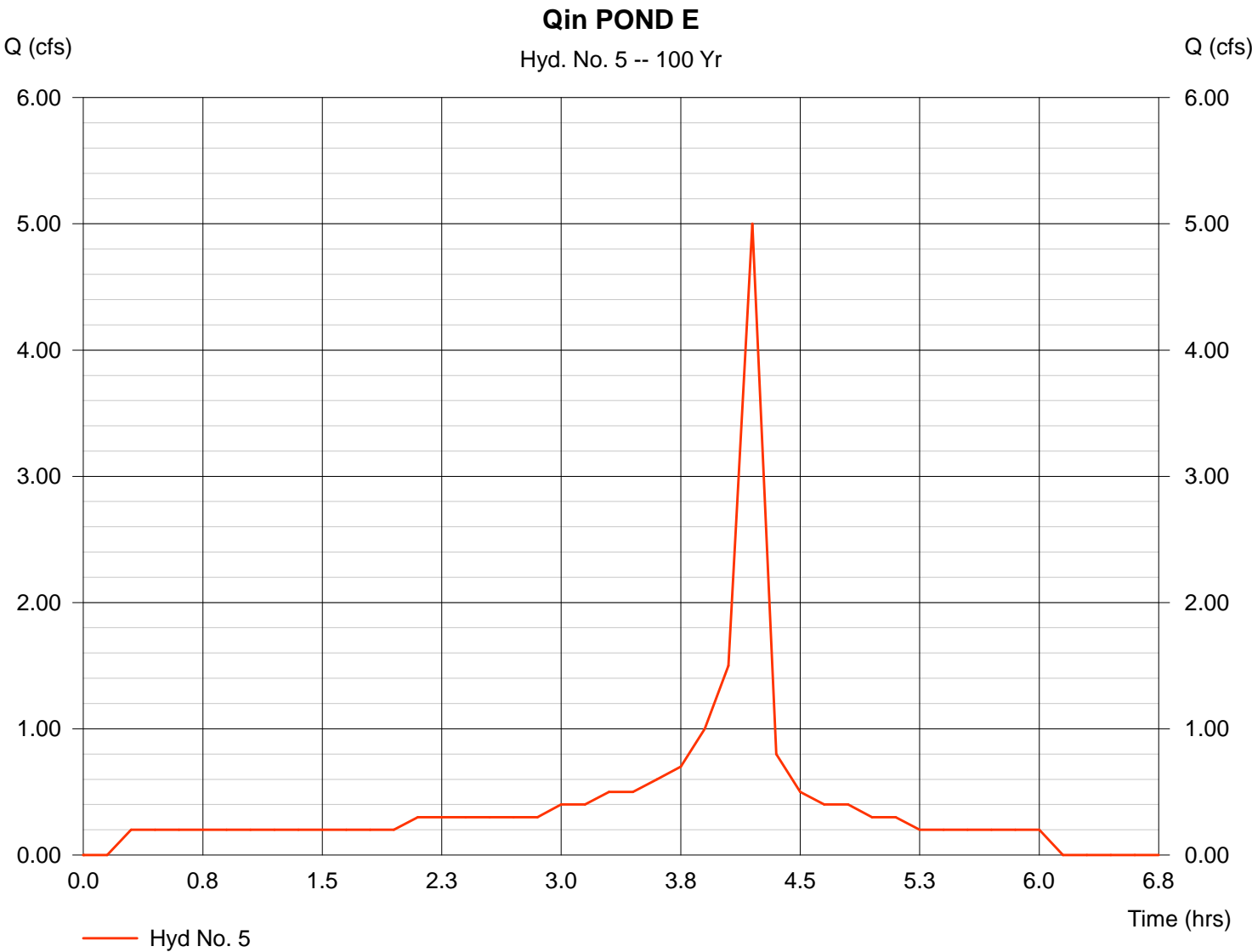
Hyd. No. 5

Qin POND E

Hydrograph type = Manual
Storm frequency = 100 yrs

Peak discharge = 5.00 cfs
Time interval = 9 min

Hydrograph Volume = 10,098 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 8:43 AM

Hyd. No. 6

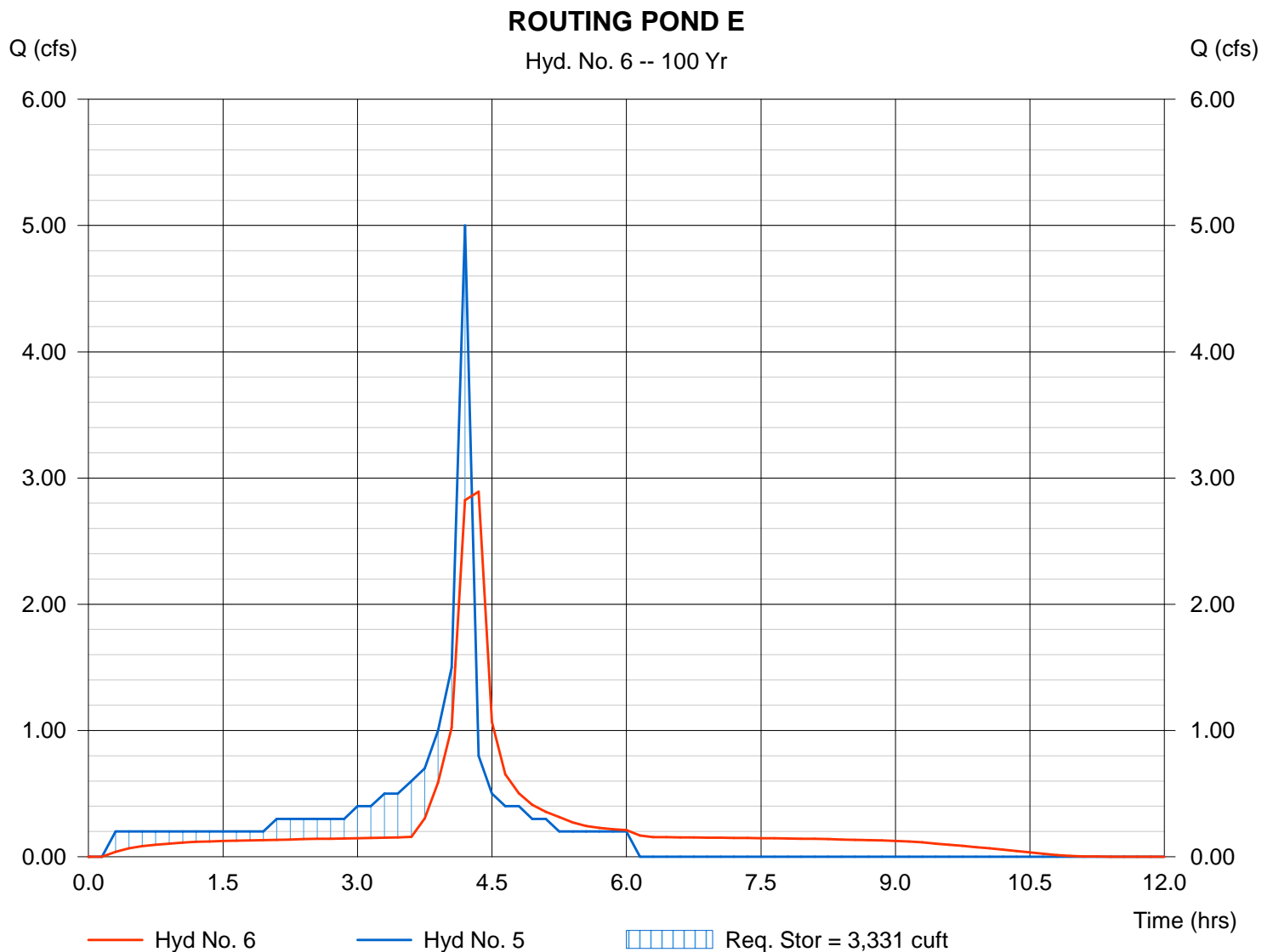
ROUTING POND E

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 5
Reservoir name = POND E - STREET B

Peak discharge = 2.89 cfs
Time interval = 9 min
Max. Elevation = 692.55 ft
Max. Storage = 3,331 cuft

Storage Indication method used.

Hydrograph Volume = 10,097 cuft



Pond Report

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 8:57 AM

Pond No. 4 - POND E - STREET B

Pond Data

Pond storage is based on known values

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	687.00	00	0	0
2.00	689.00	00	179	179
4.00	691.00	00	205	384
4.50	691.50	00	547	931
5.00	692.00	00	1,033	1,964
6.00	693.00	00	2,484	4,448
6.50	693.50	00	1,457	5,905

Culvert / Orifice Structures

	[A]	[B]	[C]	[D]
Rise (in)	= 12.00	1.50	1.00	0.00
Span (in)	= 12.00	1.50	1.00	0.00
No. Barrels	= 1	1	1	0
Invert El. (ft)	= 686.50	687.00	691.00	0.00
Length (ft)	= 122.00	0.00	0.00	0.00
Slope (%)	= 1.00	0.00	0.00	0.00
N-Value	= .013	.013	.013	.000
Orif. Coeff.	= 0.60	0.60	0.60	0.00
Multi-Stage	= n/a	Yes	Yes	No

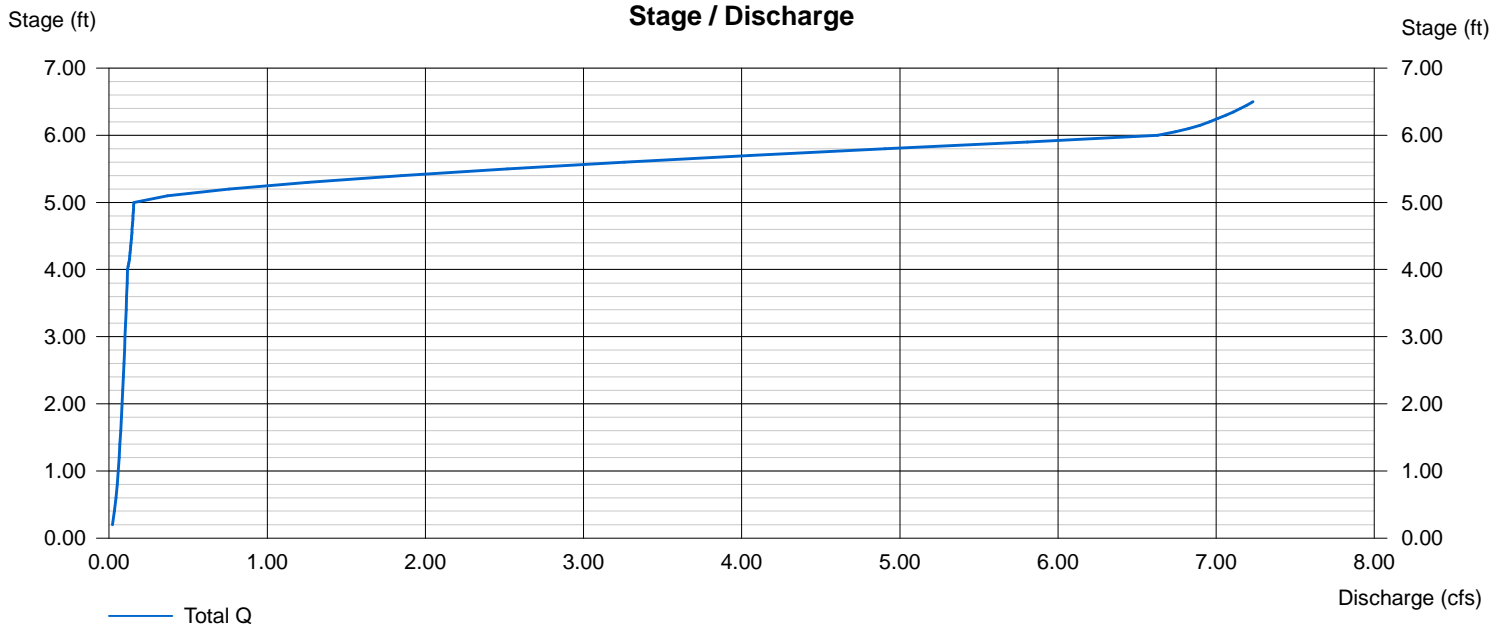
Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 2.00	0.00	0.00	0.00
Crest El. (ft)	= 692.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	0.00	0.00	0.00
Weir Type	= Riser	---	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Wet area) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Discharge



San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 01/31/13

***** Hydrology Study Control Information *****

File: 12052WQF.rd

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 131.000 to Point/Station 132.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 138.000(Ft.)
Highest elevation = 717.000(Ft.)
Lowest elevation = 716.000(Ft.)
Elevation difference = 1.000(Ft.) Slope = 0.725 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 50.00 (Ft)
for the top area slope value of 0.72 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 7.08 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (50.000^{.5})] / (0.725^{(1/3)}) = 7.08$
Rainfall intensity (I) = 7.366(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.742(CFS)
Total initial stream area = 0.168(Ac.)

Process from Point/Station 132.000 to Point/Station 133.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 714.000(Ft.)
Downstream point/station elevation = 712.000(Ft.)
Pipe length = 135.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.742(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.742(CFS)
Normal flow depth in pipe = 3.79(In.)
Flow top width inside pipe = 8.89(In.)
Critical Depth = 4.71(In.)
Pipe flow velocity = 4.21(Ft/s)
Travel time through pipe = 0.53 min.
Time of concentration (TC) = 7.62 min.

Flow rate for Pond F

++++++
 Process from Point/Station 133.000 to Point/Station 133.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.62 min.
 Rainfall intensity = 7.028(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.218
 Subarea runoff = 0.793(CFS) for 0.196(Ac.)
 Total runoff = 1.535(CFS) Total area = 0.364(Ac.)

++++++
 Process from Point/Station 133.000 to Point/Station 134.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 712.000(Ft.)
 Downstream point/station elevation = 709.400(Ft.)
 Pipe length = 85.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.535(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.535(CFS)
 Normal flow depth in pipe = 4.66(In.)
 Flow top width inside pipe = 8.99(In.)
 Critical Depth = 6.84(In.)
 Pipe flow velocity = 6.65(Ft/s)
 Travel time through pipe = 0.21 min.
 Time of concentration (TC) = 7.83 min.

++++++
 Process from Point/Station 134.000 to Point/Station 134.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 7.83 min.
 Rainfall intensity = 6.904(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.380
 Subarea runoff = 1.091(CFS) for 0.270(Ac.)
 Total runoff = 2.626(CFS) Total area = 0.634(Ac.)

++++++
 Process from Point/Station 134.000 to Point/Station 135.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 709.400(Ft.)
 Downstream point/station elevation = 701.500(Ft.)
 Pipe length = 152.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.626(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 2.626(CFS)
 Normal flow depth in pipe = 5.53(In.)
 Flow top width inside pipe = 8.76(In.)
 Critical Depth = 8.42(In.)

Flow rate for Pond F

Pipe flow velocity = 9.23(Ft/s)
Travel time through pipe = 0.27 min.
Time of concentration (TC) = 8.11 min.

Process from Point/Station 135.000 to Point/Station 135.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.11 min.
Rainfall intensity = 6.753(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.477
Subarea runoff = 0.595(CFS) for 0.161(Ac.)
Total runoff = 3.221(CFS) Total area = 0.795(Ac.)

Process from Point/Station 135.000 to Point/Station 136.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 701.500(Ft.)
Downstream point/station elevation = 699.600(Ft.)
Pipe length = 154.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.221(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.221(CFS)
Normal flow depth in pipe = 8.23(In.)
Flow top width inside pipe = 11.14(In.)
Critical Depth = 9.23(In.)
Pipe flow velocity = 5.62(Ft/s)
Travel time through pipe = 0.46 min.
Time of concentration (TC) = 8.56 min.

Process from Point/Station 136.000 to Point/Station 136.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.56 min.
Rainfall intensity = 6.518(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.701
Subarea runoff = 1.347(CFS) for 0.373(Ac.)
Total runoff = 4.568(CFS) Total area = 1.168(Ac.)

Process from Point/Station 136.000 to Point/Station 137.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 699.600(Ft.)
Downstream point/station elevation = 694.400(Ft.)
Pipe length = 130.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 4.568(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 4.568(CFS)

Flow rate for Pond F

Normal flow depth in pipe = 6.98(In.)
 Flow top width inside pipe = 11.84(In.)
 Critical Depth = 10.70(In.)
 Pipe flow velocity = 9.63(Ft/s)
 Travel time through pipe = 0.23 min.
 Time of concentration (TC) = 8.79 min.

 Process from Point/Station 137.000 to Point/Station 137.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.79 min.
 Rainfall intensity = 6.410(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.932
 Subarea runoff = 1.409(CFS) for 0.386(Ac.)
 Total runoff = 5.976(CFS) Total area = 1.554(Ac.)

 Process from Point/Station 137.000 to Point/Station 138.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 694.400(Ft.)
 Downstream point/station elevation = 694.200(Ft.)
 Pipe length = 9.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 5.976(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 5.976(CFS)
 Normal flow depth in pipe = 8.55(In.)
 Flow top width inside pipe = 14.85(In.)
 Critical Depth = 11.87(In.)
 Pipe flow velocity = 8.27(Ft/s)
 Travel time through pipe = 0.02 min.
 Time of concentration (TC) = 8.81 min.

 Process from Point/Station 138.000 to Point/Station 139.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 6.088(CFS)
 Depth of flow = 0.166(Ft.), Average velocity = 1.210(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	2.50
2	5.00	0.00
3	35.00	0.00
4	40.00	2.50

 Manning's 'N' friction factor = 0.030

Sub-Channel flow = 6.088(CFS)

'	'	flow top width = 30.663(Ft.)
'	'	velocity = 1.210(Ft/s)
'	'	area = 5.031(Sq.Ft)
'	'	Froude number = 0.526

Upstream point elevation = 694.200(Ft.)
 Downstream point elevation = 694.000(Ft.)
 Flow length = 30.000(Ft.)
 Travel time = 0.41 min.
 Time of concentration = 9.22 min.

Flow rate for Pond F

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Depth of flow = 0.166(Ft.)
Average velocity = 1.210(Ft/s)
Total irregular channel flow = 6.088(CFS)
Irregular channel normal depth above invert elev. = 0.166(Ft.)
Average velocity of channel(s) = 1.210(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity = 6.215(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.982
Subarea runoff = 0.128(CFS) for 0.083(Ac.)
Total runoff = 6.104(CFS) Total area = 1.637(Ac.)
Depth of flow = 0.166(Ft.), Average velocity = 1.211(Ft/s)

+++++
Process from Point/Station 139.000 to Point/Station 130.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 692.000(Ft.)
Downstream point/station elevation = 689.000(Ft.)
Pipe length = 75.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 6.104(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 6.104(CFS)
Normal flow depth in pipe = 8.55(In.)
Flow top width inside pipe = 10.86(In.)
Critical depth could not be calculated.
Pipe flow velocity = 10.20(Ft/s)
Travel time through pipe = 0.12 min.
Time of concentration (TC) = 9.34 min.
End of computations, total study area = 1.637 (Ac.)

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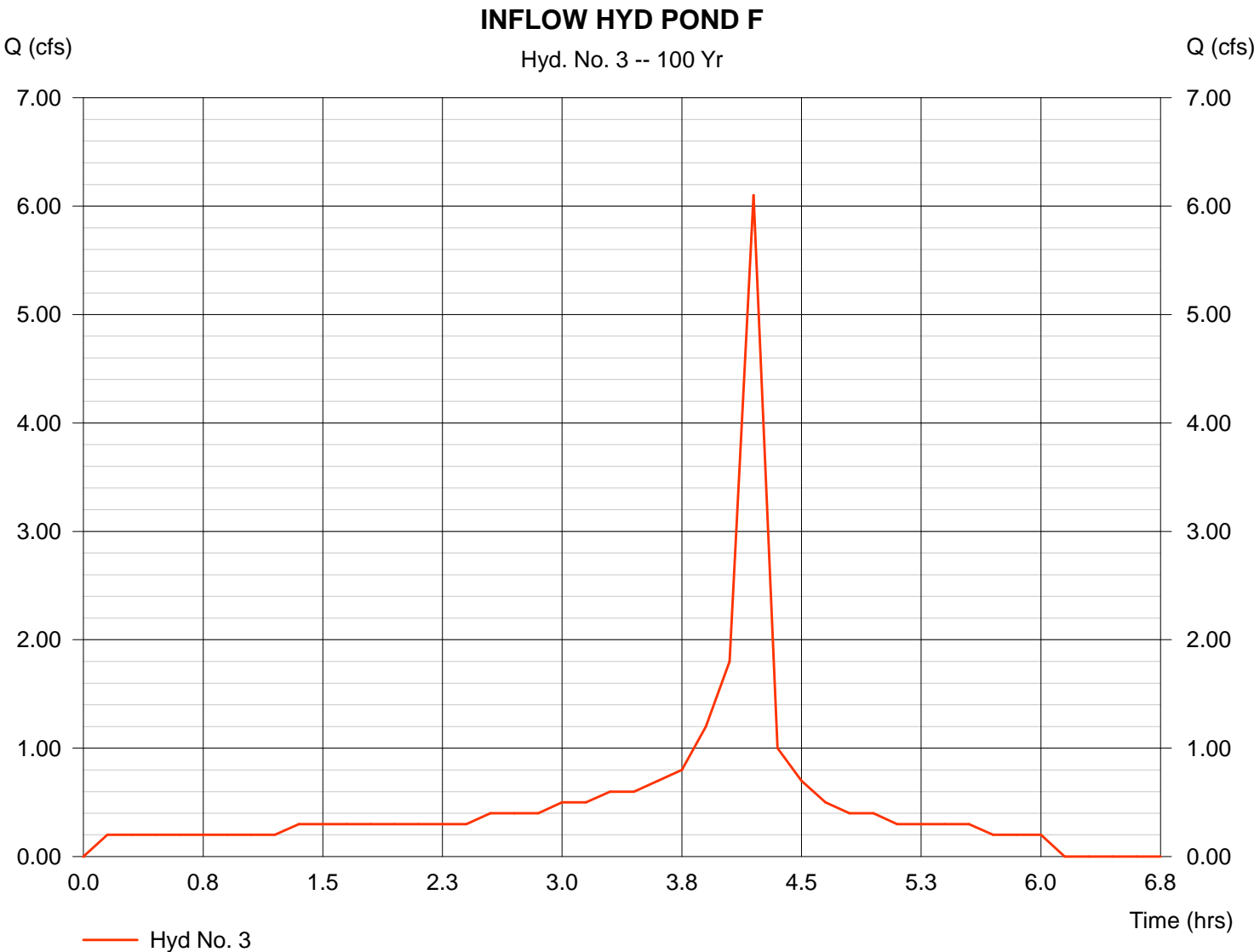
Hydrograph Plot

Hyd. No. 3

INFLOW HYD POND F

Hydrograph type	= Manual	Peak discharge	= 6.10 cfs
Storm frequency	= 100 yrs	Time interval	= 9 min

Hydrograph Volume = 12,312 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 9:15 AM

Hyd. No. 4

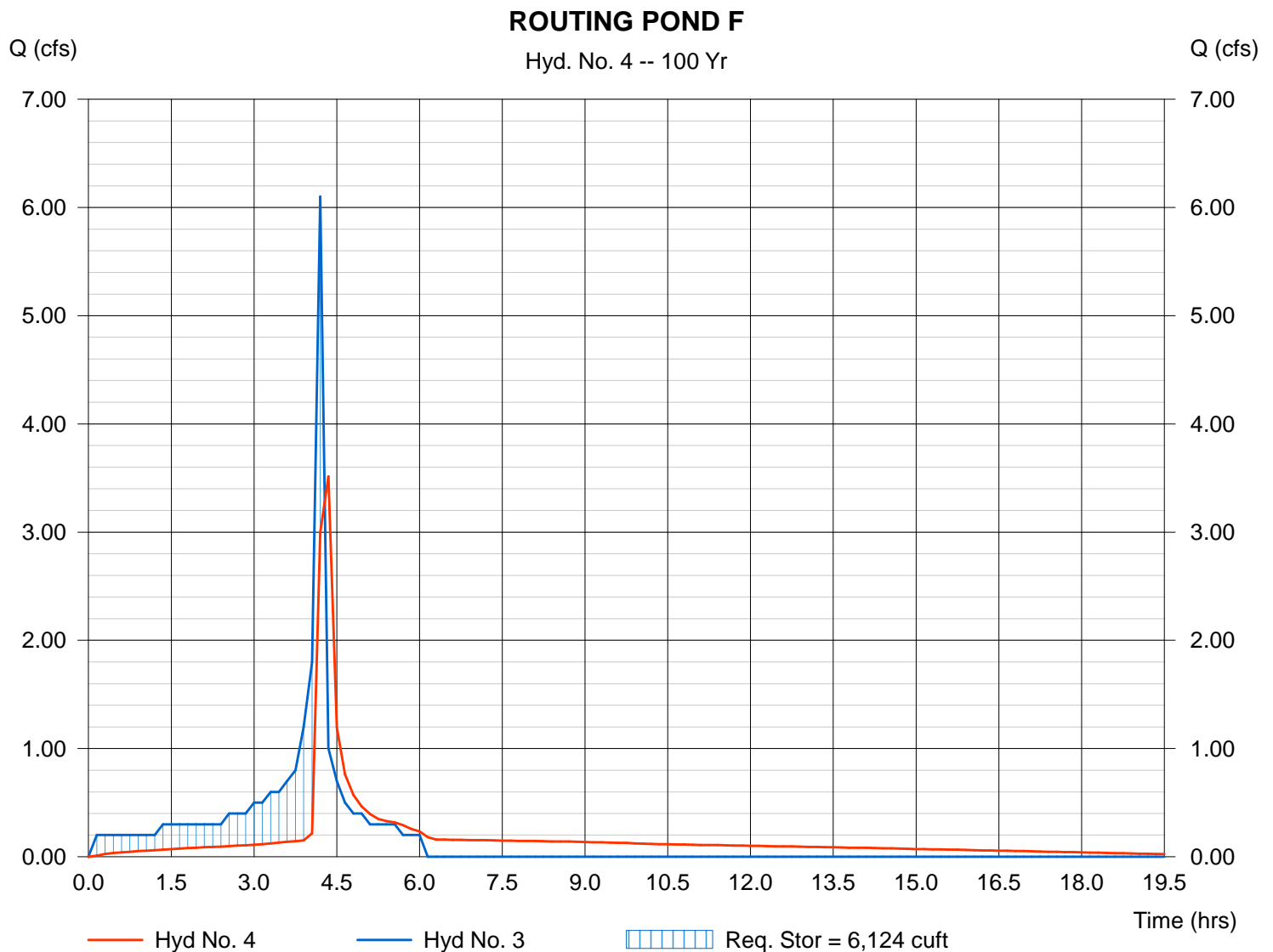
ROUTING POND F

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 3
Reservoir name = POND F - STREET B

Peak discharge = 3.51 cfs
Time interval = 9 min
Max. Elevation = 695.63 ft
Max. Storage = 6,124 cuft

Storage Indication method used.

Hydrograph Volume = 12,307 cuft



Pond Report

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 9:17 AM

Pond No. 2 - POND F - STREET B

Pond Data

Pond storage is based on known values

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	689.90	00	0	0
2.00	691.90	00	1,184	1,184
4.00	693.90	00	1,354	2,538
4.50	694.40	00	893	3,431
5.10	695.00	00	1,205	4,636
6.10	696.00	00	2,358	6,994

Culvert / Orifice Structures

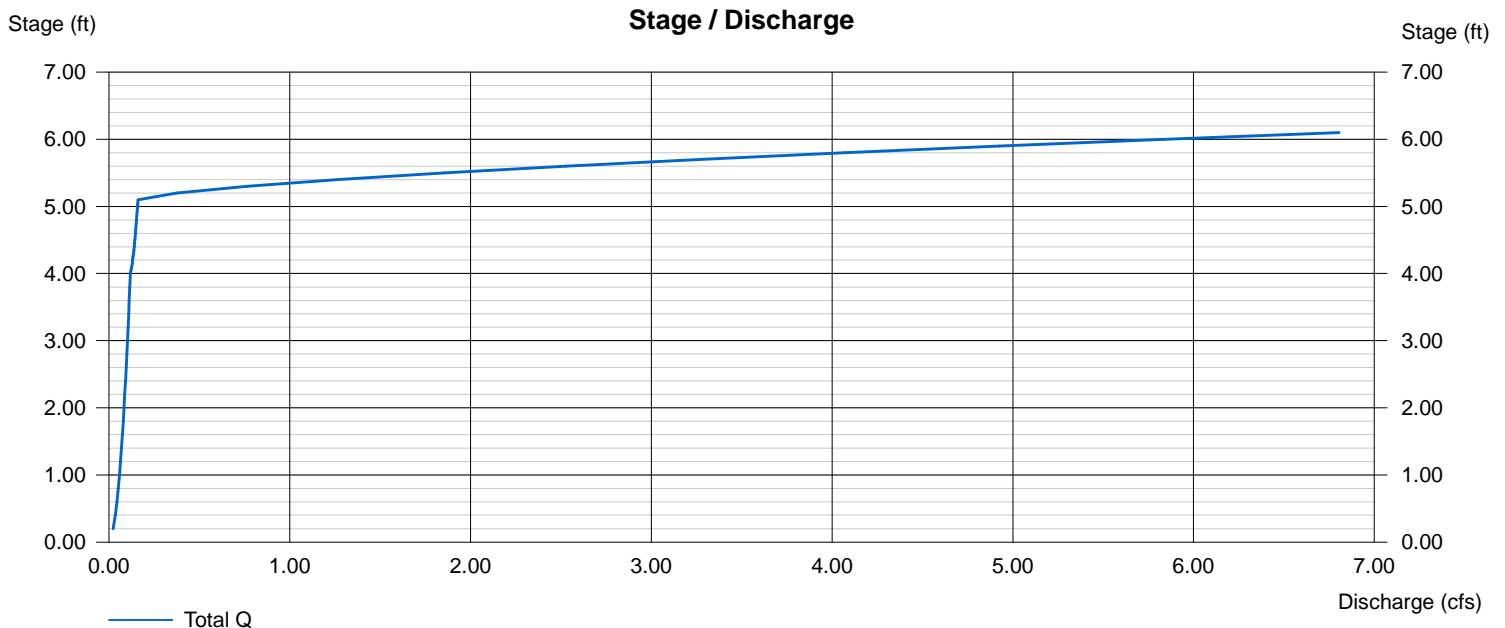
	[A]	[B]	[C]	[D]
Rise (in)	= 12.00	1.50	1.00	0.00
Span (in)	= 12.00	1.50	1.00	0.00
No. Barrels	= 1	1	1	0
Invert El. (ft)	= 689.00	689.90	693.90	0.00
Length (ft)	= 75.00	0.00	0.00	0.00
Slope (%)	= 5.60	0.00	0.00	0.00
N-Value	= .013	.013	.013	.000
Orif. Coeff.	= 0.60	0.60	0.60	0.00
Multi-Stage	= n/a	Yes	Yes	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 2.00	0.00	0.00	0.00
Crest El. (ft)	= 695.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	0.00	0.00	0.00
Weir Type	= Riser	---	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Wet area) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/14/13

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 31.000 to Point/Station 31.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.072(Ac.) Total runoff = 0.140(CFS)

Process from Point/Station 31.000 to Point/Station 32.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 698.500(Ft.)
Downstream point/station elevation = 693.300(Ft.)
Pipe length = 85.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.140(CFS)
Nearest computed pipe diameter = 3.00(In.)
Calculated individual pipe flow = 0.140(CFS)
Normal flow depth in pipe = 1.74(In.)
Flow top width inside pipe = 2.96(In.)
Critical Depth = 2.66(In.)
Pipe flow velocity = 4.72(Ft/s)
Travel time through pipe = 0.30 min.
Time of concentration (TC) = 12.30 min.

Process from Point/Station 32.000 to Point/Station 32.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.072(Ac.)
Runoff from this stream = 0.140(CFS)
Time of concentration = 12.30 min.
Rainfall intensity = 5.160(In/Hr)

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Process from Point/Station      32.000 to Point/Station      32.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) =      5.243(In/Hr) for a    100.0 year storm
User specified values are as follows:
TC =  12.00 min.  Rain intensity =      5.24(In/Hr)
Total area =      0.065(Ac.)  Total runoff =      0.140(CFS)

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Process from Point/Station      32.000 to Point/Station      32.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 2
Stream flow area =      0.065(Ac.)
Runoff from this stream =      0.140(CFS)
Time of concentration =  12.00 min.
Rainfall intensity =      5.243(In/Hr)
Summary of stream data:

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Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.140	12.30	5.160
2	0.140	12.00	5.243

Qmax(1) =
1.000 * 1.000 * 0.140) +
0.984 * 1.000 * 0.140) + = 0.278
Qmax(2) =
1.000 * 0.976 * 0.140) +
1.000 * 1.000 * 0.140) + = 0.277

```

Total of 2 streams to confluence:
Flow rates before confluence point:
0.140      0.140
Maximum flow rates at confluence using above data:
0.278      0.277
Area of streams before confluence:
0.072      0.065
Results of confluence:
Total flow rate =      0.278(CFS)
Time of concentration =  12.300 min.
Effective stream area after confluence =      0.137(Ac.)

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Process from Point/Station      32.000 to Point/Station      33.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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Upstream point/station elevation =  693.300(Ft.)
Downstream point/station elevation =  691.300(Ft.)
Pipe length =  85.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      0.278(CFS)
Nearest computed pipe diameter =      6.00(In.)
Calculated individual pipe flow =      0.278(CFS)
Normal flow depth in pipe =      2.35(In.)
Flow top width inside pipe =      5.86(In.)
Critical Depth =      3.19(In.)
Pipe flow velocity =      3.91(Ft/s)
Travel time through pipe =      0.36 min.
Time of concentration (TC) =      12.66 min.

```

Process from Point/Station 33.000 to Point/Station 33.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.137(Ac.)
Runoff from this stream = 0.278(CFS)
Time of concentration = 12.66 min.
Rainfall intensity = 5.064(In/Hr)

Process from Point/Station 33.000 to Point/Station 33.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.065(Ac.) Total runoff = 0.140(CFS)

Process from Point/Station 33.000 to Point/Station 34.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.300(Ft.)
Downstream point/station elevation = 690.800(Ft.)
Pipe length = 43.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.140(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.140(CFS)
Normal flow depth in pipe = 1.96(In.)
Flow top width inside pipe = 5.63(In.)
Critical Depth = 2.23(In.)
Pipe flow velocity = 2.51(Ft/s)
Travel time through pipe = 0.29 min.
Time of concentration (TC) = 12.29 min.

Process from Point/Station 34.000 to Point/Station 34.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 0.065(Ac.)
Runoff from this stream = 0.140(CFS)
Time of concentration = 12.29 min.
Rainfall intensity = 5.164(In/Hr)

Process from Point/Station 34.000 to Point/Station 34.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.038(Ac.) Total runoff = 0.070(CFS)

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*****
Process from Point/Station      34.000 to Point/Station      34.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 2

Stream flow area = 0.038(Ac.)
 Runoff from this stream = 0.070(CFS)
 Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.140	12.29	5.164
2	0.070	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 0.140) +
 0.985 * 1.000 * 0.070) + = 0.209

Qmax(2) =
 1.000 * 0.977 * 0.140) +
 1.000 * 1.000 * 0.070) + = 0.207

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.140 0.070

Maximum flow rates at confluence using above data:
 0.209 0.207

Area of streams before confluence:
 0.065 0.038

Results of confluence:
 Total flow rate = 0.209(CFS)
 Time of concentration = 12.286 min.
 Effective stream area after confluence = 0.103(Ac.)

```

*****
Process from Point/Station      34.000 to Point/Station      39.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 690.800(Ft.)
 Downstream point/station elevation = 688.000(Ft.)
 Pipe length = 3.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.209(CFS)
 Nearest computed pipe diameter = 3.00(In.)
 Calculated individual pipe flow = 0.209(CFS)
 Normal flow depth in pipe = 1.01(In.)
 Flow top width inside pipe = 2.84(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 14.38(Ft/s)
 Travel time through pipe = 0.00 min.
 Time of concentration (TC) = 12.29 min.

```

*****
Process from Point/Station      39.000 to Point/Station      39.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 0.103(Ac.)
 Runoff from this stream = 0.209(CFS)
 Time of concentration = 12.29 min.
 Rainfall intensity = 5.163(In/Hr)

Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.140	12.37	5.142
2	0.140	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 0.140) +
 0.981 * 1.000 * 0.140) + = 0.277

Qmax(2) =
 1.000 * 0.970 * 0.140) +
 1.000 * 1.000 * 0.140) + = 0.276

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.140 0.140
 Maximum flow rates at confluence using above data:
 0.277 0.276
 Area of streams before confluence:
 0.073 0.068
 Results of confluence:
 Total flow rate = 0.277(CFS)
 Time of concentration = 12.368 min.
 Effective stream area after confluence = 0.141(Ac.)

 Process from Point/Station 36.000 to Point/Station 37.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 695.000(Ft.)
 Downstream point/station elevation = 691.300(Ft.)
 Pipe length = 84.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.277(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.277(CFS)
 Normal flow depth in pipe = 1.98(In.)
 Flow top width inside pipe = 5.64(In.)
 Critical Depth = 3.19(In.)
 Pipe flow velocity = 4.90(Ft/s)
 Travel time through pipe = 0.29 min.
 Time of concentration (TC) = 12.65 min.

 Process from Point/Station 37.000 to Point/Station 37.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 12.00 min. Rain intensity = 5.24(In/Hr)
 Total area = 0.061(Ac.) Total runoff = 0.140(CFS)

 Process from Point/Station 37.000 to Point/Station 37.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.061(Ac.)

Runoff from this stream = 0.140(CFS)
 Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.140	12.37	5.142
2	0.140	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 0.140) +
 0.981 * 1.000 * 0.140) + = 0.277
 Qmax(2) =
 1.000 * 0.970 * 0.140) +
 1.000 * 1.000 * 0.140) + = 0.276

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.140 0.140
 Maximum flow rates at confluence using above data:
 0.277 0.276
 Area of streams before confluence:
 0.073 0.061
 Results of confluence:
 Total flow rate = 0.277(CFS)
 Time of concentration = 12.368 min.
 Effective stream area after confluence = 0.134(Ac.)

 Process from Point/Station 37.000 to Point/Station 38.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.300(Ft.)
 Downstream point/station elevation = 689.300(Ft.)
 Pipe length = 84.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.277(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.277(CFS)
 Normal flow depth in pipe = 2.34(In.)
 Flow top width inside pipe = 5.85(In.)
 Critical Depth = 3.19(In.)
 Pipe flow velocity = 3.93(Ft/s)
 Travel time through pipe = 0.36 min.
 Time of concentration (TC) = 12.72 min.

 Process from Point/Station 38.000 to Point/Station 38.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.134(Ac.)
 Runoff from this stream = 0.277(CFS)
 Time of concentration = 12.72 min.
 Rainfall intensity = 5.048(In/Hr)

 Process from Point/Station 38.000 to Point/Station 38.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600

Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 12.00 min. Rain intensity = 5.24(In/Hr)
 Total area = 0.040(Ac.) Total runoff = 0.140(CFS)

 Process from Point/Station 38.000 to Point/Station 38.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.040(Ac.)
 Runoff from this stream = 0.140(CFS)
 Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.277	12.72	5.048
2	0.140	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 0.277) +
 0.963 * 1.000 * 0.140) + = 0.412
 Qmax(2) =
 1.000 * 0.943 * 0.277) +
 1.000 * 1.000 * 0.140) + = 0.402

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.277 0.140
 Maximum flow rates at confluence using above data:
 0.412 0.402
 Area of streams before confluence:
 0.134 0.040
 Results of confluence:
 Total flow rate = 0.412(CFS)
 Time of concentration = 12.725 min.
 Effective stream area after confluence = 0.174(Ac.)

 Process from Point/Station 38.000 to Point/Station 39.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 689.300(Ft.)
 Downstream point/station elevation = 688.000(Ft.)
 Pipe length = 33.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.412(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.412(CFS)
 Normal flow depth in pipe = 2.52(In.)
 Flow top width inside pipe = 5.92(In.)
 Critical Depth = 3.92(In.)
 Pipe flow velocity = 5.24(Ft/s)
 Travel time through pipe = 0.10 min.
 Time of concentration (TC) = 12.83 min.

 Process from Point/Station 39.000 to Point/Station 39.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.174(Ac.)
 Runoff from this stream = 0.412(CFS)
 Time of concentration = 12.83 min.
 Rainfall intensity = 5.022(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.277	12.72	5.048
2	0.412	12.83	5.022

Qmax(1) =
 1.000 * 1.000 * 0.277) +
 1.000 * 0.992 * 0.412) + = 0.686
 Qmax(2) =
 0.995 * 1.000 * 0.277) +
 1.000 * 1.000 * 0.412) + = 0.688

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.277 0.412
 Maximum flow rates at confluence using above data:
 0.686 0.688
 Area of streams before confluence:
 0.134 0.174
 Results of confluence:
 Total flow rate = 0.688(CFS)
 Time of concentration = 12.830 min.
 Effective stream area after confluence = 0.308(Ac.)

 Process from Point/Station 39.000 to Point/Station 130.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
 Downstream point/station elevation = 685.700(Ft.)
 Pipe length = 128.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.688(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.688(CFS)
 Normal flow depth in pipe = 4.51(In.)
 Flow top width inside pipe = 5.18(In.)
 Critical Depth = 5.03(In.)
 Pipe flow velocity = 4.34(Ft/s)
 Travel time through pipe = 0.49 min.
 Time of concentration (TC) = 13.32 min.

 Process from Point/Station 130.000 to Point/Station 130.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.308(Ac.)
 Runoff from this stream = 0.688(CFS)
 Time of concentration = 13.32 min.
 Rainfall intensity = 4.901(In/Hr)

 Process from Point/Station 139.000 to Point/Station 139.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 4.036(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 18.00 min. Rain intensity = 4.04(In/Hr)
 Total area = 1.640(Ac.) Total runoff = 3.510(CFS)

Process from Point/Station 139.000 to Point/Station 130.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 689.900(Ft.)
Downstream point/station elevation = 685.700(Ft.)
Pipe length = 75.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.510(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 3.510(CFS)
Normal flow depth in pipe = 6.66(In.)
Flow top width inside pipe = 7.90(In.)
Critical depth could not be calculated.
Pipe flow velocity = 10.02(Ft/s)
Travel time through pipe = 0.12 min.
Time of concentration (TC) = 18.12 min.

Process from Point/Station 130.000 to Point/Station 130.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 1.640(Ac.)
Runoff from this stream = 3.510(CFS)
Time of concentration = 18.12 min.
Rainfall intensity = 4.018(In/Hr)

Process from Point/Station 129.000 to Point/Station 129.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 4.036(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 18.00 min. Rain intensity = 4.04(In/Hr)
Total area = 1.340(Ac.) Total runoff = 2.890(CFS)

Process from Point/Station 129.000 to Point/Station 130.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
Downstream point/station elevation = 685.700(Ft.)
Pipe length = 123.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.890(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 2.890(CFS)
Normal flow depth in pipe = 8.04(In.)
Flow top width inside pipe = 11.29(In.)
Critical Depth = 8.75(In.)
Pipe flow velocity = 5.17(Ft/s)
Travel time through pipe = 0.40 min.
Time of concentration (TC) = 18.40 min.

Process from Point/Station 130.000 to Point/Station 130.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 1.340(Ac.)

Runoff from this stream = 2.890(CFS)
 Time of concentration = 18.40 min.
 Rainfall intensity = 3.980(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.688	13.32	4.901
2	3.510	18.12	4.018
3	2.890	18.40	3.980

Qmax(1) =
 1.000 * 1.000 * 0.688) +
 1.000 * 0.735 * 3.510) +
 1.000 * 0.724 * 2.890) + = 5.360
 Qmax(2) =
 0.820 * 1.000 * 0.688) +
 1.000 * 1.000 * 3.510) +
 1.000 * 0.985 * 2.890) + = 6.921
 Qmax(3) =
 0.812 * 1.000 * 0.688) +
 0.990 * 1.000 * 3.510) +
 1.000 * 1.000 * 2.890) + = 6.925

Total of 3 streams to confluence:
 Flow rates before confluence point:
 0.688 3.510 2.890
 Maximum flow rates at confluence using above data:
 5.360 6.921 6.925
 Area of streams before confluence:
 0.308 1.640 1.340
 Results of confluence:
 Total flow rate = 6.925(CFS)
 Time of concentration = 18.397 min.
 Effective stream area after confluence = 3.288(Ac.)

 Process from Point/Station 130.000 to Point/Station 42.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.700(Ft.)
 Downstream point/station elevation = 684.700(Ft.)
 Pipe length = 92.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 6.925(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 6.925(CFS)
 Normal flow depth in pipe = 10.38(In.)
 Flow top width inside pipe = 17.79(In.)
 Critical Depth = 12.22(In.)
 Pipe flow velocity = 6.56(Ft/s)
 Travel time through pipe = 0.23 min.
 Time of concentration (TC) = 18.63 min.

 Process from Point/Station 42.000 to Point/Station 42.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 3.288(Ac.)
 Runoff from this stream = 6.925(CFS)
 Time of concentration = 18.63 min.
 Rainfall intensity = 3.948(In/Hr)

 Process from Point/Station 40.000 to Point/Station 40.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000

```

Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) =      5.243(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  12.00 min.  Rain intensity =      5.24(In/Hr)
Total area =      0.173(Ac.)  Total runoff =      0.210(CFS)

+++++
Process from Point/Station      40.000 to Point/Station      42.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation =  685.500(Ft.)
Downstream point/station elevation =  684.700(Ft.)
Pipe length =  12.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      0.210(CFS)
Nearest computed pipe diameter =      3.00(In.)
Calculated individual pipe flow =      0.210(CFS)
Normal flow depth in pipe =      2.27(In.)
Flow top width inside pipe =      2.58(In.)
Critical depth could not be calculated.
Pipe flow velocity =      5.27(Ft/s)
Travel time through pipe =      0.04 min.
Time of concentration (TC) =      12.04 min.

+++++
Process from Point/Station      42.000 to Point/Station      42.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area =      0.173(Ac.)
Runoff from this stream =      0.210(CFS)
Time of concentration =      12.04 min.
Rainfall intensity =      5.232(In/Hr)

+++++
Process from Point/Station      41.000 to Point/Station      41.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) =      5.243(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  12.00 min.  Rain intensity =      5.24(In/Hr)
Total area =      0.175(Ac.)  Total runoff =      0.210(CFS)

+++++
Process from Point/Station      41.000 to Point/Station      42.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation =  685.500(Ft.)
Downstream point/station elevation =  684.700(Ft.)
Pipe length =  38.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      0.210(CFS)
Nearest computed pipe diameter =      6.00(In.)
Calculated individual pipe flow =      0.210(CFS)
Normal flow depth in pipe =      2.08(In.)
Flow top width inside pipe =      5.71(In.)
Critical Depth =      2.76(In.)

```

Pipe flow velocity = 3.48(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 12.18 min.

 Process from Point/Station 42.000 to Point/Station 42.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 0.175(Ac.)
 Runoff from this stream = 0.210(CFS)
 Time of concentration = 12.18 min.
 Rainfall intensity = 5.192(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	6.925	18.63	3.948
2	0.210	12.04	5.232
3	0.210	12.18	5.192

Qmax(1) =
 1.000 * 1.000 * 6.925 +
 0.755 * 1.000 * 0.210 +
 0.760 * 1.000 * 0.210 + = 7.243

Qmax(2) =
 1.000 * 0.646 * 6.925 +
 1.000 * 1.000 * 0.210 +
 1.000 * 0.988 * 0.210 + = 4.892

Qmax(3) =
 1.000 * 0.654 * 6.925 +
 0.992 * 1.000 * 0.210 +
 1.000 * 1.000 * 0.210 + = 4.947

Total of 3 streams to confluence:
 Flow rates before confluence point:
 6.925 0.210 0.210
 Maximum flow rates at confluence using above data:
 7.243 4.892 4.947
 Area of streams before confluence:
 3.288 0.173 0.175
 Results of confluence:
 Total flow rate = 7.243(CFS)
 Time of concentration = 18.631 min.
 Effective stream area after confluence = 3.636(Ac.)

 Process from Point/Station 42.000 to Point/Station 43.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 684.700(Ft.)
 Downstream point/station elevation = 684.000(Ft.)
 Pipe length = 52.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 7.243(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 7.243(CFS)
 Normal flow depth in pipe = 11.86(In.)
 Flow top width inside pipe = 12.21(In.)
 Critical Depth = 12.90(In.)
 Pipe flow velocity = 6.96(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 18.76 min.
 End of computations, total study area = 3.810 (Ac.)

```

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13
-----
***** Hydrology Study Control Information *****
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Program License Serial Number 4012

-----
Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

*****
Process from Point/Station 80.000 to Point/Station 52.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.810(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 8.00 min. Rain intensity = 6.81(In/Hr)
Total area = 50.718(Ac.) Total runoff = 131.200(CFS)

*****
Process from Point/Station 80.000 to Point/Station 52.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
-----
Upstream point/station elevation = 686.500(Ft.)
Downstream point/station elevation = 679.800(Ft.)
Pipe length = 322.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 131.200(CFS)
Nearest computed pipe diameter = 42.00(In.)
Calculated individual pipe flow = 131.200(CFS)
Normal flow depth in pipe = 31.27(In.)
Flow top width inside pipe = 36.64(In.)
Critical Depth = 39.79(In.)
Pipe flow velocity = 17.08(Ft/s)
Travel time through pipe = 0.31 min.
Time of concentration (TC) = 8.31 min.

*****
Process from Point/Station 52.000 to Point/Station 52.000
**** CONFLUENCE OF MINOR STREAMS ****
-----
Along Main Stream number: 1 in normal stream number 1
Stream flow area = 50.718(Ac.)
Runoff from this stream = 131.200(CFS)
Time of concentration = 8.31 min.

```

Street C – Before Detention

Rainfall intensity = 6.643(In/Hr)

Process from Point/Station 44.000 to Point/Station 45.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 87.000(Ft.)
Highest elevation = 696.000(Ft.)
Lowest elevation = 693.000(Ft.)
Elevation difference = 3.000(Ft.) Slope = 3.448 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.45 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.65 minutes
TC = $[1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5} / (\% \text{ slope}^{(1/3)})]$
TC = $[1.8 * (1.1 - 0.6000) * (90.000^{.5}) / (3.448^{(1/3)})] = 5.65$
Rainfall intensity (I) = 8.521(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.332(CFS)
Total initial stream area = 0.065(Ac.)

Process from Point/Station 45.000 to Point/Station 46.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.300(Ft.)
Downstream point/station elevation = 685.500(Ft.)
Pipe length = 84.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.332(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.332(CFS)
Normal flow depth in pipe = 3.38(In.)
Flow top width inside pipe = 5.95(In.)
Critical Depth = 3.50(In.)
Pipe flow velocity = 2.92(Ft/s)
Travel time through pipe = 0.48 min.
Time of concentration (TC) = 6.13 min.

Process from Point/Station 46.000 to Point/Station 46.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.13 min.
Rainfall intensity = 8.085(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.074
Subarea runoff = 0.269(CFS) for 0.059(Ac.)
Total runoff = 0.602(CFS) Total area = 0.124(Ac.)

```

*****
Process from Point/Station      46.000 to Point/Station      47.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 685.500(Ft.)
Downstream point/station elevation = 680.300(Ft.)
Pipe length = 86.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.602(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.602(CFS)
Normal flow depth in pipe = 2.77(In.)
Flow top width inside pipe = 5.98(In.)
Critical Depth = 4.73(In.)
Pipe flow velocity = 6.79(Ft/s)
Travel time through pipe = 0.21 min.
Time of concentration (TC) = 6.34 min.

```

```

*****
Process from Point/Station      47.000 to Point/Station      47.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.34 min.
Rainfall intensity = 7.911(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.113
Subarea runoff = 0.296(CFS) for 0.065(Ac.)
Total runoff = 0.897(CFS) Total area = 0.189(Ac.)

```

```

*****
Process from Point/Station      47.000 to Point/Station      52.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 680.300(Ft.)
Downstream point/station elevation = 679.800(Ft.)
Pipe length = 9.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.897(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.897(CFS)
Normal flow depth in pipe = 3.62(In.)
Flow top width inside pipe = 5.87(In.)
Critical Depth = 5.52(In.)
Pipe flow velocity = 7.24(Ft/s)
Travel time through pipe = 0.02 min.
Time of concentration (TC) = 6.36 min.

```

```

*****
Process from Point/Station      52.000 to Point/Station      52.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.189(Ac.)
Runoff from this stream = 0.897(CFS)
Time of concentration = 6.36 min.
Rainfall intensity = 7.894(In/Hr)

```

```

*****
Process from Point/Station      48.000 to Point/Station      49.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 71.000(Ft.)
Highest elevation = 696.000(Ft.)
Lowest elevation = 694.000(Ft.)
Elevation difference = 2.000(Ft.) Slope = 2.817 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 2.82 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.05 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3)]
TC = [1.8*(1.1-0.6000)*( 90.000^.5)/( 2.817^(1/3))]= 6.05
Rainfall intensity (I) = 8.159(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.259(CFS)
Total initial stream area = 0.053(Ac.)

+++++
Process from Point/Station 49.000 to Point/Station 50.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.300(Ft.)
Downstream point/station elevation = 684.300(Ft.)
Pipe length = 86.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.259(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.259(CFS)
Normal flow depth in pipe = 2.03(In.)
Flow top width inside pipe = 5.68(In.)
Critical Depth = 3.08(In.)
Pipe flow velocity = 4.42(Ft/s)
Travel time through pipe = 0.32 min.
Time of concentration (TC) = 6.37 min.

+++++
Process from Point/Station 50.000 to Point/Station 50.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.37 min.
Rainfall intensity = 7.888(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.070
Subarea runoff = 0.294(CFS) for 0.064(Ac.)
Total runoff = 0.554(CFS) Total area = 0.117(Ac.)

+++++
Process from Point/Station 50.000 to Point/Station 51.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 684.300(Ft.)
Downstream point/station elevation = 680.300(Ft.)
Pipe length = 108.00(Ft.) Manning's N = 0.013

```

No. of pipes = 1 Required pipe flow = 0.554(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.554(CFS)
 Normal flow depth in pipe = 3.05(In.)
 Flow top width inside pipe = 6.00(In.)
 Critical Depth = 4.55(In.)
 Pipe flow velocity = 5.54(Ft/s)
 Travel time through pipe = 0.33 min.
 Time of concentration (TC) = 6.69 min.

 Process from Point/Station 51.000 to Point/Station 51.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.69 min.
 Rainfall intensity = 7.639(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.119
 Subarea runoff = 0.358(CFS) for 0.082(Ac.)
 Total runoff = 0.912(CFS) Total area = 0.199(Ac.)

 Process from Point/Station 51.000 to Point/Station 52.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 680.300(Ft.)
 Downstream point/station elevation = 679.800(Ft.)
 Pipe length = 37.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.912(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 0.912(CFS)
 Normal flow depth in pipe = 4.37(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical Depth = 5.25(In.)
 Pipe flow velocity = 4.30(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 6.84 min.

 Process from Point/Station 52.000 to Point/Station 52.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 0.199(Ac.)
 Runoff from this stream = 0.912(CFS)
 Time of concentration = 6.84 min.
 Rainfall intensity = 7.535(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	131.200	8.31	6.643
2	0.897	6.36	7.894
3	0.912	6.84	7.535

Qmax(1) =
 1.000 * 1.000 * 131.200) +
 0.842 * 1.000 * 0.897) +
 0.882 * 1.000 * 0.912) + = 132.759

Street C – Before Detention

Qmax(2) =
 1.000 * 0.765 * 131.200) +
 1.000 * 1.000 * 0.897) +
 1.000 * 0.930 * 0.912) + = 102.148

Qmax(3) =
 1.000 * 0.822 * 131.200) +
 0.955 * 1.000 * 0.897) +
 1.000 * 1.000 * 0.912) + = 109.679

Total of 3 streams to confluence:
 Flow rates before confluence point:
 131.200 0.897 0.912
 Maximum flow rates at confluence using above data:
 132.759 102.148 109.679
 Area of streams before confluence:
 50.718 0.189 0.199
 Results of confluence:
 Total flow rate = 132.759(CFS)
 Time of concentration = 8.314 min.
 Effective stream area after confluence = 51.106(Ac.)

 Process from Point/Station 52.000 to Point/Station 53.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 679.800(Ft.)
 Downstream point/station elevation = 678.800(Ft.)
 Pipe length = 84.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 132.759(CFS)
 Nearest computed pipe diameter = 48.00(In.)
 Calculated individual pipe flow = 132.759(CFS)
 Normal flow depth in pipe = 33.89(In.)
 Flow top width inside pipe = 43.73(In.)
 Critical Depth = 41.29(In.)
 Pipe flow velocity = 13.99(Ft/s)
 Travel time through pipe = 0.10 min.
 Time of concentration (TC) = 8.41 min.

 Process from Point/Station 53.000 to Point/Station 53.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 51.106(Ac.)
 Runoff from this stream = 132.759(CFS)
 Time of concentration = 8.41 min.
 Rainfall intensity = 6.592(In/Hr)

 Process from Point/Station 47.000 to Point/Station 53.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 84.000(Ft.)
 Highest elevation = 687.000(Ft.)
 Lowest elevation = 684.000(Ft.)
 Elevation difference = 3.000(Ft.) Slope = 3.571 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 3.57 %, in a development type of
 10.9 DU/A or Less

Street C – Before Detention

In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.59 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.571^{(1/3)}) = 5.59$
Rainfall intensity (I) = 8.585(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.340(CFS)
Total initial stream area = 0.066(Ac.)

Process from Point/Station 53.000 to Point/Station 53.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.066(Ac.)
Runoff from this stream = 0.340(CFS)
Time of concentration = 5.59 min.
Rainfall intensity = 8.585(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	132.759	8.41	6.592
2	0.340	5.59	8.585

Qmax(1) =
1.000 * 1.000 * 132.759) +
0.768 * 1.000 * 0.340) + = 133.020
Qmax(2) =
1.000 * 0.664 * 132.759) +
1.000 * 1.000 * 0.340) + = 88.475

Total of 2 streams to confluence:
Flow rates before confluence point:
132.759 0.340
Maximum flow rates at confluence using above data:
133.020 88.475
Area of streams before confluence:
51.106 0.066
Results of confluence:
Total flow rate = 133.020(CFS)
Time of concentration = 8.414 min.
Effective stream area after confluence = 51.172(Ac.)

Process from Point/Station 53.000 to Point/Station 58.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 678.800(Ft.)
Downstream point/station elevation = 676.000(Ft.)
Pipe length = 30.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 133.020(CFS)
Nearest computed pipe diameter = 33.00(In.)
Calculated individual pipe flow = 133.020(CFS)
Normal flow depth in pipe = 22.80(In.)
Flow top width inside pipe = 30.50(In.)
Critical depth could not be calculated.
Pipe flow velocity = 30.37(Ft/s)
Travel time through pipe = 0.02 min.
Time of concentration (TC) = 8.43 min.

Process from Point/Station 58.000 to Point/Station 58.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 51.172(Ac.)

Street C – Before Detention

Runoff from this stream = 133.020(CFS)
 Time of concentration = 8.43 min.
 Rainfall intensity = 6.584(In/Hr)

 Process from Point/Station 51.000 to Point/Station 57.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 112.000(Ft.)
 Highest elevation = 687.000(Ft.)
 Lowest elevation = 683.000(Ft.)
 Elevation difference = 4.000(Ft.) Slope = 3.571 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 3.57 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.59 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.571^{(1/3)}) = 5.59$
 Rainfall intensity (I) = 8.585(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.438(CFS)
 Total initial stream area = 0.085(Ac.)

 Process from Point/Station 57.000 to Point/Station 58.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 678.500(Ft.)
 Downstream point/station elevation = 676.000(Ft.)
 Pipe length = 35.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.438(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.438(CFS)
 Normal flow depth in pipe = 2.22(In.)
 Flow top width inside pipe = 5.79(In.)
 Critical Depth = 4.05(In.)
 Pipe flow velocity = 6.63(Ft/s)
 Travel time through pipe = 0.09 min.
 Time of concentration (TC) = 5.67 min.

 Process from Point/Station 58.000 to Point/Station 58.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.085(Ac.)
 Runoff from this stream = 0.438(CFS)
 Time of concentration = 5.67 min.
 Rainfall intensity = 8.499(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	133.020	8.43	6.584
2	0.438	5.67	8.499

Qmax(1) =

Street C – Before Detention

```

      1.000 *      1.000 *      133.020) +
      0.775 *      1.000 *      0.438) + =      133.359
Qmax(2) =
      1.000 *      0.673 *      133.020) +
      1.000 *      1.000 *      0.438) + =      89.963

```

```

Total of 2 streams to confluence:
Flow rates before confluence point:
      133.020      0.438
Maximum flow rates at confluence using above data:
      133.359      89.963
Area of streams before confluence:
      51.172      0.085
Results of confluence:
Total flow rate =      133.359(CFS)
Time of concentration =      8.431 min.
Effective stream area after confluence =      51.257(Ac.)

```

```

*****
Process from Point/Station      58.000 to Point/Station      54.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      676.000(Ft.)
Downstream point/station elevation =      675.500(Ft.)
Pipe length =      56.00(Ft.)      Manning's N = 0.013
No. of pipes = 1      Required pipe flow =      133.359(CFS)
Nearest computed pipe diameter =      48.00(In.)
Calculated individual pipe flow =      133.359(CFS)
Normal flow depth in pipe =      38.63(In.)
Flow top width inside pipe =      38.06(In.)
Critical Depth =      41.36(In.)
Pipe flow velocity =      12.31(Ft/s)
Travel time through pipe =      0.08 min.
Time of concentration (TC) =      8.51 min.

```

```

*****
Process from Point/Station      54.000 to Point/Station      54.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 1
Stream flow area =      51.257(Ac.)
Runoff from this stream =      133.359(CFS)
Time of concentration =      8.51 min.
Rainfall intensity =      6.546(In/Hr)

```

```

*****
Process from Point/Station      53.000 to Point/Station      54.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance =      86.000(Ft.)
Highest elevation =      684.000(Ft.)
Lowest elevation =      681.000(Ft.)
Elevation difference =      3.000(Ft.) Slope =      3.488 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of      3.49 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration =      5.63 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^.5]/(% slope^(1/3))

```

Street C – Before Detention

```

TC = [1.8*(1.1-0.6000)*( 90.000^.5)/(( 3.488^(1/3))]= 5.63
Rainfall intensity (I) = 8.542(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.302(CFS)
Total initial stream area = 0.059(Ac.)

+++++
Process from Point/Station 54.000 to Point/Station 54.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.059(Ac.)
Runoff from this stream = 0.302(CFS)
Time of concentration = 5.63 min.
Rainfall intensity = 8.542(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 133.359 8.51 6.546
2 0.302 5.63 8.542
Qmax(1) =
1.000 * 1.000 * 133.359) +
0.766 * 1.000 * 0.302) + = 133.591
Qmax(2) =
1.000 * 0.662 * 133.359) +
1.000 * 1.000 * 0.302) + = 88.565

Total of 2 streams to confluence:
Flow rates before confluence point:
133.359 0.302
Maximum flow rates at confluence using above data:
133.591 88.565
Area of streams before confluence:
51.257 0.059
Results of confluence:
Total flow rate = 133.591(CFS)
Time of concentration = 8.507 min.
Effective stream area after confluence = 51.316(Ac.)

+++++
Process from Point/Station 54.000 to Point/Station 59.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 675.500(Ft.)
Downstream point/station elevation = 673.000(Ft.)
Pipe length = 80.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 133.591(CFS)
Nearest computed pipe diameter = 39.00(In.)
Calculated individual pipe flow = 133.591(CFS)
Normal flow depth in pipe = 29.34(In.)
Flow top width inside pipe = 33.67(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.95(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 8.57 min.

+++++
Process from Point/Station 59.000 to Point/Station 59.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 51.316(Ac.)
Runoff from this stream = 133.591(CFS)
Time of concentration = 8.57 min.
Rainfall intensity = 6.513(In/Hr)

```

 Process from Point/Station 54.000 to Point/Station 55.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 80.000(Ft.)
 Highest elevation = 681.000(Ft.)
 Lowest elevation = 678.000(Ft.)
 Elevation difference = 3.000(Ft.) Slope = 3.750 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 3.75 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.50 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.750^{(1/3)}) = 5.50$
 Rainfall intensity (I) = 8.676(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.333(CFS)
 Total initial stream area = 0.064(Ac.)

 Process from Point/Station 55.000 to Point/Station 59.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 673.500(Ft.)
 Downstream point/station elevation = 673.000(Ft.)
 Pipe length = 10.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.333(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.333(CFS)
 Normal flow depth in pipe = 2.11(In.)
 Flow top width inside pipe = 5.73(In.)
 Critical Depth = 3.51(In.)
 Pipe flow velocity = 5.41(Ft/s)
 Travel time through pipe = 0.03 min.
 Time of concentration (TC) = 5.53 min.

 Process from Point/Station 59.000 to Point/Station 59.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.064(Ac.)
 Runoff from this stream = 0.333(CFS)
 Time of concentration = 5.53 min.
 Rainfall intensity = 8.645(In/Hr)

 Process from Point/Station 57.000 to Point/Station 58.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)

Street C – Before Detention

Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 145.000(Ft.)
 Highest elevation = 683.000(Ft.)
 Lowest elevation = 678.000(Ft.)
 Elevation difference = 5.000(Ft.) Slope = 3.448 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 3.45 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.65 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.448^{(1/3)}) = 5.65$
 Rainfall intensity (I) = 8.521(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.552(CFS)
 Total initial stream area = 0.108(Ac.)

 Process from Point/Station 58.000 to Point/Station 59.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 673.500(Ft.)
 Downstream point/station elevation = 673.000(Ft.)
 Pipe length = 35.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.552(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.552(CFS)
 Normal flow depth in pipe = 4.15(In.)
 Flow top width inside pipe = 5.54(In.)
 Critical Depth = 4.54(In.)
 Pipe flow velocity = 3.81(Ft/s)
 Travel time through pipe = 0.15 min.
 Time of concentration (TC) = 5.80 min.

 Process from Point/Station 59.000 to Point/Station 59.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 0.108(Ac.)
 Runoff from this stream = 0.552(CFS)
 Time of concentration = 5.80 min.
 Rainfall intensity = 8.375(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	133.591	8.57	6.513
2	0.333	5.53	8.645
3	0.552	5.80	8.375
Qmax(1) =			
	1.000 *	1.000 *	133.591) +
	0.753 *	1.000 *	0.333) +
	0.778 *	1.000 *	0.552) + = 134.271
Qmax(2) =			
	1.000 *	0.645 *	133.591) +
	1.000 *	1.000 *	0.333) +
	1.000 *	0.952 *	0.552) + = 86.973
Qmax(3) =			
	1.000 *	0.677 *	133.591) +
	0.969 *	1.000 *	0.333) +
	1.000 *	1.000 *	0.552) + = 91.322

Total of 3 streams to confluence:
 Flow rates before confluence point:

Street C – Before Detention

Process from Point/Station 56.000 to Point/Station 62.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 664.300(Ft.)
Downstream point/station elevation = 663.000(Ft.)
Pipe length = 5.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.853(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.853(CFS)
Normal flow depth in pipe = 2.25(In.)
Flow top width inside pipe = 5.81(In.)
Critical Depth = 5.44(In.)
Pipe flow velocity = 12.72(Ft/s)
Travel time through pipe = 0.01 min.
Time of concentration (TC) = 5.83 min.

Process from Point/Station 62.000 to Point/Station 62.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.170(Ac.)
Runoff from this stream = 0.853(CFS)
Time of concentration = 5.83 min.
Rainfall intensity = 8.353(In/Hr)

Process from Point/Station 58.000 to Point/Station 60.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 102.000(Ft.)
Highest elevation = 678.000(Ft.)
Lowest elevation = 675.000(Ft.)
Elevation difference = 3.000(Ft.) Slope = 2.941 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 2.94 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.96 minutes
TC = $[1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{0.5}] / (\% \text{ slope}^{1/3})$
TC = $[1.8 * (1.1 - 0.6000) * (90.000^{0.5}) / (2.941^{1/3})] = 5.96$
Rainfall intensity (I) = 8.235(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.395(CFS)
Total initial stream area = 0.080(Ac.)

Process from Point/Station 60.000 to Point/Station 61.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 668.300(Ft.)
Downstream point/station elevation = 664.300(Ft.)
Pipe length = 88.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.395(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.395(CFS)
Normal flow depth in pipe = 2.37(In.)
Flow top width inside pipe = 5.87(In.)
Critical Depth = 3.84(In.)

Street C – Before Detention

Pipe flow velocity = 5.46(Ft/s)
 Travel time through pipe = 0.27 min.
 Time of concentration (TC) = 6.23 min.

 Process from Point/Station 61.000 to Point/Station 61.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 6.23 min.
 Rainfall intensity = 8.004(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.088
 Subarea runoff = 0.311(CFS) for 0.067(Ac.)
 Total runoff = 0.706(CFS) Total area = 0.147(Ac.)

 Process from Point/Station 61.000 to Point/Station 62.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 664.300(Ft.)
 Downstream point/station elevation = 663.000(Ft.)
 Pipe length = 38.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.706(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.706(CFS)
 Normal flow depth in pipe = 3.63(In.)
 Flow top width inside pipe = 5.87(In.)
 Critical Depth = 5.08(In.)
 Pipe flow velocity = 5.68(Ft/s)
 Travel time through pipe = 0.11 min.
 Time of concentration (TC) = 6.34 min.

 Process from Point/Station 62.000 to Point/Station 62.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 0.147(Ac.)
 Runoff from this stream = 0.706(CFS)
 Time of concentration = 6.34 min.
 Rainfall intensity = 7.913(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	134.271	8.74	6.434
2	0.853	5.83	8.353
3	0.706	6.34	7.913
Qmax(1) =			
	1.000 *	1.000 *	134.271) +
	0.770 *	1.000 *	0.853) +
	0.813 *	1.000 *	0.706) + = 135.502
Qmax(2) =			
	1.000 *	0.667 *	134.271) +
	1.000 *	1.000 *	0.853) +
	1.000 *	0.920 *	0.706) + = 91.088
Qmax(3) =			
	1.000 *	0.726 *	134.271) +

Street C – Before Detention

0.947 *	1.000 *	0.853) +	
1.000 *	1.000 *	0.706) + =	98.937

Total of 3 streams to confluence:
 Flow rates before confluence point:
 134.271 0.853 0.706
 Maximum flow rates at confluence using above data:
 135.502 91.088 98.937
 Area of streams before confluence:
 51.488 0.170 0.147
 Results of confluence:
 Total flow rate = 135.502(CFS)
 Time of concentration = 8.737 min.
 Effective stream area after confluence = 51.805(Ac.)

++++++
 Process from Point/Station 62.000 to Point/Station 29.100
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 663.000(Ft.)
 Downstream point/station elevation = 662.500(Ft.)
 Pipe length = 34.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 135.502(CFS)
 Nearest computed pipe diameter = 45.00(In.)
 Calculated individual pipe flow = 135.502(CFS)
 Normal flow depth in pipe = 34.13(In.)
 Flow top width inside pipe = 38.53(In.)
 Critical Depth = 41.17(In.)
 Pipe flow velocity = 15.07(Ft/s)
 Travel time through pipe = 0.04 min.
 Time of concentration (TC) = 8.77 min.
 End of computations, total study area = 51.805 (Ac.)

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San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13
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***** Hydrology Study Control Information *****
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File: D12052POSTC.RD3

Program License Serial Number 4012
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Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

*****
Process from Point/Station 80.000 to Point/Station 52.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.810(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 8.00 min. Rain intensity = 6.81(In/Hr)
Total area = 50.718(Ac.) Total runoff = 131.200(CFS)

*****
Process from Point/Station 80.000 to Point/Station 52.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
-----
Upstream point/station elevation = 686.500(Ft.)
Downstream point/station elevation = 679.800(Ft.)
Pipe length = 322.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 131.200(CFS)
Nearest computed pipe diameter = 42.00(In.)
Calculated individual pipe flow = 131.200(CFS)
Normal flow depth in pipe = 31.27(In.)
Flow top width inside pipe = 36.64(In.)
Critical Depth = 39.79(In.)
Pipe flow velocity = 17.08(Ft/s)
Travel time through pipe = 0.31 min.
Time of concentration (TC) = 8.31 min.

*****
Process from Point/Station 52.000 to Point/Station 52.000
**** CONFLUENCE OF MAIN STREAMS ****
-----
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 50.718(Ac.)
Runoff from this stream = 131.200(CFS)

```

Time of concentration = 8.31 min.
Rainfall intensity = 6.643(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 45.000 to Point/Station 45.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.066(Ac.) Total runoff = 0.140(CFS)

Process from Point/Station 45.000 to Point/Station 46.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.300(Ft.)
Downstream point/station elevation = 685.500(Ft.)
Pipe length = 84.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.140(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.140(CFS)
Normal flow depth in pipe = 2.07(In.)
Flow top width inside pipe = 5.70(In.)
Critical Depth = 2.23(In.)
Pipe flow velocity = 2.33(Ft/s)
Travel time through pipe = 0.60 min.
Time of concentration (TC) = 12.60 min.

Process from Point/Station 46.000 to Point/Station 46.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 0.066(Ac.)
Runoff from this stream = 0.140(CFS)
Time of concentration = 12.60 min.
Rainfall intensity = 5.080(In/Hr)

Process from Point/Station 46.000 to Point/Station 46.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.059(Ac.) Total runoff = 0.140(CFS)

Process from Point/Station 46.000 to Point/Station 46.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
Stream flow area = 0.059(Ac.)
Runoff from this stream = 0.140(CFS)
Time of concentration = 12.00 min.
Rainfall intensity = 5.243(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	0.140	12.60	5.080
2	0.140	12.00	5.243

Qmax(1) =
1.000 * 1.000 * 0.140) +
0.969 * 1.000 * 0.140) + = 0.276
Qmax(2) =
1.000 * 0.952 * 0.140) +
1.000 * 1.000 * 0.140) + = 0.273

Total of 2 streams to confluence:
Flow rates before confluence point:
0.140 0.140

Maximum flow rates at confluence using above data:
0.276 0.273

Area of streams before confluence:
0.066 0.059

Results of confluence:
Total flow rate = 0.276(CFS)
Time of concentration = 12.600 min.
Effective stream area after confluence = 0.125(Ac.)

Process from Point/Station 46.000 to Point/Station 47.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.500(Ft.)
Downstream point/station elevation = 680.300(Ft.)
Pipe length = 86.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.276(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.276(CFS)
Normal flow depth in pipe = 1.82(In.)
Flow top width inside pipe = 5.52(In.)
Critical Depth = 3.18(In.)
Pipe flow velocity = 5.49(Ft/s)
Travel time through pipe = 0.26 min.
Time of concentration (TC) = 12.86 min.

Process from Point/Station 47.000 to Point/Station 47.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 0.125(Ac.)
Runoff from this stream = 0.276(CFS)
Time of concentration = 12.86 min.
Rainfall intensity = 5.014(In/Hr)

Process from Point/Station 47.000 to Point/Station 47.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 12.00 min. Rain intensity = 5.24(In/Hr)
 Total area = 0.065(Ac.) Total runoff = 0.140(CFS)

++++++
 Process from Point/Station 47.000 to Point/Station 47.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.065(Ac.)
 Runoff from this stream = 0.140(CFS)
 Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.276	12.86	5.014
2	0.140	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 0.276) +
 0.956 * 1.000 * 0.140) + = 0.410
 Qmax(2) =
 1.000 * 0.933 * 0.276) +
 1.000 * 1.000 * 0.140) + = 0.397

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.276 0.140
 Maximum flow rates at confluence using above data:
 0.410 0.397
 Area of streams before confluence:
 0.125 0.065
 Results of confluence:
 Total flow rate = 0.410(CFS)
 Time of concentration = 12.862 min.
 Effective stream area after confluence = 0.190(Ac.)

++++++
 Process from Point/Station 47.000 to Point/Station 52.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 680.300(Ft.)
 Downstream point/station elevation = 679.800(Ft.)
 Pipe length = 9.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.410(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.410(CFS)
 Normal flow depth in pipe = 2.29(In.)
 Flow top width inside pipe = 5.83(In.)
 Critical Depth = 3.90(In.)
 Pipe flow velocity = 5.94(Ft/s)
 Travel time through pipe = 0.03 min.
 Time of concentration (TC) = 12.89 min.

++++++
 Process from Point/Station 52.000 to Point/Station 52.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 0.190(Ac.)
Runoff from this stream = 0.410(CFS)
Time of concentration = 12.89 min.
Rainfall intensity = 5.007(In/Hr)
Program is now starting with Main Stream No. 3

Process from Point/Station 49.000 to Point/Station 49.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.053(Ac.) Total runoff = 0.140(CFS)

Process from Point/Station 49.000 to Point/Station 50.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.300(Ft.)
Downstream point/station elevation = 684.300(Ft.)
Pipe length = 86.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.140(CFS)
Nearest computed pipe diameter = 3.00(In.)
Calculated individual pipe flow = 0.140(CFS)
Normal flow depth in pipe = 2.11(In.)
Flow top width inside pipe = 2.74(In.)
Critical Depth = 2.66(In.)
Pipe flow velocity = 3.77(Ft/s)
Travel time through pipe = 0.38 min.
Time of concentration (TC) = 12.38 min.

Process from Point/Station 50.000 to Point/Station 50.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 1
Stream flow area = 0.053(Ac.)
Runoff from this stream = 0.140(CFS)
Time of concentration = 12.38 min.
Rainfall intensity = 5.138(In/Hr)

Process from Point/Station 50.000 to Point/Station 50.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)

Total area = 0.064(Ac.) Total runoff = 0.140(CFS)

Process from Point/Station 50.000 to Point/Station 50.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 2

Stream flow area = 0.064(Ac.)
Runoff from this stream = 0.140(CFS)
Time of concentration = 12.00 min.
Rainfall intensity = 5.243(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.140	12.38	5.138
2	0.140	12.00	5.243

Qmax(1) =

1.000 *	1.000 *	0.140) +	
0.980 *	1.000 *	0.140) + =	0.277

Qmax(2) =

1.000 *	0.969 *	0.140) +	
1.000 *	1.000 *	0.140) + =	0.276

Total of 2 streams to confluence:

Flow rates before confluence point:

0.140 0.140

Maximum flow rates at confluence using above data:

0.277 0.276

Area of streams before confluence:

0.053 0.064

Results of confluence:

Total flow rate = 0.277(CFS)

Time of concentration = 12.380 min.

Effective stream area after confluence = 0.117(Ac.)

Process from Point/Station 50.000 to Point/Station 51.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 684.300(Ft.)
Downstream point/station elevation = 680.300(Ft.)
Pipe length = 108.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.277(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.277(CFS)
Normal flow depth in pipe = 2.07(In.)
Flow top width inside pipe = 5.71(In.)
Critical Depth = 3.19(In.)
Pipe flow velocity = 4.60(Ft/s)
Travel time through pipe = 0.39 min.
Time of concentration (TC) = 12.77 min.

Process from Point/Station 51.000 to Point/Station 51.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 1

Stream flow area = 0.117(Ac.)
Runoff from this stream = 0.277(CFS)
Time of concentration = 12.77 min.
Rainfall intensity = 5.036(In/Hr)

Process from Point/Station 51.000 to Point/Station 51.000

**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 12.00 min. Rain intensity = 5.24(In/Hr)
 Total area = 0.082(Ac.) Total runoff = 0.110(CFS)

 Process from Point/Station 51.000 to Point/Station 51.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 2
 Stream flow area = 0.082(Ac.)
 Runoff from this stream = 0.110(CFS)
 Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.277	12.77	5.036
2	0.110	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 0.277) +
 0.961 * 1.000 * 0.110) + = 0.383
 Qmax(2) =
 1.000 * 0.940 * 0.277) +
 1.000 * 1.000 * 0.110) + = 0.370

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.277 0.110
 Maximum flow rates at confluence using above data:
 0.383 0.370
 Area of streams before confluence:
 0.117 0.082
 Results of confluence:
 Total flow rate = 0.383(CFS)
 Time of concentration = 12.771 min.
 Effective stream area after confluence = 0.199(Ac.)

 Process from Point/Station 51.000 to Point/Station 52.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 680.300(Ft.)
 Downstream point/station elevation = 679.800(Ft.)
 Pipe length = 37.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.383(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.383(CFS)
 Normal flow depth in pipe = 3.30(In.)
 Flow top width inside pipe = 5.97(In.)
 Critical Depth = 3.77(In.)
 Pipe flow velocity = 3.45(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 12.95 min.

 Process from Point/Station 52.000 to Point/Station 52.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 3
 Stream flow area = 0.199(Ac.)
 Runoff from this stream = 0.383(CFS)
 Time of concentration = 12.95 min.
 Rainfall intensity = 4.992(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	131.200	8.31	6.643
2	0.410	12.89	5.007
3	0.383	12.95	4.992

Qmax(1) =
 1.000 * 1.000 * 131.200) +
 1.000 * 0.645 * 0.410) +
 1.000 * 0.642 * 0.383) + = 131.710

Qmax(2) =
 0.754 * 1.000 * 131.200) +
 1.000 * 1.000 * 0.410) +
 1.000 * 0.995 * 0.383) + = 99.685

Qmax(3) =
 0.751 * 1.000 * 131.200) +
 0.997 * 1.000 * 0.410) +
 1.000 * 1.000 * 0.383) + = 99.377

Total of 3 main streams to confluence:

Flow rates before confluence point:

131.200 0.410 0.383

Maximum flow rates at confluence using above data:

131.710 99.685 99.377

Area of streams before confluence:

50.718 0.190 0.199

Results of confluence:

Total flow rate = 131.710(CFS)

Time of concentration = 8.314 min.

Effective stream area after confluence = 51.107(Ac.)

 Process from Point/Station 52.000 to Point/Station 53.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 679.800(Ft.)
 Downstream point/station elevation = 678.800(Ft.)
 Pipe length = 84.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 131.710(CFS)
 Nearest computed pipe diameter = 45.00(In.)
 Calculated individual pipe flow = 131.710(CFS)
 Normal flow depth in pipe = 36.84(In.)
 Flow top width inside pipe = 34.67(In.)
 Critical Depth = 40.85(In.)
 Pipe flow velocity = 13.62(Ft/s)
 Travel time through pipe = 0.10 min.
 Time of concentration (TC) = 8.42 min.

 Process from Point/Station 53.000 to Point/Station 53.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 51.107(Ac.)

Runoff from this stream = 131.710(CFS)
 Time of concentration = 8.42 min.
 Rainfall intensity = 6.590(In/Hr)

 Process from Point/Station 53.000 to Point/Station 53.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 12.00 min. Rain intensity = 5.24(In/Hr)
 Total area = 0.066(Ac.) Total runoff = 0.140(CFS)

 Process from Point/Station 53.000 to Point/Station 53.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.066(Ac.)
 Runoff from this stream = 0.140(CFS)
 Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	131.710	8.42	6.590
2	0.140	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 131.710) +
 1.000 * 0.701 * 0.140) + = 131.808
 Qmax(2) =
 0.796 * 1.000 * 131.710) +
 1.000 * 1.000 * 0.140) + = 104.919

Total of 2 streams to confluence:
 Flow rates before confluence point:
 131.710 0.140
 Maximum flow rates at confluence using above data:
 131.808 104.919
 Area of streams before confluence:
 51.107 0.066
 Results of confluence:
 Total flow rate = 131.808(CFS)
 Time of concentration = 8.417 min.
 Effective stream area after confluence = 51.173(Ac.)

 Process from Point/Station 53.000 to Point/Station 58.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 678.800(Ft.)
 Downstream point/station elevation = 676.000(Ft.)
 Pipe length = 30.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 131.808(CFS)
 Nearest computed pipe diameter = 33.00(In.)
 Calculated individual pipe flow = 131.808(CFS)
 Normal flow depth in pipe = 22.64(In.)

Flow top width inside pipe = 30.63(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 30.32(Ft/s)
 Travel time through pipe = 0.02 min.
 Time of concentration (TC) = 8.43 min.

 Process from Point/Station 58.000 to Point/Station 58.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 51.173(Ac.)
 Runoff from this stream = 131.808(CFS)
 Time of concentration = 8.43 min.
 Rainfall intensity = 6.582(In/Hr)

 Process from Point/Station 57.000 to Point/Station 57.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 12.00 min. Rain intensity = 5.24(In/Hr)
 Total area = 0.085(Ac.) Total runoff = 0.110(CFS)

 Process from Point/Station 57.000 to Point/Station 58.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 678.500(Ft.)
 Downstream point/station elevation = 676.000(Ft.)
 Pipe length = 35.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.110(CFS)
 Nearest computed pipe diameter = 3.00(In.)
 Calculated individual pipe flow = 0.110(CFS)
 Normal flow depth in pipe = 1.43(In.)
 Flow top width inside pipe = 3.00(In.)
 Critical Depth = 2.40(In.)
 Pipe flow velocity = 4.72(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 12.12 min.

 Process from Point/Station 58.000 to Point/Station 58.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.085(Ac.)
 Runoff from this stream = 0.110(CFS)
 Time of concentration = 12.12 min.
 Rainfall intensity = 5.208(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	131.808	8.43	6.582
2	0.110	12.12	5.208

```

Qmax(1) =
      1.000 *      1.000 *      131.808) +
      1.000 *      0.696 *      0.110) + =      131.885
Qmax(2) =
      0.791 *      1.000 *      131.808) +
      1.000 *      1.000 *      0.110) + =      104.408

Total of 2 streams to confluence:
Flow rates before confluence point:
      131.808      0.110
Maximum flow rates at confluence using above data:
      131.885      104.408
Area of streams before confluence:
      51.173      0.085
Results of confluence:
Total flow rate =      131.885(CFS)
Time of concentration =      8.433 min.
Effective stream area after confluence =      51.258(Ac.)

+++++
Process from Point/Station      58.000 to Point/Station      54.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation =      676.000(Ft.)
Downstream point/station elevation =      675.500(Ft.)
Pipe length =      56.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow =      131.885(CFS)
Nearest computed pipe diameter =      48.00(In.)
Calculated individual pipe flow =      131.885(CFS)
Normal flow depth in pipe =      38.16(In.)
Flow top width inside pipe =      38.76(In.)
Critical Depth =      41.18(In.)
Pipe flow velocity =      12.31(Ft/s)
Travel time through pipe =      0.08 min.
Time of concentration (TC) =      8.51 min.

+++++
Process from Point/Station      54.000 to Point/Station      54.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area =      51.258(Ac.)
Runoff from this stream =      131.885(CFS)
Time of concentration =      8.51 min.
Rainfall intensity =      6.544(In/Hr)

+++++
Process from Point/Station      54.000 to Point/Station      54.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) =      5.243(In/Hr) for a      100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity =      5.24(In/Hr)
Total area =      0.059(Ac.) Total runoff =      0.140(CFS)

+++++
Process from Point/Station      54.000 to Point/Station      54.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.059(Ac.)
 Runoff from this stream = 0.140(CFS)
 Time of concentration = 12.00 min.
 Rainfall intensity = 5.243(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	131.885	8.51	6.544
2	0.140	12.00	5.243

Qmax(1) =
 1.000 * 1.000 * 131.885 +
 1.000 * 0.709 * 0.140 + = 131.984
 Qmax(2) =
 0.801 * 1.000 * 131.885 +
 1.000 * 1.000 * 0.140 + = 105.799

Total of 2 streams to confluence:
 Flow rates before confluence point:
 131.885 0.140
 Maximum flow rates at confluence using above data:
 131.984 105.799
 Area of streams before confluence:
 51.258 0.059
 Results of confluence:
 Total flow rate = 131.984(CFS)
 Time of concentration = 8.509 min.
 Effective stream area after confluence = 51.317(Ac.)

 Process from Point/Station 54.000 to Point/Station 59.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 675.500(Ft.)
 Downstream point/station elevation = 673.000(Ft.)
 Pipe length = 80.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 131.984(CFS)
 Nearest computed pipe diameter = 39.00(In.)
 Calculated individual pipe flow = 131.984(CFS)
 Normal flow depth in pipe = 29.06(In.)
 Flow top width inside pipe = 33.99(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 19.93(Ft/s)
 Travel time through pipe = 0.07 min.
 Time of concentration (TC) = 8.58 min.

 Process from Point/Station 59.000 to Point/Station 59.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 51.317(Ac.)
 Runoff from this stream = 131.984(CFS)
 Time of concentration = 8.58 min.
 Rainfall intensity = 6.511(In/Hr)

 Process from Point/Station 55.000 to Point/Station 55.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]

```

(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) =      5.243(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  12.00 min.  Rain intensity =      5.24(In/Hr)
Total area =      0.064(Ac.)  Total runoff =      0.140(CFS)

*****
Process from Point/Station      55.000 to Point/Station      59.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation =  673.500(Ft.)
Downstream point/station elevation =  673.000(Ft.)
Pipe length =  10.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =  0.140(CFS)
Nearest computed pipe diameter =  3.00(In.)
Calculated individual pipe flow =  0.140(CFS)
Normal flow depth in pipe =  1.86(In.)
Flow top width inside pipe =  2.91(In.)
Critical Depth =  2.66(In.)
Pipe flow velocity =  4.36(Ft/s)
Travel time through pipe =  0.04 min.
Time of concentration (TC) =  12.04 min.

*****
Process from Point/Station      59.000 to Point/Station      59.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area =  0.064(Ac.)
Runoff from this stream =  0.140(CFS)
Time of concentration =  12.04 min.
Rainfall intensity =  5.232(In/Hr)

*****
Process from Point/Station      58.000 to Point/Station      58.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) =      5.243(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  12.00 min.  Rain intensity =      5.24(In/Hr)
Total area =      0.108(Ac.)  Total runoff =      0.460(CFS)

*****
Process from Point/Station      58.000 to Point/Station      59.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation =  673.500(Ft.)
Downstream point/station elevation =  673.000(Ft.)
Pipe length =  35.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =  0.460(CFS)
Nearest computed pipe diameter =  6.00(In.)
Calculated individual pipe flow =  0.460(CFS)
Normal flow depth in pipe =  3.64(In.)
Flow top width inside pipe =  5.86(In.)
Critical Depth =  4.15(In.)
Pipe flow velocity =  3.68(Ft/s)
Travel time through pipe =  0.16 min.

```


Time of concentration (TC) = 12.16 min.

Process from Point/Station 59.000 to Point/Station 59.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 0.108(Ac.)
Runoff from this stream = 0.460(CFS)
Time of concentration = 12.16 min.
Rainfall intensity = 5.199(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	131.984	8.58	6.511
2	0.140	12.04	5.232
3	0.460	12.16	5.199

Qmax(1) =
1.000 * 1.000 * 131.984) +
1.000 * 0.712 * 0.140) +
1.000 * 0.705 * 0.460) + = 132.408

Qmax(2) =
0.804 * 1.000 * 131.984) +
1.000 * 1.000 * 0.140) +
1.000 * 0.990 * 0.460) + = 106.652

Qmax(3) =
0.798 * 1.000 * 131.984) +
0.994 * 1.000 * 0.140) +
1.000 * 1.000 * 0.460) + = 105.977

Total of 3 streams to confluence:

Flow rates before confluence point:

131.984 0.140 0.460

Maximum flow rates at confluence using above data:

132.408 106.652 105.977

Area of streams before confluence:

51.317 0.064 0.108

Results of confluence:

Total flow rate = 132.408(CFS)

Time of concentration = 8.576 min.

Effective stream area after confluence = 51.489(Ac.)

Process from Point/Station 59.000 to Point/Station 62.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 673.000(Ft.)
Downstream point/station elevation = 663.000(Ft.)
Pipe length = 223.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 132.408(CFS)
Nearest computed pipe diameter = 36.00(In.)
Calculated individual pipe flow = 132.408(CFS)
Normal flow depth in pipe = 27.66(In.)
Flow top width inside pipe = 30.38(In.)
Critical depth could not be calculated.
Pipe flow velocity = 22.71(Ft/s)
Travel time through pipe = 0.16 min.
Time of concentration (TC) = 8.74 min.

Process from Point/Station 62.000 to Point/Station 62.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1

Stream flow area = 51.489(Ac.)
Runoff from this stream = 132.408(CFS)
Time of concentration = 8.74 min.
Rainfall intensity = 6.432(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 56.000 to Point/Station 56.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.170(Ac.) Total runoff = 0.110(CFS)

Process from Point/Station 56.000 to Point/Station 62.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 664.300(Ft.)
Downstream point/station elevation = 663.000(Ft.)
Pipe length = 5.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.110(CFS)
Nearest computed pipe diameter = 3.00(In.)
Calculated individual pipe flow = 0.110(CFS)
Normal flow depth in pipe = 1.01(In.)
Flow top width inside pipe = 2.84(In.)
Critical Depth = 2.40(In.)
Pipe flow velocity = 7.59(Ft/s)
Travel time through pipe = 0.01 min.
Time of concentration (TC) = 12.01 min.

Process from Point/Station 62.000 to Point/Station 62.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area = 0.170(Ac.)
Runoff from this stream = 0.110(CFS)
Time of concentration = 12.01 min.
Rainfall intensity = 5.240(In/Hr)
Program is now starting with Main Stream No. 3

Process from Point/Station 60.000 to Point/Station 60.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)

Total area = 0.080(Ac.) Total runoff = 0.110(CFS)

Process from Point/Station 60.000 to Point/Station 61.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 668.300(Ft.)
Downstream point/station elevation = 664.300(Ft.)
Pipe length = 88.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.110(CFS)
Nearest computed pipe diameter = 3.00(In.)
Calculated individual pipe flow = 0.110(CFS)
Normal flow depth in pipe = 1.65(In.)
Flow top width inside pipe = 2.99(In.)
Critical Depth = 2.40(In.)
Pipe flow velocity = 3.98(Ft/s)
Travel time through pipe = 0.37 min.
Time of concentration (TC) = 12.37 min.

Process from Point/Station 61.000 to Point/Station 61.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 1
Stream flow area = 0.080(Ac.)
Runoff from this stream = 0.110(CFS)
Time of concentration = 12.37 min.
Rainfall intensity = 5.142(In/Hr)

Process from Point/Station 61.000 to Point/Station 61.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.243(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 12.00 min. Rain intensity = 5.24(In/Hr)
Total area = 0.067(Ac.) Total runoff = 0.140(CFS)

Process from Point/Station 61.000 to Point/Station 61.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 2
Stream flow area = 0.067(Ac.)
Runoff from this stream = 0.140(CFS)
Time of concentration = 12.00 min.
Rainfall intensity = 5.243(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	0.110	12.37	5.142
2	0.140	12.00	5.243
Qmax(1) =			
	1.000 *	1.000 *	0.110) +
	0.981 *	1.000 *	0.140) + = 0.247
Qmax(2) =			

1.000 * 0.970 * 0.110) +
 1.000 * 1.000 * 0.140) + = 0.247

Total of 2 streams to confluence:
 Flow rates before confluence point:
 0.110 0.140

Maximum flow rates at confluence using above data:
 0.247 0.247

Area of streams before confluence:
 0.080 0.067

Results of confluence:
 Total flow rate = 0.247(CFS)
 Time of concentration = 12.368 min.
 Effective stream area after confluence = 0.147(Ac.)

 Process from Point/Station 61.000 to Point/Station 62.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 664.300(Ft.)
 Downstream point/station elevation = 663.000(Ft.)
 Pipe length = 38.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.247(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.247(CFS)
 Normal flow depth in pipe = 2.00(In.)
 Flow top width inside pipe = 5.65(In.)
 Critical Depth = 3.00(In.)
 Pipe flow velocity = 4.34(Ft/s)
 Travel time through pipe = 0.15 min.
 Time of concentration (TC) = 12.51 min.

 Process from Point/Station 62.000 to Point/Station 62.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 3
 Stream flow area = 0.147(Ac.)
 Runoff from this stream = 0.247(CFS)
 Time of concentration = 12.51 min.
 Rainfall intensity = 5.103(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	132.408	8.74	6.432
2	0.110	12.01	5.240
3	0.247	12.51	5.103

Qmax(1) =
 1.000 * 1.000 * 132.408) +
 1.000 * 0.728 * 0.110) +
 1.000 * 0.698 * 0.247) + = 132.661

Qmax(2) =
 0.815 * 1.000 * 132.408) +
 1.000 * 1.000 * 0.110) +
 1.000 * 0.960 * 0.247) + = 108.207

Qmax(3) =
 0.793 * 1.000 * 132.408) +
 0.974 * 1.000 * 0.110) +
 1.000 * 1.000 * 0.247) + = 105.397

Total of 3 main streams to confluence:
 Flow rates before confluence point:
 132.408 0.110 0.247
 Maximum flow rates at confluence using above data:
 132.661 108.207 105.397

Area of streams before confluence:
51.489 0.170 0.147

Results of confluence:
Total flow rate = 132.661(CFS)
Time of concentration = 8.740 min.
Effective stream area after confluence = 51.806(Ac.)

Process from Point/Station 62.000 to Point/Station 29.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 663.000(Ft.)
Downstream point/station elevation = 662.500(Ft.)
Pipe length = 34.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 132.661(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 132.661(CFS)
Normal flow depth in pipe = 33.52(In.)
Flow top width inside pipe = 39.24(In.)
Critical Depth = 40.96(In.)
Pipe flow velocity = 15.04(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 8.78 min.
End of computations, total study area = 51.806 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/10/13

***** Hydrology Study Control Information *****

File: 12052POSTD.RD3

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 300.000 to Point/Station 301.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 756.000(Ft.)
Highest elevation = 905.000(Ft.)
Lowest elevation = 780.000(Ft.)
Elevation difference = 125.000(Ft.) Slope = 16.534 %
Top of Initial Area Slope adjusted by User to 25.000 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 25.00 %, in a development type of
Permanent Open Space
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.90 minutes
(for slope value of 10.00 %)
Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 59.236(CFS)
Total initial stream area = 22.591(Ac.)

Process from Point/Station 301.000 to Point/Station 302.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 78.088(CFS)
Depth of flow = 1.218(Ft.), Average velocity = 6.583(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 5.00
2 40.00 0.00
3 80.00 5.00
Manning's 'N' friction factor = 0.045

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Sub-Channel flow = 78.088(CFS)
'      '      flow top width = 19.484(Ft.)
'      '      velocity= 6.583(Ft/s)
'      '      area = 11.863(Sq.Ft)
'      '      Froude number = 1.487

Upstream point elevation = 780.000(Ft.)
Downstream point elevation = 705.000(Ft.)
Flow length = 964.000(Ft.)
Travel time = 2.44 min.
Time of concentration = 9.34 min.
Depth of flow = 1.218(Ft.)
Average velocity = 6.583(Ft/s)
Total irregular channel flow = 78.088(CFS)
Irregular channel normal depth above invert elev. = 1.218(Ft.)
Average velocity of channel(s) = 6.583(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Rainfall intensity = 6.162(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350 CA = 15.715
Subarea runoff = 37.607(CFS) for 22.310(Ac.)
Total runoff = 96.843(CFS) Total area = 44.901(Ac.)
Depth of flow = 1.320(Ft.), Average velocity = 6.947(Ft/s)

*****
Process from Point/Station 302.000 to Point/Station 145.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 702.000(Ft.)
Downstream point/station elevation = 699.200(Ft.)
Pipe length = 276.50(Ft.) Manning's N = 0.013
No. of pipes = 3 Required pipe flow = 96.843(CFS)
Nearest computed pipe diameter = 30.00(In.)
Calculated individual pipe flow = 32.281(CFS)
Normal flow depth in pipe = 19.97(In.)
Flow top width inside pipe = 28.31(In.)
Critical Depth = 23.23(In.)
Pipe flow velocity = 9.30(Ft/s)
Travel time through pipe = 0.50 min.
Time of concentration (TC) = 9.84 min.

*****
Process from Point/Station 145.000 to Point/Station 145.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 44.901(Ac.)
Runoff from this stream = 96.843(CFS)
Time of concentration = 9.84 min.
Rainfall intensity = 5.960(In/Hr)

*****
Process from Point/Station 140.000 to Point/Station 141.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000

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[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 204.000(Ft.)
Highest elevation = 717.000(Ft.)
Lowest elevation = 716.000(Ft.)
Elevation difference = 1.000(Ft.) Slope = 0.490 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 50.00 (Ft)
for the top area slope value of 0.49 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 8.70 minutes
(for slope value of 0.50 %)
Rainfall intensity (I) = 6.451(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 2.353(CFS)
Total initial stream area = 0.608(Ac.)

*****
Process from Point/Station 141.000 to Point/Station 142.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 714.000(Ft.)
Downstream point/station elevation = 713.000(Ft.)
Pipe length = 170.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.353(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 2.353(CFS)
Normal flow depth in pipe = 8.59(In.)
Flow top width inside pipe = 10.82(In.)
Critical Depth = 7.88(In.)
Pipe flow velocity = 3.91(Ft/s)
Travel time through pipe = 0.72 min.
Time of concentration (TC) = 9.42 min.

*****
Process from Point/Station 142.000 to Point/Station 142.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 9.42 min.
Rainfall intensity = 6.127(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.612
Subarea runoff = 1.396(CFS) for 0.412(Ac.)
Total runoff = 3.750(CFS) Total area = 1.020(Ac.)

*****
Process from Point/Station 142.000 to Point/Station 143.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 713.000(Ft.)
Downstream point/station elevation = 712.500(Ft.)
Pipe length = 40.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.750(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.750(CFS)
Normal flow depth in pipe = 9.26(In.)
Flow top width inside pipe = 10.08(In.)

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Critical Depth = 9.89(In.)
 Pipe flow velocity = 5.77(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 9.54 min.

 Process from Point/Station 143.000 to Point/Station 144.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 3.882(CFS)
 Depth of flow = 0.123(Ft.), Average velocity = 2.072(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	2.00
2	4.00	0.00
3	19.00	0.00
4	23.00	2.00

 Manning's 'N' friction factor = 0.030

Sub-Channel flow = 3.882(CFS)
 ' ' flow top width = 15.492(Ft.)
 ' ' velocity = 2.072(Ft/s)
 ' ' area = 1.873(Sq.Ft)
 ' ' Froude number = 1.050

Upstream point elevation = 712.500(Ft.)
 Downstream point elevation = 712.000(Ft.)
 Flow length = 17.000(Ft.)
 Travel time = 0.14 min.
 Time of concentration = 9.68 min.
 Depth of flow = 0.123(Ft.)
 Average velocity = 2.072(Ft/s)
 Total irregular channel flow = 3.882(CFS)
 Irregular channel normal depth above invert elev. = 0.123(Ft.)
 Average velocity of channel(s) = 2.072(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity = 6.024(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.655
 Subarea runoff = 0.197(CFS) for 0.072(Ac.)
 Total runoff = 3.947(CFS) Total area = 1.092(Ac.)
 Depth of flow = 0.124(Ft.), Average velocity = 2.086(Ft/s)

 Process from Point/Station 144.000 to Point/Station 145.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

 Upstream point/station elevation = 710.000(Ft.)
 Downstream point/station elevation = 699.200(Ft.)
 Pipe length = 66.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 3.947(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 3.947(CFS)
 Normal flow depth in pipe = 4.97(In.)
 Flow top width inside pipe = 8.95(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 15.77(Ft/s)
 Travel time through pipe = 0.07 min.
 Time of concentration (TC) = 9.75 min.

 Process from Point/Station 145.000 to Point/Station 145.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 1.092(Ac.)
 Runoff from this stream = 3.947(CFS)
 Time of concentration = 9.75 min.
 Rainfall intensity = 5.996(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	96.843	9.84	5.960
2	3.947	9.75	5.996

Qmax(1) =
 1.000 * 1.000 * 96.843) +
 0.994 * 1.000 * 3.947) + = 100.766
 Qmax(2) =
 1.000 * 0.991 * 96.843) +
 1.000 * 1.000 * 3.947) + = 99.903

Total of 2 streams to confluence:
 Flow rates before confluence point:
 96.843 3.947
 Maximum flow rates at confluence using above data:
 100.766 99.903
 Area of streams before confluence:
 44.901 1.092
 Results of confluence:
 Total flow rate = 100.766(CFS)
 Time of concentration = 9.836 min.
 Effective stream area after confluence = 45.993(Ac.)

 Process from Point/Station 145.000 to Point/Station 72.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 699.200(Ft.)
 Downstream point/station elevation = 698.500(Ft.)
 Pipe length = 74.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 100.766(CFS)
 Nearest computed pipe diameter = 45.00(In.)
 Calculated individual pipe flow = 100.766(CFS)
 Normal flow depth in pipe = 32.06(In.)
 Flow top width inside pipe = 40.73(In.)
 Critical Depth = 36.88(In.)
 Pipe flow velocity = 11.97(Ft/s)
 Travel time through pipe = 0.10 min.
 Time of concentration (TC) = 9.94 min.

 Process from Point/Station 72.000 to Point/Station 72.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 45.993(Ac.)
 Runoff from this stream = 100.766(CFS)
 Time of concentration = 9.94 min.
 Rainfall intensity = 5.920(In/Hr)

 Process from Point/Station 70.000 to Point/Station 72.000
 **** INITIAL AREA EVALUATION ****

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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 254.000(Ft.)
Highest elevation = 714.000(Ft.)
Lowest elevation = 710.000(Ft.)
Elevation difference = 4.000(Ft.) Slope = 1.575 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 80.00 (Ft)
for the top area slope value of 1.58 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.92 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 80.000^0.5)]/( 1.575^(1/3))= 6.92
Rainfall intensity (I) = 7.479(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 1.032(CFS)
Total initial stream area = 0.230(Ac.)

*****
Process from Point/Station 72.000 to Point/Station 72.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.230(Ac.)
Runoff from this stream = 1.032(CFS)
Time of concentration = 6.92 min.
Rainfall intensity = 7.479(In/Hr)
Summary of stream data:

Stream Flow rate TC Rainfall Intensity
No. (CFS) (min) (In/Hr)

1 100.766 9.94 5.920
2 1.032 6.92 7.479
Qmax(1) =
1.000 * 1.000 * 100.766) +
0.792 * 1.000 * 1.032) + = 101.583
Qmax(2) =
1.000 * 0.696 * 100.766) +
1.000 * 1.000 * 1.032) + = 71.176

Total of 2 streams to confluence:
Flow rates before confluence point:
100.766 1.032
Maximum flow rates at confluence using above data:
101.583 71.176
Area of streams before confluence:
45.993 0.230
Results of confluence:
Total flow rate = 101.583(CFS)
Time of concentration = 9.939 min.
Effective stream area after confluence = 46.223(Ac.)

*****
Process from Point/Station 72.000 to Point/Station 73.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 698.500(Ft.)
Downstream point/station elevation = 698.000(Ft.)
Pipe length = 53.00(Ft.) Manning's N = 0.013

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No. of pipes = 1 Required pipe flow = 101.583(CFS)
 Nearest computed pipe diameter = 45.00(In.)
 Calculated individual pipe flow = 101.583(CFS)
 Normal flow depth in pipe = 32.30(In.)
 Flow top width inside pipe = 40.51(In.)
 Critical Depth = 37.02(In.)
 Pipe flow velocity = 11.97(Ft/s)
 Travel time through pipe = 0.07 min.
 Time of concentration (TC) = 10.01 min.

 Process from Point/Station 73.000 to Point/Station 73.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 46.223(Ac.)
 Runoff from this stream = 101.583(CFS)
 Time of concentration = 10.01 min.
 Rainfall intensity = 5.892(In/Hr)

 Process from Point/Station 70.000 to Point/Station 71.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 278.000(Ft.)
 Highest elevation = 714.000(Ft.)
 Lowest elevation = 708.000(Ft.)
 Elevation difference = 6.000(Ft.) Slope = 2.158 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 80.00 (Ft)
 for the top area slope value of 2.16 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.23 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (80.000^{.5})] / (2.158^{(1/3)}) = 6.23$
 Rainfall intensity (I) = 8.003(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.200(CFS)
 Total initial stream area = 0.250(Ac.)

 Process from Point/Station 71.000 to Point/Station 73.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 703.500(Ft.)
 Downstream point/station elevation = 698.000(Ft.)
 Pipe length = 37.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.200(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 1.200(CFS)
 Normal flow depth in pipe = 3.19(In.)
 Flow top width inside pipe = 5.99(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 11.30(Ft/s)
 Travel time through pipe = 0.05 min.
 Time of concentration (TC) = 6.28 min.

Process from Point/Station 73.000 to Point/Station 73.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 0.250(Ac.)
Runoff from this stream = 1.200(CFS)
Time of concentration = 6.28 min.
Rainfall intensity = 7.958(In/Hr)

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	101.583	10.01	5.892
2	1.200	6.28	7.958

Qmax(1) =

1.000 * 1.000 * 101.583) +
0.740 * 1.000 * 1.200) + = 102.472

Qmax(2) =

1.000 * 0.628 * 101.583) +
1.000 * 1.000 * 1.200) + = 64.951

Total of 2 streams to confluence:

Flow rates before confluence point:

101.583 1.200

Maximum flow rates at confluence using above data:

102.472 64.951

Area of streams before confluence:

46.223 0.250

Results of confluence:

Total flow rate = 102.472(CFS)

Time of concentration = 10.013 min.

Effective stream area after confluence = 46.473(Ac.)

Process from Point/Station 73.000 to Point/Station 74.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 698.000(Ft.)
Downstream point/station elevation = 696.000(Ft.)
Pipe length = 197.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 102.472(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 102.472(CFS)
Normal flow depth in pipe = 31.59(In.)
Flow top width inside pipe = 41.16(In.)
Critical Depth = 37.16(In.)
Pipe flow velocity = 12.36(Ft/s)
Travel time through pipe = 0.27 min.
Time of concentration (TC) = 10.28 min.

Process from Point/Station 74.000 to Point/Station 74.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 46.473(Ac.)
Runoff from this stream = 102.472(CFS)
Time of concentration = 10.28 min.
Rainfall intensity = 5.794(In/Hr)

Process from Point/Station 303.000 to Point/Station 304.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000

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Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN          ]
(Permanent Open Space    )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 84.000(Ft.)
Highest elevation = 772.000(Ft.)
Lowest elevation = 755.000(Ft.)
Elevation difference = 17.000(Ft.) Slope = 20.238 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 20.24 %, in a development type of
Permanent Open Space
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.90 minutes
(for slope value of 10.00 %)
Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 1.030(CFS)
Total initial stream area = 0.393(Ac.)

*****
Process from Point/Station 304.000 to Point/Station 305.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

-----
Estimated mean flow rate at midpoint of channel = 4.261(CFS)
Depth of flow = 0.191(Ft.), Average velocity = 2.345(Ft/s)
***** Irregular Channel Data *****
-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
1                  0.00                2.00
2                 100.00                0.00
3                 200.00                2.00
Manning's 'N' friction factor = 0.045
-----
Sub-Channel flow = 4.261(CFS)
'      '      flow top width = 19.062(Ft.)
'      '      velocity= 2.345(Ft/s)
'      '      area = 1.817(Sq.Ft)
'      '      Froude number = 1.339

Upstream point elevation = 755.000(Ft.)
Downstream point elevation = 704.000(Ft.)
Flow length = 440.000(Ft.)
Travel time = 3.13 min.
Time of concentration = 10.03 min.
Depth of flow = 0.191(Ft.)
Average velocity = 2.345(Ft/s)
Total irregular channel flow = 4.261(CFS)
Irregular channel normal depth above invert elev. = 0.191(Ft.)
Average velocity of channel(s) = 2.345(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN          ]
(Permanent Open Space    )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Rainfall intensity = 5.887(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350 CA = 1.260
Subarea runoff = 6.387(CFS) for 3.207(Ac.)
Total runoff = 7.418(CFS) Total area = 3.600(Ac.)
Depth of flow = 0.235(Ft.), Average velocity = 2.694(Ft/s)

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*****
Process from Point/Station      305.000 to Point/Station      74.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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Upstream point/station elevation = 701.000(Ft.)
Downstream point/station elevation = 696.000(Ft.)
Pipe length = 114.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 7.418(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 7.418(CFS)
Normal flow depth in pipe = 9.77(In.)
Flow top width inside pipe = 9.33(In.)
Critical depth could not be calculated.
Pipe flow velocity = 10.83(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 10.20 min.

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*****
Process from Point/Station      74.000 to Point/Station      74.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 2
Stream flow area = 3.600(Ac.)
Runoff from this stream = 7.418(CFS)
Time of concentration = 10.20 min.
Rainfall intensity = 5.822(In/Hr)
Summary of stream data:

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Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	102.472	10.28	5.794
2	7.418	10.20	5.822
Qmax(1) =			
	1.000 *	1.000 *	102.472) +
	0.995 *	1.000 *	7.418) + = 109.854
Qmax(2) =			
	1.000 *	0.993 *	102.472) +
	1.000 *	1.000 *	7.418) + = 109.127

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Total of 2 streams to confluence:
Flow rates before confluence point:
102.472      7.418
Maximum flow rates at confluence using above data:
109.854      109.127
Area of streams before confluence:
46.473      3.600
Results of confluence:
Total flow rate = 109.854(CFS)
Time of concentration = 10.279 min.
Effective stream area after confluence = 50.073(Ac.)

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*****
Process from Point/Station      74.000 to Point/Station      75.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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Upstream point/station elevation = 696.000(Ft.)
Downstream point/station elevation = 695.500(Ft.)
Pipe length = 50.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 109.854(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 109.854(CFS)
Normal flow depth in pipe = 33.66(In.)
Flow top width inside pipe = 39.08(In.)
Critical Depth = 38.29(In.)
Pipe flow velocity = 12.41(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 10.35 min.

```

 Process from Point/Station 75.000 to Point/Station 75.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 50.073(Ac.)
 Runoff from this stream = 109.854(CFS)
 Time of concentration = 10.35 min.
 Rainfall intensity = 5.769(In/Hr)

 Process from Point/Station 72.000 to Point/Station 75.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 300.000(Ft.)
 Highest elevation = 710.000(Ft.)
 Lowest elevation = 701.500(Ft.)
 Elevation difference = 8.500(Ft.) Slope = 2.833 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 2.83 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.03 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (2.833^{(1/3)}) = 6.03$
 Rainfall intensity (I) = 8.169(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.103(CFS)
 Total initial stream area = 0.225(Ac.)

 Process from Point/Station 75.000 to Point/Station 75.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.225(Ac.)
 Runoff from this stream = 1.103(CFS)
 Time of concentration = 6.03 min.
 Rainfall intensity = 8.169(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	109.854	10.35	5.769
2	1.103	6.03	8.169

Qmax(1) =
 $1.000 * 1.000 * 109.854 + 0.706 * 1.000 * 1.103 = 110.633$
 Qmax(2) =
 $1.000 * 0.583 * 109.854 + 1.000 * 1.000 * 1.103 = 65.175$

Total of 2 streams to confluence:
 Flow rates before confluence point:
 109.854 1.103
 Maximum flow rates at confluence using above data:

Upstream point/station elevation = 694.000(Ft.)
 Downstream point/station elevation = 693.500(Ft.)
 Pipe length = 37.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.335(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.335(CFS)
 Normal flow depth in pipe = 5.52(In.)
 Flow top width inside pipe = 8.77(In.)
 Critical Depth = 6.39(In.)
 Pipe flow velocity = 4.70(Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 6.19 min.

++++++
 Process from Point/Station 77.000 to Point/Station 77.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.273(Ac.)
 Runoff from this stream = 1.335(CFS)
 Time of concentration = 6.19 min.
 Rainfall intensity = 8.037(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	110.633	10.46	5.729
2	1.335	6.19	8.037

Qmax(1) =
 1.000 * 1.000 * 110.633) +
 0.713 * 1.000 * 1.335) + = 111.584
 Qmax(2) =
 1.000 * 0.592 * 110.633) +
 1.000 * 1.000 * 1.335) + = 66.784

Total of 2 streams to confluence:
 Flow rates before confluence point:
 110.633 1.335
 Maximum flow rates at confluence using above data:
 111.584 66.784
 Area of streams before confluence:
 50.298 0.273
 Results of confluence:
 Total flow rate = 111.584(CFS)
 Time of concentration = 10.459 min.
 Effective stream area after confluence = 50.571(Ac.)

++++++
 Process from Point/Station 77.000 to Point/Station 80.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 693.500(Ft.)
 Downstream point/station elevation = 686.500(Ft.)
 Pipe length = 185.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 111.584(CFS)
 Nearest computed pipe diameter = 36.00(In.)
 Calculated individual pipe flow = 111.584(CFS)
 Normal flow depth in pipe = 25.73(In.)
 Flow top width inside pipe = 32.51(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 20.64(Ft/s)
 Travel time through pipe = 0.15 min.
 Time of concentration (TC) = 10.61 min.

+++++

Process from Point/Station 80.000 to Point/Station 80.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 50.571(Ac.)
Runoff from this stream = 111.584(CFS)
Time of concentration = 10.61 min.
Rainfall intensity = 5.677(In/Hr)

Process from Point/Station 76.000 to Point/Station 78.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 181.000(Ft.)
Highest elevation = 698.500(Ft.)
Lowest elevation = 693.000(Ft.)
Elevation difference = 5.500(Ft.) Slope = 3.039 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.04 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.89 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.039^{(1/3)}) = 5.89$
Rainfall intensity (I) = 8.293(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.776(CFS)
Total initial stream area = 0.156(Ac.)

Process from Point/Station 78.000 to Point/Station 79.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.500(Ft.)
Downstream point/station elevation = 688.000(Ft.)
Pipe length = 37.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.776(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.776(CFS)
Normal flow depth in pipe = 3.98(In.)
Flow top width inside pipe = 8.94(In.)
Critical Depth = 4.82(In.)
Pipe flow velocity = 4.12(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 6.04 min.

Process from Point/Station 79.000 to Point/Station 79.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.04 min.

Rainfall intensity = 8.160(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.226
 Subarea runoff = 1.070(CFS) for 0.221(Ac.)
 Total runoff = 1.846(CFS) Total area = 0.377(Ac.)

++++++
 Process from Point/Station 79.000 to Point/Station 80.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
 Downstream point/station elevation = 686.500(Ft.)
 Pipe length = 150.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.846(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 1.846(CFS)
 Normal flow depth in pipe = 6.13(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical Depth = 6.95(In.)
 Pipe flow velocity = 4.58(Ft/s)
 Travel time through pipe = 0.55 min.
 Time of concentration (TC) = 6.59 min.

++++++
 Process from Point/Station 80.000 to Point/Station 80.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.377(Ac.)
 Runoff from this stream = 1.846(CFS)
 Time of concentration = 6.59 min.
 Rainfall intensity = 7.717(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	111.584	10.61	5.677
2	1.846	6.59	7.717

Qmax(1) =
 1.000 * 1.000 * 111.584) +
 0.736 * 1.000 * 1.846) + = 112.942
 Qmax(2) =
 1.000 * 0.621 * 111.584) +
 1.000 * 1.000 * 1.846) + = 71.167

Total of 2 streams to confluence:
 Flow rates before confluence point:
 111.584 1.846
 Maximum flow rates at confluence using above data:
 112.942 71.167
 Area of streams before confluence:
 50.571 0.377
 Results of confluence:
 Total flow rate = 112.942(CFS)
 Time of concentration = 10.609 min.
 Effective stream area after confluence = 50.948(Ac.)
 End of computations, total study area = 50.948 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 01/31/13

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 140.000 to Point/Station 141.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 204.000(Ft.)
Highest elevation = 717.000(Ft.)
Lowest elevation = 716.000(Ft.)
Elevation difference = 1.000(Ft.) Slope = 0.490 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 50.00 (Ft)
for the top area slope value of 0.49 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 8.07 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (50.000^{.5})] / (0.490^{(1/3)}) = 8.07$
Rainfall intensity (I) = 6.771(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 2.470(CFS)
Total initial stream area = 0.608(Ac.)

Process from Point/Station 141.000 to Point/Station 142.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 714.000(Ft.)
Downstream point/station elevation = 713.000(Ft.)
Pipe length = 170.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.470(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 2.470(CFS)
Normal flow depth in pipe = 8.93(In.)
Flow top width inside pipe = 10.47(In.)
Critical Depth = 8.07(In.)
Pipe flow velocity = 3.94(Ft/s)

Flow rate for Pond at Park B
Page 1 of 3

Travel time through pipe = 0.72 min.
Time of concentration (TC) = 8.79 min.

Process from Point/Station 142.000 to Point/Station 142.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.79 min.
Rainfall intensity = 6.408(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.612
Subarea runoff = 1.452(CFS) for 0.412(Ac.)
Total runoff = 3.922(CFS) Total area = 1.020(Ac.)

Process from Point/Station 142.000 to Point/Station 143.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 713.000(Ft.)
Downstream point/station elevation = 712.500(Ft.)
Pipe length = 40.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.922(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.922(CFS)
Normal flow depth in pipe = 9.68(In.)
Flow top width inside pipe = 9.48(In.)
Critical Depth = 10.08(In.)
Pipe flow velocity = 5.78(Ft/s)
Travel time through pipe = 0.12 min.
Time of concentration (TC) = 8.91 min.

Process from Point/Station 143.000 to Point/Station 144.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 4.060(CFS)
Depth of flow = 0.126(Ft.), Average velocity = 2.109(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 2.00
2 4.00 0.00
3 19.00 0.00
4 23.00 2.00
Manning's 'N' friction factor = 0.030

Sub-Channel flow = 4.060(CFS)
' ' flow top width = 15.505(Ft.)
' ' velocity = 2.109(Ft/s)
' ' area = 1.925(Sq.Ft)
' ' Froude number = 1.055

Upstream point elevation = 712.500(Ft.)
Downstream point elevation = 712.000(Ft.)
Flow length = 17.000(Ft.)
Travel time = 0.13 min.
Time of concentration = 9.04 min.
Depth of flow = 0.126(Ft.)
Average velocity = 2.109(Ft/s)

```

Total irregular channel flow =      4.060(CFS)
Irregular channel normal depth above invert elev. =   0.126(Ft.)
Average velocity of channel(s) =   2.109(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL                ]
(10.9 DU/A or Less                )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity =      6.293(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.655
Subarea runoff =      0.202(CFS) for      0.072(Ac.)
Total runoff =      4.123(CFS)      Total area =      1.092(Ac.)
Depth of flow =   0.127(Ft.), Average velocity =   2.122(Ft/s)

+++++
Process from Point/Station      144.000 to Point/Station      145.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =   710.000(Ft.)
Downstream point/station elevation =   708.000(Ft.)
Pipe length =    66.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =    4.123(CFS)
Nearest computed pipe diameter =    12.00(In.)
Calculated individual pipe flow =    4.123(CFS)
Normal flow depth in pipe =    7.15(In.)
Flow top width inside pipe =   11.78(In.)
Critical Depth =   10.29(In.)
Pipe flow velocity =    8.45(Ft/s)
Travel time through pipe =    0.13 min.
Time of concentration (TC) =    9.17 min.
End of computations, total study area =          1.092 (Ac.)

```

Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 10:10 AM

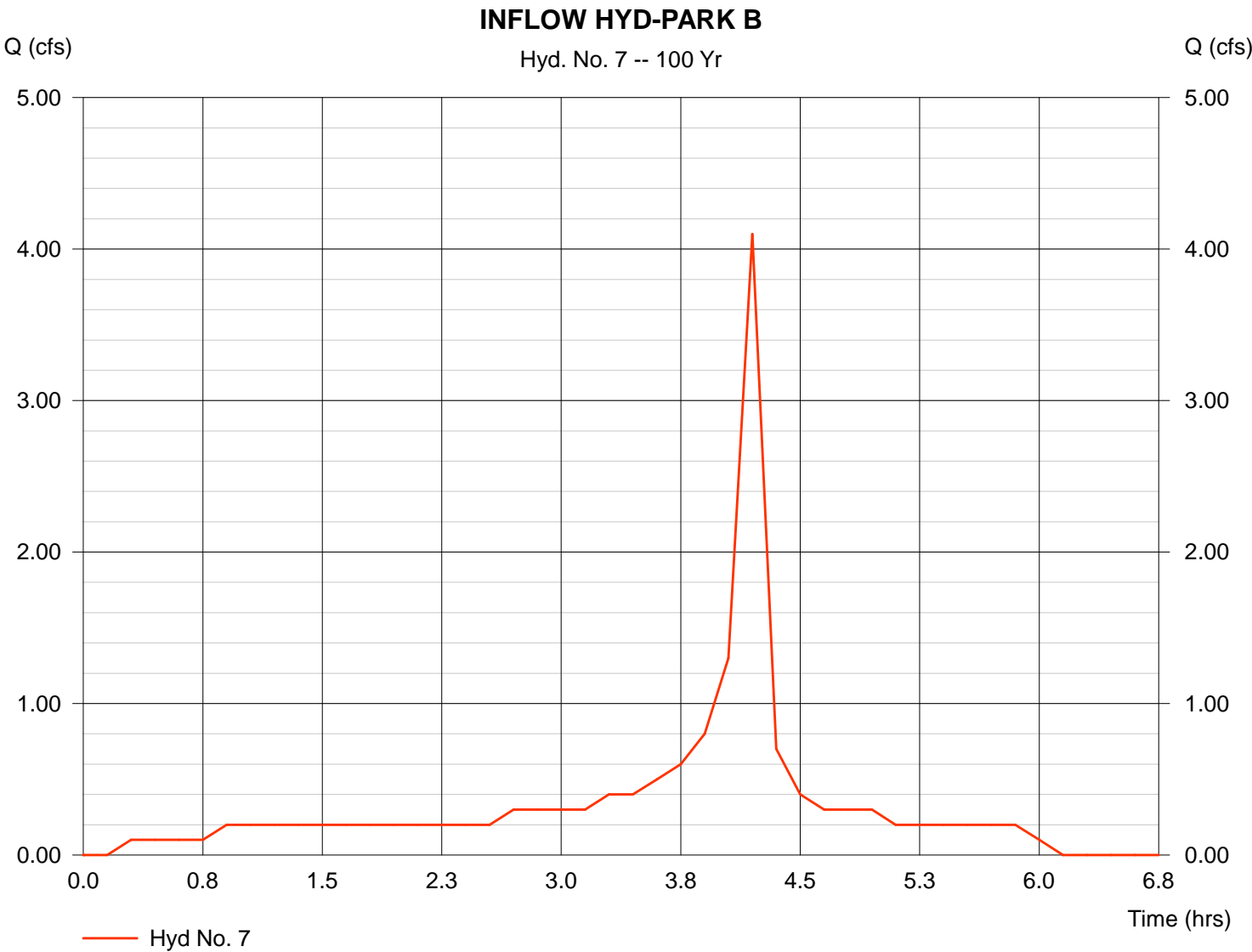
Hyd. No. 7

INFLOW HYD-PARK B

Hydrograph type = Manual
Storm frequency = 100 yrs

Peak discharge = 4.10 cfs
Time interval = 9 min

Hydrograph Volume = 8,316 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 10:13 AM

Hyd. No. 2

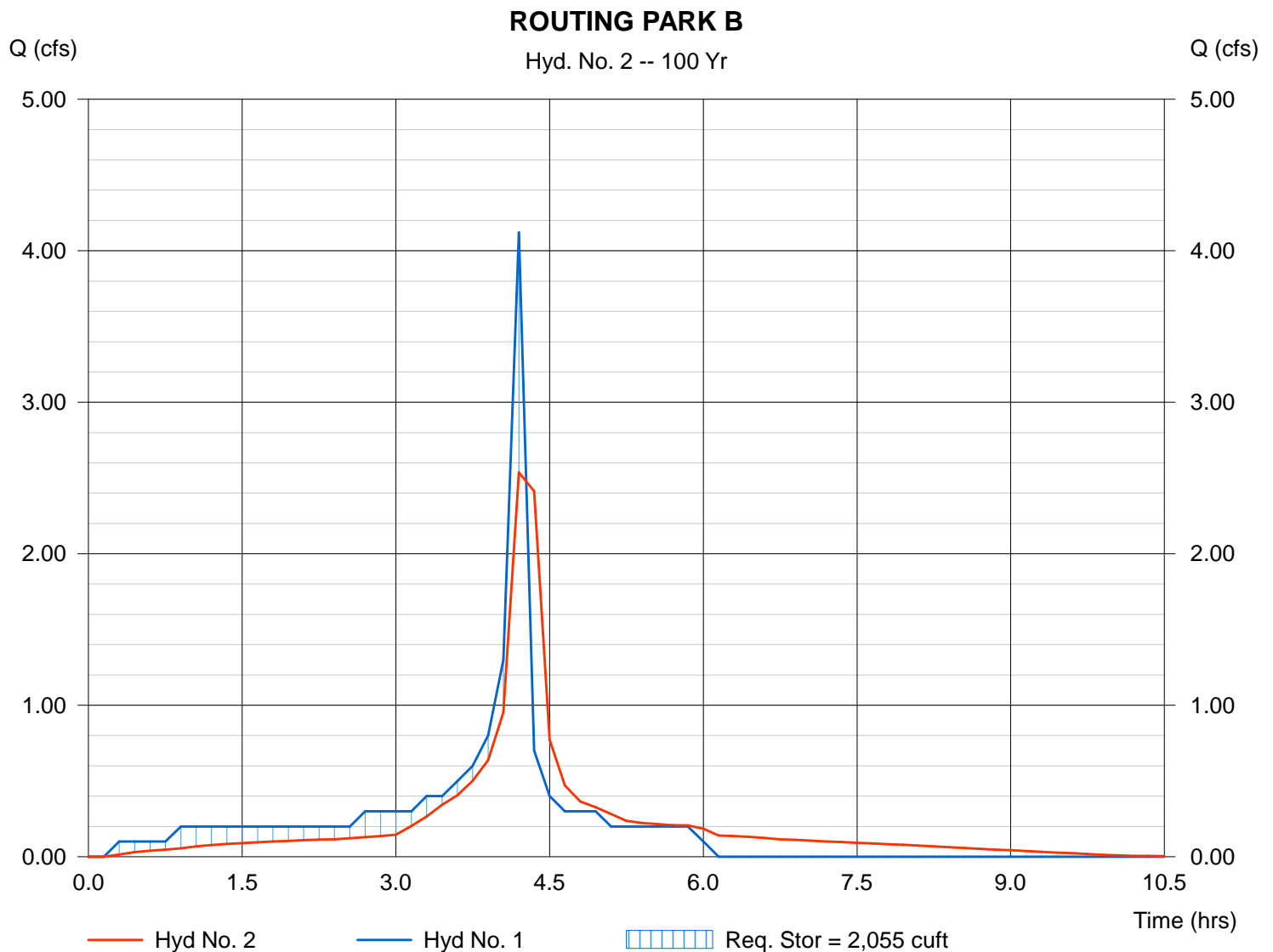
ROUTING PARK B

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 1
Reservoir name = PARK B POND

Peak discharge = 2.54 cfs
Time interval = 9 min
Max. Elevation = 5.77 ft
Max. Storage = 2,055 cuft

Storage Indication method used.

Hydrograph Volume = 8,325 cuft



Pond Report

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 10:14 AM

Pond No. 1 - PARK B POND

Pond Data

Pond storage is based on known values

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	0.00	00	0	0
2.00	2.00	00	357	357
4.00	4.00	00	408	765
4.50	4.50	00	281	1,046
6.00	6.00	00	1,196	2,242

Culvert / Orifice Structures

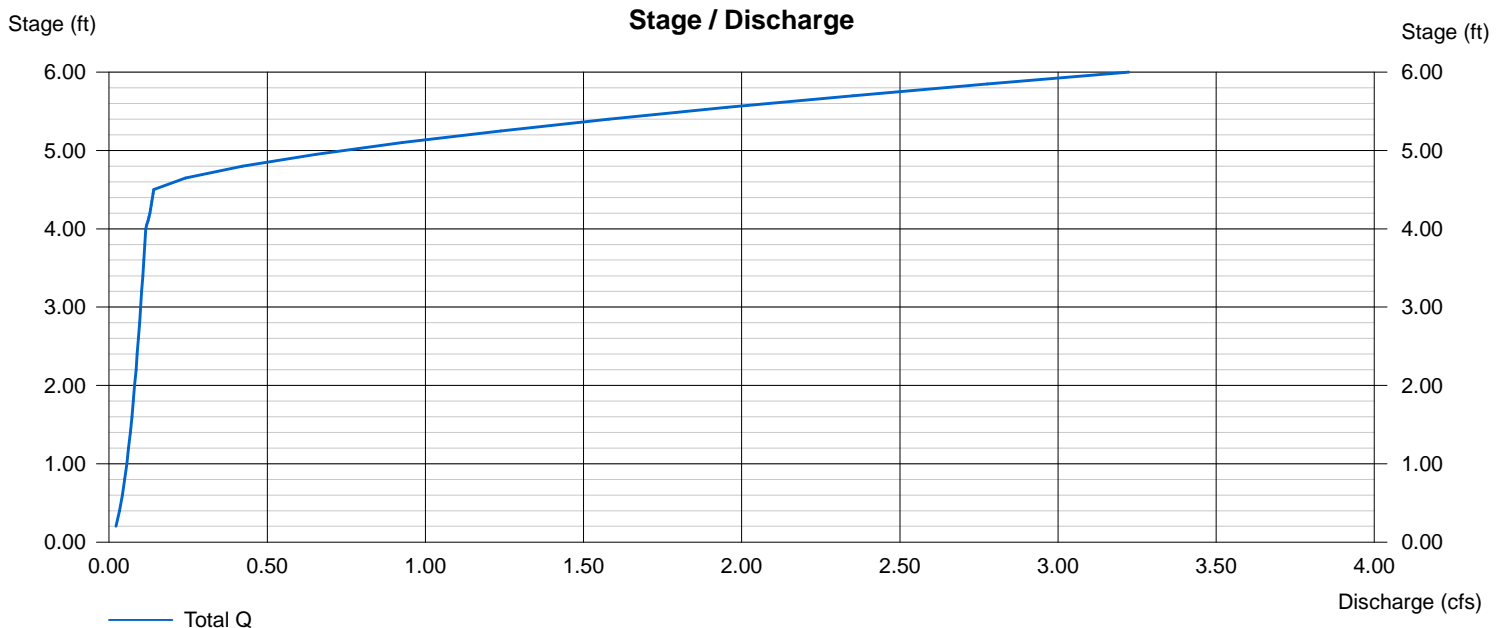
	[A]	[B]	[C]	[D]
Rise (in)	= 12.00	1.50	1.00	0.00
Span (in)	= 12.00	1.50	1.00	0.00
No. Barrels	= 1	1	1	0
Invert El. (ft)	= 0.00	0.00	4.00	0.00
Length (ft)	= 66.00	0.00	0.00	0.00
Slope (%)	= 13.00	0.00	0.00	0.00
N-Value	= .013	.013	.013	.013
Orif. Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	Yes	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 0.50	0.00	0.00	0.00
Crest El. (ft)	= 4.50	0.00	0.00	0.00
Weir Coeff.	= 3.33	0.00	0.00	0.00
Weir Type	= Riser	---	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Wet area) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/14/13

***** Hydrology Study Control Information *****

File: D12052POSTD.rd3

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 300.000 to Point/Station 301.000
*** INITIAL AREA EVALUATION ***

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 756.000(Ft.)
Highest elevation = 905.000(Ft.)
Lowest elevation = 780.000(Ft.)
Elevation difference = 125.000(Ft.) Slope = 16.534 %
Top of Initial Area Slope adjusted by User to 25.000 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 25.00 %, in a development type of
Permanent Open Space
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.90 minutes
(for slope value of 10.00 %)
Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 59.236(CFS)
Total initial stream area = 22.591(Ac.)

Process from Point/Station 301.000 to Point/Station 302.000
*** IRREGULAR CHANNEL FLOW TRAVEL TIME ***

Estimated mean flow rate at midpoint of channel = 78.088(CFS)
Depth of flow = 1.218(Ft.), Average velocity = 6.583(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 5.00
2 40.00 0.00
3 80.00 5.00
Manning's 'N' friction factor = 0.045

Sub-Channel flow = 78.088(CFS)
' ' flow top width = 19.484(Ft.)

```

'      '      velocity=    6.583(Ft/s)
'      '      area =      11.863(Sq.Ft)
'      '      Froude number =    1.487

Upstream point elevation =    780.000(Ft.)
Downstream point elevation =    705.000(Ft.)
Flow length =    964.000(Ft.)
Travel time =    2.44 min.
Time of concentration =    9.34 min.
Depth of flow =    1.218(Ft.)
Average velocity =    6.583(Ft/s)
Total irregular channel flow =    78.088(CFS)
Irregular channel normal depth above invert elev. =    1.218(Ft.)
Average velocity of channel(s) =    6.583(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN                                ]
(Permanent Open Space )
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Rainfall intensity =    6.162(In/Hr) for a    100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350  CA =    15.715
Subarea runoff =    37.607(CFS) for    22.310(Ac.)
Total runoff =    96.843(CFS)      Total area =    44.901(Ac.)
Depth of flow =    1.320(Ft.), Average velocity =    6.947(Ft/s)

+-----+
Process from Point/Station    302.000 to Point/Station    145.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation =    702.000(Ft.)
Downstream point/station elevation =    699.200(Ft.)
Pipe length =    276.50(Ft.)  Manning's N = 0.013
No. of pipes = 3  Required pipe flow =    96.843(CFS)
Nearest computed pipe diameter =    30.00(In.)
Calculated individual pipe flow =    32.281(CFS)
Normal flow depth in pipe =    19.97(In.)
Flow top width inside pipe =    28.31(In.)
Critical Depth =    23.23(In.)
Pipe flow velocity =    9.30(Ft/s)
Travel time through pipe =    0.50 min.
Time of concentration (TC) =    9.84 min.

+-----+
Process from Point/Station    145.000 to Point/Station    145.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area =    44.901(Ac.)
Runoff from this stream =    96.843(CFS)
Time of concentration =    9.84 min.
Rainfall intensity =    5.960(In/Hr)

+-----+
Process from Point/Station    144.000 to Point/Station    144.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL                                ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) =    6.312(In/Hr) for a    100.0 year storm

```

User specified values are as follows:

TC = 9.00 min. Rain intensity = 6.31(In/Hr)
Total area = 1.100(Ac.) Total runoff = 2.530(CFS)

Process from Point/Station 144.000 to Point/Station 145.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 710.000(Ft.)
Downstream point/station elevation = 699.200(Ft.)
Pipe length = 66.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.530(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.530(CFS)
Normal flow depth in pipe = 3.83(In.)
Flow top width inside pipe = 8.90(In.)
Critical Depth = 8.33(In.)
Pipe flow velocity = 14.09(Ft/s)
Travel time through pipe = 0.08 min.
Time of concentration (TC) = 9.08 min.

Process from Point/Station 145.000 to Point/Station 145.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 1.100(Ac.)
Runoff from this stream = 2.530(CFS)
Time of concentration = 9.08 min.
Rainfall intensity = 6.277(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	96.843	9.84	5.960
2	2.530	9.08	6.277

Qmax(1) =

1.000 *	1.000 *	96.843) +	
0.950 *	1.000 *	2.530) + =	99.245

Qmax(2) =

1.000 *	0.923 *	96.843) +	
1.000 *	1.000 *	2.530) + =	91.910

Total of 2 streams to confluence:
Flow rates before confluence point:
96.843 2.530

Maximum flow rates at confluence using above data:
99.245 91.910

Area of streams before confluence:
44.901 1.100

Results of confluence:
Total flow rate = 99.245(CFS)
Time of concentration = 9.836 min.
Effective stream area after confluence = 46.001(Ac.)

Process from Point/Station 145.000 to Point/Station 72.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 699.200(Ft.)
Downstream point/station elevation = 698.500(Ft.)
Pipe length = 74.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 99.245(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 99.245(CFS)
Normal flow depth in pipe = 31.69(In.)
Flow top width inside pipe = 41.08(In.)
Critical Depth = 36.63(In.)

Pipe flow velocity = 11.94(Ft/s)
 Travel time through pipe = 0.10 min.
 Time of concentration (TC) = 9.94 min.

 Process from Point/Station 72.000 to Point/Station 72.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 46.001(Ac.)
 Runoff from this stream = 99.245(CFS)
 Time of concentration = 9.94 min.
 Rainfall intensity = 5.920(In/Hr)

 Process from Point/Station 70.000 to Point/Station 72.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 254.000(Ft.)
 Highest elevation = 714.000(Ft.)
 Lowest elevation = 710.000(Ft.)
 Elevation difference = 4.000(Ft.) Slope = 1.575 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 80.00 (Ft)
 for the top area slope value of 1.58 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.92 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (80.000^{.5})] / (1.575^{(1/3)}) = 6.92$
 Rainfall intensity (I) = 7.479(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.032(CFS)
 Total initial stream area = 0.230(Ac.)

 Process from Point/Station 72.000 to Point/Station 72.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.230(Ac.)
 Runoff from this stream = 1.032(CFS)
 Time of concentration = 6.92 min.
 Rainfall intensity = 7.479(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	99.245	9.94	5.920
2	1.032	6.92	7.479
Qmax(1) =			
	1.000 *	1.000 *	99.245) +
	0.792 *	1.000 *	1.032) + = 100.062
Qmax(2) =			
	1.000 *	0.696 *	99.245) +
	1.000 *	1.000 *	1.032) + = 70.116

Total of 2 streams to confluence:
 Flow rates before confluence point:
 99.245 1.032

```

      100.062      70.116
Area of streams before confluence:
      46.001      0.230
Results of confluence:
Total flow rate =      100.062(CFS)
Time of concentration =      9.939 min.
Effective stream area after confluence =      46.231(Ac.)

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Process from Point/Station      72.000 to Point/Station      73.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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Upstream point/station elevation = 698.500(Ft.)
Downstream point/station elevation = 698.000(Ft.)
Pipe length = 53.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 100.062(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 100.062(CFS)
Normal flow depth in pipe = 31.92(In.)
Flow top width inside pipe = 40.86(In.)
Critical Depth = 36.77(In.)
Pipe flow velocity = 11.94(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 10.01 min.

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Process from Point/Station      73.000 to Point/Station      73.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area = 46.231(Ac.)
Runoff from this stream = 100.062(CFS)
Time of concentration = 10.01 min.
Rainfall intensity = 5.892(In/Hr)

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Process from Point/Station      70.000 to Point/Station      71.000
**** INITIAL AREA EVALUATION ****

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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL                ]
(10.9 DU/A or Less                        )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance  = 278.000(Ft.)
Highest elevation = 714.000(Ft.)
Lowest elevation = 708.000(Ft.)
Elevation difference = 6.000(Ft.) Slope = 2.158 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 80.00 (Ft)
for the top area slope value of 2.16 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 6.23 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^(.5)]/(% slope^(1/3))
TC = [1.8*(1.1-0.6000)*( 80.000^.5)]/( 2.158^(1/3))]= 6.23
Rainfall intensity (I) = 8.003(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 1.200(CFS)
Total initial stream area = 0.250(Ac.)

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Process from Point/Station      71.000 to Point/Station      73.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 703.500(Ft.)
 Downstream point/station elevation = 698.000(Ft.)
 Pipe length = 37.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.200(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 1.200(CFS)
 Normal flow depth in pipe = 3.19(In.)
 Flow top width inside pipe = 5.99(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 11.30(Ft/s)
 Travel time through pipe = 0.05 min.
 Time of concentration (TC) = 6.28 min.

 Process from Point/Station 73.000 to Point/Station 73.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.250(Ac.)
 Runoff from this stream = 1.200(CFS)
 Time of concentration = 6.28 min.
 Rainfall intensity = 7.958(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	100.062	10.01	5.892
2	1.200	6.28	7.958

Qmax(1) =
 1.000 * 1.000 * 100.062) +
 0.740 * 1.000 * 1.200) + = 100.951

Qmax(2) =
 1.000 * 0.628 * 100.062) +
 1.000 * 1.000 * 1.200) + = 63.994

Total of 2 streams to confluence:
 Flow rates before confluence point:
 100.062 1.200
 Maximum flow rates at confluence using above data:
 100.951 63.994
 Area of streams before confluence:
 46.231 0.250
 Results of confluence:
 Total flow rate = 100.951(CFS)
 Time of concentration = 10.013 min.
 Effective stream area after confluence = 46.481(Ac.)

 Process from Point/Station 73.000 to Point/Station 74.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 698.000(Ft.)
 Downstream point/station elevation = 696.000(Ft.)
 Pipe length = 197.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 100.951(CFS)
 Nearest computed pipe diameter = 42.00(In.)
 Calculated individual pipe flow = 100.951(CFS)
 Normal flow depth in pipe = 34.27(In.)
 Flow top width inside pipe = 32.56(In.)
 Critical Depth = 36.95(In.)
 Pipe flow velocity = 12.01(Ft/s)
 Travel time through pipe = 0.27 min.
 Time of concentration (TC) = 10.29 min.

 Process from Point/Station 74.000 to Point/Station 74.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 46.481(Ac.)
Runoff from this stream = 100.951(CFS)
Time of concentration = 10.29 min.
Rainfall intensity = 5.791(In/Hr)

Process from Point/Station 303.000 to Point/Station 304.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 84.000(Ft.)
Highest elevation = 772.000(Ft.)
Lowest elevation = 755.000(Ft.)
Elevation difference = 17.000(Ft.) Slope = 20.238 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 20.24 %, in a development type of
Permanent Open Space
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.90 minutes
(for slope value of 10.00 %)
Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 1.030(CFS)
Total initial stream area = 0.393(Ac.)

Process from Point/Station 304.000 to Point/Station 305.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 4.261(CFS)
Depth of flow = 0.191(Ft.), Average velocity = 2.345(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 2.00
2 100.00 0.00
3 200.00 2.00
Manning's 'N' friction factor = 0.045

Sub-Channel flow = 4.261(CFS)
' ' flow top width = 19.062(Ft.)
' ' velocity = 2.345(Ft/s)
' ' area = 1.817(Sq.Ft)
' ' Froude number = 1.339

Upstream point elevation = 755.000(Ft.)
Downstream point elevation = 704.000(Ft.)
Flow length = 440.000(Ft.)
Travel time = 3.13 min.
Time of concentration = 10.03 min.
Depth of flow = 0.191(Ft.)
Average velocity = 2.345(Ft/s)
Total irregular channel flow = 4.261(CFS)
Irregular channel normal depth above invert elev. = 0.191(Ft.)
Average velocity of channel(s) = 2.345(Ft/s)
Adding area flow to channel

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]

(Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Rainfall intensity = 5.887(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.350 CA = 1.260
 Subarea runoff = 6.387(CFS) for 3.207(Ac.)
 Total runoff = 7.418(CFS) Total area = 3.600(Ac.)
 Depth of flow = 0.235(Ft.), Average velocity = 2.694(Ft/s)

 Process from Point/Station 305.000 to Point/Station 74.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 701.000(Ft.)
 Downstream point/station elevation = 696.000(Ft.)
 Pipe length = 114.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 7.418(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 7.418(CFS)
 Normal flow depth in pipe = 9.77(In.)
 Flow top width inside pipe = 9.33(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 10.83(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 10.20 min.

 Process from Point/Station 74.000 to Point/Station 74.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 3.600(Ac.)
 Runoff from this stream = 7.418(CFS)
 Time of concentration = 10.20 min.
 Rainfall intensity = 5.822(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	100.951	10.29	5.791
2	7.418	10.20	5.822

Qmax(1) =
 1.000 * 1.000 * 100.951) +
 0.995 * 1.000 * 7.418) + = 108.329

Qmax(2) =
 1.000 * 0.992 * 100.951) +
 1.000 * 1.000 * 7.418) + = 107.538

Total of 2 streams to confluence:
 Flow rates before confluence point:
 100.951 7.418
 Maximum flow rates at confluence using above data:
 108.329 107.538
 Area of streams before confluence:
 46.481 3.600
 Results of confluence:
 Total flow rate = 108.329(CFS)
 Time of concentration = 10.287 min.
 Effective stream area after confluence = 50.081(Ac.)

 Process from Point/Station 74.000 to Point/Station 75.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 696.000(Ft.)
 Downstream point/station elevation = 695.500(Ft.)
 Pipe length = 50.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 108.329(CFS)
 Nearest computed pipe diameter = 45.00(In.)
 Calculated individual pipe flow = 108.329(CFS)
 Normal flow depth in pipe = 33.23(In.)
 Flow top width inside pipe = 39.55(In.)
 Critical Depth = 38.04(In.)
 Pipe flow velocity = 12.38(Ft/s)
 Travel time through pipe = 0.07 min.
 Time of concentration (TC) = 10.35 min.

 Process from Point/Station 75.000 to Point/Station 75.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 50.081(Ac.)
 Runoff from this stream = 108.329(CFS)
 Time of concentration = 10.35 min.
 Rainfall intensity = 5.766(In/Hr)

 Process from Point/Station 72.000 to Point/Station 75.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 300.000(Ft.)
 Highest elevation = 710.000(Ft.)
 Lowest elevation = 701.500(Ft.)
 Elevation difference = 8.500(Ft.) Slope = 2.833 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 2.83 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.03 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (2.833^{(1/3)}) = 6.03$
 Rainfall intensity (I) = 8.169(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.103(CFS)
 Total initial stream area = 0.225(Ac.)

 Process from Point/Station 75.000 to Point/Station 75.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.225(Ac.)
 Runoff from this stream = 1.103(CFS)
 Time of concentration = 6.03 min.
 Rainfall intensity = 8.169(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	108.329	10.35	5.766
2	1.103	6.03	8.169

Qmax(1) =
 $1.000 * 108.329 + 0.706 * 1.103 = 109.108$
 Qmax(2) =

$1.000 * 0.583 * 108.329) +$
 $1.000 * 1.000 * 1.103) + = 64.235$

Total of 2 streams to confluence:
 Flow rates before confluence point:
 108.329 1.103
 Maximum flow rates at confluence using above data:
 109.108 64.235
 Area of streams before confluence:
 50.081 0.225
 Results of confluence:
 Total flow rate = 109.108(CFS)
 Time of concentration = 10.354 min.
 Effective stream area after confluence = 50.306(Ac.)

 Process from Point/Station 75.000 to Point/Station 77.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 695.500(Ft.)
 Downstream point/station elevation = 693.500(Ft.)
 Pipe length = 106.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 109.108(CFS)
 Nearest computed pipe diameter = 39.00(In.)
 Calculated individual pipe flow = 109.108(CFS)
 Normal flow depth in pipe = 30.70(In.)
 Flow top width inside pipe = 31.92(In.)
 Critical Depth = 36.94(In.)
 Pipe flow velocity = 15.57(Ft/s)
 Travel time through pipe = 0.11 min.
 Time of concentration (TC) = 10.47 min.

 Process from Point/Station 77.000 to Point/Station 77.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 50.306(Ac.)
 Runoff from this stream = 109.108(CFS)
 Time of concentration = 10.47 min.
 Rainfall intensity = 5.726(In/Hr)

 Process from Point/Station 71.000 to Point/Station 76.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 339.000(Ft.)
 Highest elevation = 708.000(Ft.)
 Lowest elevation = 698.500(Ft.)
 Elevation difference = 9.500(Ft.) Slope = 2.802 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 90.00 (Ft)
 for the top area slope value of 2.80 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.06 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (2.802^{(1/3)}) = 6.06$
 Rainfall intensity (I) = 8.149(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 1.335(CFS)
 Total initial stream area = 0.273(Ac.)

 Process from Point/Station 76.000 to Point/Station 77.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 694.000(Ft.)
 Downstream point/station elevation = 693.500(Ft.)
 Pipe length = 37.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.335(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 1.335(CFS)
 Normal flow depth in pipe = 5.52(In.)
 Flow top width inside pipe = 8.77(In.)
 Critical Depth = 6.39(In.)
 Pipe flow velocity = 4.70(Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 6.19 min.

 Process from Point/Station 77.000 to Point/Station 77.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.273(Ac.)
 Runoff from this stream = 1.335(CFS)
 Time of concentration = 6.19 min.
 Rainfall intensity = 8.037(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	109.108	10.47	5.726
2	1.335	6.19	8.037
Qmax(1) =			
	1.000 *	1.000 *	109.108) +
	0.712 *	1.000 *	1.335) + = 110.059
Qmax(2) =			
	1.000 *	0.591 *	109.108) +
	1.000 *	1.000 *	1.335) + = 65.830

Total of 2 streams to confluence:
 Flow rates before confluence point:
 109.108 1.335
 Maximum flow rates at confluence using above data:
 110.059 65.830
 Area of streams before confluence:
 50.306 0.273
 Results of confluence:
 Total flow rate = 110.059(CFS)
 Time of concentration = 10.467 min.
 Effective stream area after confluence = 50.579(Ac.)

 Process from Point/Station 77.000 to Point/Station 80.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 693.500(Ft.)
 Downstream point/station elevation = 686.500(Ft.)
 Pipe length = 185.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 110.059(CFS)
 Nearest computed pipe diameter = 36.00(In.)
 Calculated individual pipe flow = 110.059(CFS)
 Normal flow depth in pipe = 25.45(In.)
 Flow top width inside pipe = 32.77(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 20.60(Ft/s)
 Travel time through pipe = 0.15 min.
 Time of concentration (TC) = 10.62 min.

Process from Point/Station 80.000 to Point/Station 80.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 50.579(Ac.)
Runoff from this stream = 110.059(CFS)
Time of concentration = 10.62 min.
Rainfall intensity = 5.674(In/Hr)

Process from Point/Station 76.000 to Point/Station 78.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 181.000(Ft.)
Highest elevation = 698.500(Ft.)
Lowest elevation = 693.000(Ft.)
Elevation difference = 5.500(Ft.) Slope = 3.039 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.04 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.89 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5} / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5}) / (3.039^{(1/3)})] = 5.89$
Rainfall intensity (I) = 8.293(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.776(CFS)
Total initial stream area = 0.156(Ac.)

Process from Point/Station 78.000 to Point/Station 79.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.500(Ft.)
Downstream point/station elevation = 688.000(Ft.)
Pipe length = 37.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.776(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.776(CFS)
Normal flow depth in pipe = 3.98(In.)
Flow top width inside pipe = 8.94(In.)
Critical Depth = 4.82(In.)
Pipe flow velocity = 4.12(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 6.04 min.

Process from Point/Station 79.000 to Point/Station 79.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600

Time of concentration = 6.04 min.
 Rainfall intensity = 8.160(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.226
 Subarea runoff = 1.070(CFS) for 0.221(Ac.)
 Total runoff = 1.846(CFS) Total area = 0.377(Ac.)

 Process from Point/Station 79.000 to Point/Station 80.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
 Downstream point/station elevation = 686.500(Ft.)
 Pipe length = 150.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.846(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 1.846(CFS)
 Normal flow depth in pipe = 6.13(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical Depth = 6.95(In.)
 Pipe flow velocity = 4.58(Ft/s)
 Travel time through pipe = 0.55 min.
 Time of concentration (TC) = 6.59 min.

 Process from Point/Station 80.000 to Point/Station 80.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.377(Ac.)
 Runoff from this stream = 1.846(CFS)
 Time of concentration = 6.59 min.
 Rainfall intensity = 7.717(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	110.059	10.62	5.674
2	1.846	6.59	7.717

Qmax(1) =
 1.000 * 1.000 * 110.059) +
 0.735 * 1.000 * 1.846) + = 111.416

Qmax(2) =
 1.000 * 0.621 * 110.059) +
 1.000 * 1.000 * 1.846) + = 70.163

Total of 2 streams to confluence:
 Flow rates before confluence point:
 110.059 1.846
 Maximum flow rates at confluence using above data:
 111.416 70.163
 Area of streams before confluence:
 50.579 0.377
 Results of confluence:
 Total flow rate = 111.416(CFS)
 Time of concentration = 10.617 min.
 Effective stream area after confluence = 50.956(Ac.)
 End of computations, total study area = 50.956 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/15/13

***** Hydrology Study Control Information *****

File: PADPONDD.rd3

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 83.000 to Point/Station 84.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 72.000(Ft.)
Highest elevation = 748.000(Ft.)
Lowest elevation = 747.280(Ft.)
Elevation difference = 0.720(Ft.) Slope = 1.000 %
Top of Initial Area Slope adjusted by User to 0.500 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 50.00 (Ft)
for the top area slope value of 0.50 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 8.70 minutes
(for slope value of 0.50 %)
Rainfall intensity (I) = 6.451(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.453(CFS)
Total initial stream area = 0.117(Ac.)

Process from Point/Station 84.000 to Point/Station 85.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 745.280(Ft.)
Downstream point/station elevation = 730.000(Ft.)
Pipe length = 203.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.453(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.453(CFS)
Normal flow depth in pipe = 2.23(In.)
Flow top width inside pipe = 5.80(In.)
Critical Depth = 4.12(In.)
Pipe flow velocity = 6.82(Ft/s)
Travel time through pipe = 0.50 min.

Time of concentration (TC) = 9.20 min.

Process from Point/Station 85.000 to Point/Station 85.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 9.20 min.
Rainfall intensity = 6.225(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.349
Subarea runoff = 1.717(CFS) for 0.464(Ac.)
Total runoff = 2.170(CFS) Total area = 0.581(Ac.)

Process from Point/Station 85.000 to Point/Station 86.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 730.000(Ft.)
Downstream point/station elevation = 715.000(Ft.)
Pipe length = 154.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.170(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.170(CFS)
Normal flow depth in pipe = 4.07(In.)
Flow top width inside pipe = 8.96(In.)
Critical Depth = 7.95(In.)
Pipe flow velocity = 11.18(Ft/s)
Travel time through pipe = 0.23 min.
Time of concentration (TC) = 9.43 min.

Process from Point/Station 86.000 to Point/Station 86.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 9.43 min.
Rainfall intensity = 6.126(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.547
Subarea runoff = 1.182(CFS) for 0.331(Ac.)
Total runoff = 3.352(CFS) Total area = 0.912(Ac.)

Process from Point/Station 86.000 to Point/Station 87.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 715.000(Ft.)
Downstream point/station elevation = 700.000(Ft.)
Pipe length = 167.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.352(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 3.352(CFS)
Normal flow depth in pipe = 5.43(In.)

Flow top width inside pipe = 8.81(In.)
Critical depth could not be calculated.
Pipe flow velocity = 12.05(Ft/s)
Travel time through pipe = 0.23 min.
Time of concentration (TC) = 9.66 min.

Process from Point/Station 87.000 to Point/Station 87.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 9.66 min.
Rainfall intensity = 6.032(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.813
Subarea runoff = 1.551(CFS) for 0.443(Ac.)
Total runoff = 4.904(CFS) Total area = 1.355(Ac.)

Process from Point/Station 87.000 to Point/Station 88.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 700.000(Ft.)
Downstream point/station elevation = 688.000(Ft.)
Pipe length = 109.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 4.904(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 4.904(CFS)
Normal flow depth in pipe = 6.63(In.)
Flow top width inside pipe = 7.92(In.)
Critical depth could not be calculated.
Pipe flow velocity = 14.05(Ft/s)
Travel time through pipe = 0.13 min.
Time of concentration (TC) = 9.79 min.

Process from Point/Station 88.000 to Point/Station 88.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 1.355(Ac.)
Runoff from this stream = 4.904(CFS)
Time of concentration = 9.79 min.
Rainfall intensity = 5.980(In/Hr)

Process from Point/Station 96.000 to Point/Station 97.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 100.000(Ft.)
Highest elevation = 750.000(Ft.)
Lowest elevation = 749.000(Ft.)
Elevation difference = 1.000(Ft.) Slope = 1.000 %

INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 1.00 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 7.90 minutes
(for slope value of 1.00 %)
Rainfall intensity (I) = 6.865(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.770(CFS)
Total initial stream area = 0.187(Ac.)

Process from Point/Station 97.000 to Point/Station 98.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 747.000(Ft.)
Downstream point/station elevation = 744.000(Ft.)
Pipe length = 81.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.770(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.770(CFS)
Normal flow depth in pipe = 3.74(In.)
Flow top width inside pipe = 5.81(In.)
Critical Depth = 5.25(In.)
Pipe flow velocity = 5.97(Ft/s)
Travel time through pipe = 0.23 min.
Time of concentration (TC) = 8.13 min.

Process from Point/Station 98.000 to Point/Station 98.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.13 min.
Rainfall intensity = 6.742(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.286
Subarea runoff = 1.159(CFS) for 0.290(Ac.)
Total runoff = 1.929(CFS) Total area = 0.477(Ac.)

Process from Point/Station 98.000 to Point/Station 99.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 744.000(Ft.)
Downstream point/station elevation = 732.000(Ft.)
Pipe length = 145.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.929(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.929(CFS)
Normal flow depth in pipe = 3.99(In.)
Flow top width inside pipe = 8.94(In.)
Critical Depth = 7.60(In.)
Pipe flow velocity = 10.21(Ft/s)
Travel time through pipe = 0.24 min.
Time of concentration (TC) = 8.36 min.

Process from Point/Station 99.000 to Point/Station 99.000
**** SUBAREA FLOW ADDITION ****

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.36 min.
Rainfall intensity = 6.618(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.489
Subarea runoff = 1.307(CFS) for 0.338(Ac.)
Total runoff = 3.236(CFS) Total area = 0.815(Ac.)

+++++
Process from Point/Station 99.000 to Point/Station 100.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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```

Upstream point/station elevation = 732.000(Ft.)
Downstream point/station elevation = 717.000(Ft.)
Pipe length = 150.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.236(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 3.236(CFS)
Normal flow depth in pipe = 5.12(In.)
Flow top width inside pipe = 8.91(In.)
Critical depth could not be calculated.
Pipe flow velocity = 12.46(Ft/s)
Travel time through pipe = 0.20 min.
Time of concentration (TC) = 8.56 min.

+++++
Process from Point/Station 100.000 to Point/Station 100.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 8.56 min.
Rainfall intensity = 6.518(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.694
Subarea runoff = 1.284(CFS) for 0.341(Ac.)
Total runoff = 4.521(CFS) Total area = 1.156(Ac.)

+++++
Process from Point/Station 100.000 to Point/Station 101.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation = 717.000(Ft.)
Downstream point/station elevation = 704.000(Ft.)
Pipe length = 150.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 4.521(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 4.521(CFS)
Normal flow depth in pipe = 6.86(In.)
Flow top width inside pipe = 7.67(In.)
Critical depth could not be calculated.
Pipe flow velocity = 12.52(Ft/s)
Travel time through pipe = 0.20 min.
Time of concentration (TC) = 8.76 min.

```

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+++++
Process from Point/Station      101.000 to Point/Station      101.000
**** SUBAREA FLOW ADDITION ****

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```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      8.76 min.
Rainfall intensity =      6.421(In/Hr) for a  100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      0.898
Subarea runoff =      1.243(CFS) for      0.340(Ac.)
Total runoff =      5.764(CFS)          Total area =      1.496(Ac.)

```

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+++++
Process from Point/Station      101.000 to Point/Station      102.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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```

Upstream point/station elevation =  704.000(Ft.)
Downstream point/station elevation =  694.000(Ft.)
Pipe length =  120.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      5.764(CFS)
Nearest computed pipe diameter =      12.00(In.)
Calculated individual pipe flow =      5.764(CFS)
Normal flow depth in pipe =      6.42(In.)
Flow top width inside pipe =  11.97(In.)
Critical Depth =  11.38(In.)
Pipe flow velocity =      13.47(Ft/s)
Travel time through pipe =      0.15 min.
Time of concentration (TC) =      8.91 min.

```

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+++++
Process from Point/Station      102.000 to Point/Station      102.000
**** SUBAREA FLOW ADDITION ****

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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      8.91 min.
Rainfall intensity =      6.352(In/Hr) for a  100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      1.111
Subarea runoff =      1.295(CFS) for      0.356(Ac.)
Total runoff =      7.059(CFS)          Total area =      1.852(Ac.)

```

```

+++++
Process from Point/Station      102.000 to Point/Station      88.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =  690.000(Ft.)
Downstream point/station elevation =  688.000(Ft.)
Pipe length =  64.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      7.059(CFS)
Nearest computed pipe diameter =      15.00(In.)
Calculated individual pipe flow =      7.059(CFS)
Normal flow depth in pipe =      8.53(In.)
Flow top width inside pipe =  14.86(In.)
Critical Depth =  12.76(In.)

```

Pipe flow velocity = 9.79(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 9.02 min.

Process from Point/Station 88.000 to Point/Station 88.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 1.852(Ac.)
Runoff from this stream = 7.059(CFS)
Time of concentration = 9.02 min.
Rainfall intensity = 6.303(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	4.904	9.79	5.980
2	7.059	9.02	6.303

Qmax(1) =
1.000 * 1.000 * 4.904) +
0.949 * 1.000 * 7.059) + = 11.601

Qmax(2) =
1.000 * 0.922 * 4.904) +
1.000 * 1.000 * 7.059) + = 11.579

Total of 2 streams to confluence:
Flow rates before confluence point:
4.904 7.059
Maximum flow rates at confluence using above data:
11.601 11.579
Area of streams before confluence:
1.355 1.852
Results of confluence:
Total flow rate = 11.601(CFS)
Time of concentration = 9.786 min.
Effective stream area after confluence = 3.207(Ac.)

Process from Point/Station 88.000 to Point/Station 89.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
Downstream point/station elevation = 687.000(Ft.)
Pipe length = 43.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 11.601(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 11.601(CFS)
Normal flow depth in pipe = 11.36(In.)
Flow top width inside pipe = 17.37(In.)
Critical Depth = 15.57(In.)
Pipe flow velocity = 9.88(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 9.86 min.

Process from Point/Station 89.000 to Point/Station 89.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600

Time of concentration = 9.86 min.
 Rainfall intensity = 5.952(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 2.159
 Subarea runoff = 1.247(CFS) for 0.391(Ac.)
 Total runoff = 12.848(CFS) Total area = 3.598(Ac.)

 Process from Point/Station 89.000 to Point/Station 90.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
 Downstream point/station elevation = 680.000(Ft.)
 Pipe length = 138.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 12.848(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 12.848(CFS)
 Normal flow depth in pipe = 10.95(In.)
 Flow top width inside pipe = 13.32(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 13.38(Ft/s)
 Travel time through pipe = 0.17 min.
 Time of concentration (TC) = 10.03 min.

 Process from Point/Station 90.000 to Point/Station 90.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 10.03 min.
 Rainfall intensity = 5.886(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 2.372
 Subarea runoff = 1.115(CFS) for 0.356(Ac.)
 Total runoff = 13.963(CFS) Total area = 3.954(Ac.)

 Process from Point/Station 90.000 to Point/Station 91.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 680.000(Ft.)
 Downstream point/station elevation = 676.000(Ft.)
 Pipe length = 167.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 13.963(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 13.963(CFS)
 Normal flow depth in pipe = 12.84(In.)
 Flow top width inside pipe = 16.28(In.)
 Critical Depth = 16.55(In.)
 Pipe flow velocity = 10.34(Ft/s)
 Travel time through pipe = 0.27 min.
 Time of concentration (TC) = 10.30 min.

 Process from Point/Station 91.000 to Point/Station 91.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000

```

[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 10.30 min.
Rainfall intensity = 5.786(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 2.674
Subarea runoff = 1.506(CFS) for 0.502(Ac.)
Total runoff = 15.469(CFS) Total area = 4.456(Ac.)

*****
Process from Point/Station 91.000 to Point/Station 92.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 676.000(Ft.)
Downstream point/station elevation = 667.000(Ft.)
Pipe length = 133.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 15.469(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 15.469(CFS)
Normal flow depth in pipe = 11.34(In.)
Flow top width inside pipe = 12.88(In.)
Critical depth could not be calculated.
Pipe flow velocity = 15.54(Ft/s)
Travel time through pipe = 0.14 min.
Time of concentration (TC) = 10.44 min.

*****
Process from Point/Station 92.000 to Point/Station 92.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 4.456(Ac.)
Runoff from this stream = 15.469(CFS)
Time of concentration = 10.44 min.
Rainfall intensity = 5.735(In/Hr)

*****
Process from Point/Station 103.000 to Point/Station 104.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL
(10.9 DU/A or Less
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 72.000(Ft.)
Highest elevation = 686.000(Ft.)
Lowest elevation = 685.000(Ft.)
Elevation difference = 1.000(Ft.) Slope = 1.389 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 65.00 (Ft)
for the top area slope value of 1.38 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 7.90 minutes
(for slope value of 1.00 %)
Rainfall intensity (I) = 6.865(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.437(CFS)
Total initial stream area = 0.106(Ac.)

*****
Process from Point/Station 104.000 to Point/Station 105.000

```


**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 684.000(Ft.)
 Downstream point/station elevation = 672.000(Ft.)
 Pipe length = 285.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.437(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.437(CFS)
 Normal flow depth in pipe = 2.56(In.)
 Flow top width inside pipe = 5.93(In.)
 Critical Depth = 4.04(In.)
 Pipe flow velocity = 5.46(Ft/s)
 Travel time through pipe = 0.87 min.
 Time of concentration (TC) = 8.77 min.

 Process from Point/Station 105.000 to Point/Station 105.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 8.77 min.
 Rainfall intensity = 6.418(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.473
 Subarea runoff = 2.598(CFS) for 0.682(Ac.)
 Total runoff = 3.034(CFS) Total area = 0.788(Ac.)

 Process from Point/Station 105.000 to Point/Station 92.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 672.000(Ft.)
 Downstream point/station elevation = 667.000(Ft.)
 Pipe length = 86.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 3.034(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 3.034(CFS)
 Normal flow depth in pipe = 5.87(In.)
 Flow top width inside pipe = 8.57(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 9.94(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 8.91 min.

 Process from Point/Station 92.000 to Point/Station 92.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.788(Ac.)
 Runoff from this stream = 3.034(CFS)
 Time of concentration = 8.91 min.
 Rainfall intensity = 6.351(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	15.469	10.44	5.735
2	3.034	8.91	6.351

Qmax(1) =

	1.000 *	1.000 *	15.469) +	
Qmax(2) =	0.903 *	1.000 *	3.034) + =	18.209
	1.000 *	0.854 *	15.469) +	
	1.000 *	1.000 *	3.034) + =	16.241

Total of 2 streams to confluence:
Flow rates before confluence point:
15.469 3.034
Maximum flow rates at confluence using above data:
18.209 16.241
Area of streams before confluence:
4.456 0.788
Results of confluence:
Total flow rate = 18.209(CFS)
Time of concentration = 10.442 min.
Effective stream area after confluence = 5.244(Ac.)

Process from Point/Station 92.000 to Point/Station 93.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 667.000(Ft.)
Downstream point/station elevation = 665.000(Ft.)
Pipe length = 77.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 18.209(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 18.209(CFS)
Normal flow depth in pipe = 13.10(In.)
Flow top width inside pipe = 20.35(In.)
Critical Depth = 18.62(In.)
Pipe flow velocity = 11.53(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 10.55 min.

Process from Point/Station 93.000 to Point/Station 93.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 5.244(Ac.)
Runoff from this stream = 18.209(CFS)
Time of concentration = 10.55 min.
Rainfall intensity = 5.696(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 106.000 to Point/Station 107.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 84.000(Ft.)
Highest elevation = 710.500(Ft.)
Lowest elevation = 710.000(Ft.)
Elevation difference = 0.500(Ft.) Slope = 0.595 %
Top of Initial Area Slope adjusted by User to 0.562 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 50.00 (Ft)
for the top area slope value of 0.56 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2

Initial Area Time of Concentration = 8.70 minutes
(for slope value of 0.50 %)
Rainfall intensity (I) = 6.451(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.557(CFS)
Total initial stream area = 0.144(Ac.)

Process from Point/Station 107.000 to Point/Station 109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 707.000(Ft.)
Downstream point/station elevation = 695.000(Ft.)
Pipe length = 467.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.557(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.557(CFS)
Normal flow depth in pipe = 3.42(In.)
Flow top width inside pipe = 5.94(In.)
Critical Depth = 4.56(In.)
Pipe flow velocity = 4.83(Ft/s)
Travel time through pipe = 1.61 min.
Time of concentration (TC) = 10.31 min.

Process from Point/Station 109.000 to Point/Station 109.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 10.31 min.
Rainfall intensity = 5.781(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.759
Subarea runoff = 3.830(CFS) for 1.121(Ac.)
Total runoff = 4.388(CFS) Total area = 1.265(Ac.)

Process from Point/Station 109.000 to Point/Station 109.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 1.265(Ac.)
Runoff from this stream = 4.388(CFS)
Time of concentration = 10.31 min.
Rainfall intensity = 5.781(In/Hr)

Process from Point/Station 108.000 to Point/Station 108.100
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 68.000(Ft.)
Highest elevation = 695.000(Ft.)
Lowest elevation = 694.500(Ft.)

Elevation difference = 0.500(Ft.) Slope = 0.735 %
 Top of Initial Area Slope adjusted by User to 0.500 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 50.00 (Ft)
 for the top area slope value of 0.50 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 8.70 minutes
 (for slope value of 0.50 %)
 Rainfall intensity (I) = 6.451(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.824(CFS)
 Total initial stream area = 0.213(Ac.)

 Process from Point/Station 108.100 to Point/Station 109.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 692.500(Ft.)
 Downstream point/station elevation = 691.500(Ft.)
 Pipe length = 92.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.824(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 0.824(CFS)
 Normal flow depth in pipe = 4.38(In.)
 Flow top width inside pipe = 9.00(In.)
 Critical Depth = 4.97(In.)
 Pipe flow velocity = 3.86(Ft/s)
 Travel time through pipe = 0.40 min.
 Time of concentration (TC) = 9.10 min.

 Process from Point/Station 109.000 to Point/Station 109.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.213(Ac.)
 Runoff from this stream = 0.824(CFS)
 Time of concentration = 9.10 min.
 Rainfall intensity = 6.268(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	4.388	10.31	5.781
2	0.824	9.10	6.268
Qmax(1) =			
	1.000 *	1.000 *	4.388) +
	0.922 *	1.000 *	0.824) + =
			5.148
Qmax(2) =			
	1.000 *	0.882 *	4.388) +
	1.000 *	1.000 *	0.824) + =
			4.695

Total of 2 streams to confluence:
 Flow rates before confluence point:
 4.388 0.824
 Maximum flow rates at confluence using above data:
 5.148 4.695
 Area of streams before confluence:
 1.265 0.213
 Results of confluence:
 Total flow rate = 5.148(CFS)
 Time of concentration = 10.313 min.
 Effective stream area after confluence = 1.478(Ac.)

 Process from Point/Station 109.000 to Point/Station 111.000

**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.500(Ft.)
 Downstream point/station elevation = 690.500(Ft.)
 Pipe length = 103.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 5.148(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 5.148(CFS)
 Normal flow depth in pipe = 10.23(In.)
 Flow top width inside pipe = 13.97(In.)
 Critical Depth = 11.04(In.)
 Pipe flow velocity = 5.77(Ft/s)
 Travel time through pipe = 0.30 min.
 Time of concentration (TC) = 10.61 min.

 Process from Point/Station 111.000 to Point/Station 111.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 1.478(Ac.)
 Runoff from this stream = 5.148(CFS)
 Time of concentration = 10.61 min.
 Rainfall intensity = 5.676(In/Hr)

 Process from Point/Station 110.000 to Point/Station 111.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 95.000(Ft.)
 Highest elevation = 698.000(Ft.)
 Lowest elevation = 697.000(Ft.)
 Elevation difference = 1.000(Ft.) Slope = 1.053 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 65.00 (Ft)
 for the top area slope value of 1.05 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 7.90 minutes
 (for slope value of 1.00 %)
 Rainfall intensity (I) = 6.865(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.362(CFS)
 Total initial stream area = 0.088(Ac.)

 Process from Point/Station 111.000 to Point/Station 111.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.088(Ac.)
 Runoff from this stream = 0.362(CFS)
 Time of concentration = 7.90 min.
 Rainfall intensity = 6.865(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	5.148	10.61	5.676

```

2          0.362      7.90          6.865
Qmax(1) =
      1.000 *      1.000 *      5.148) +
      0.827 *      1.000 *      0.362) + =      5.448
Qmax(2) =
      1.000 *      0.745 *      5.148) +
      1.000 *      1.000 *      0.362) + =      4.196

```

```

Total of 2 streams to confluence:
Flow rates before confluence point:
      5.148      0.362
Maximum flow rates at confluence using above data:
      5.448      4.196
Area of streams before confluence:
      1.478      0.088
Results of confluence:
Total flow rate =      5.448(CFS)
Time of concentration =      10.610 min.
Effective stream area after confluence =      1.566(Ac.)

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Process from Point/Station      111.000 to Point/Station      112.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

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```

Upstream point/station elevation =      690.500(Ft.)
Downstream point/station elevation =      689.000(Ft.)
Pipe length =      129.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      5.448(CFS)
Nearest computed pipe diameter =      15.00(In.)
Calculated individual pipe flow =      5.448(CFS)
Normal flow depth in pipe =      9.98(In.)
Flow top width inside pipe =      14.15(In.)
Critical Depth =      11.36(In.)
Pipe flow velocity =      6.28(Ft/s)
Travel time through pipe =      0.34 min.
Time of concentration (TC) =      10.95 min.

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Process from Point/Station      112.000 to Point/Station      112.000
**** SUBAREA FLOW ADDITION ****

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```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      10.95 min.
Rainfall intensity =      5.561(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600  CA =      1.129
Subarea runoff =      0.828(CFS) for      0.315(Ac.)
Total runoff =      6.276(CFS)      Total area =      1.881(Ac.)

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Process from Point/Station      112.000 to Point/Station      113.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      689.000(Ft.)
Downstream point/station elevation =      687.000(Ft.)
Pipe length =      130.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      6.276(CFS)
Nearest computed pipe diameter =      15.00(In.)
Calculated individual pipe flow =      6.276(CFS)
Normal flow depth in pipe =      10.00(In.)
Flow top width inside pipe =      14.14(In.)
Critical Depth =      12.13(In.)

```

Pipe flow velocity = 7.23(Ft/s)
Travel time through pipe = 0.30 min.
Time of concentration (TC) = 11.25 min.

Process from Point/Station 113.000 to Point/Station 113.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 11.25 min.
Rainfall intensity = 5.465(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 1.311
Subarea runoff = 0.888(CFS) for 0.304(Ac.)
Total runoff = 7.165(CFS) Total area = 2.185(Ac.)

Process from Point/Station 113.000 to Point/Station 114.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
Downstream point/station elevation = 682.000(Ft.)
Pipe length = 130.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 7.165(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 7.165(CFS)
Normal flow depth in pipe = 8.07(In.)
Flow top width inside pipe = 14.96(In.)
Critical Depth = 12.83(In.)
Pipe flow velocity = 10.64(Ft/s)
Travel time through pipe = 0.20 min.
Time of concentration (TC) = 11.46 min.

Process from Point/Station 114.000 to Point/Station 114.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 11.46 min.
Rainfall intensity = 5.402(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 1.487
Subarea runoff = 0.867(CFS) for 0.293(Ac.)
Total runoff = 8.032(CFS) Total area = 2.478(Ac.)

Process from Point/Station 114.000 to Point/Station 115.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 682.000(Ft.)
Downstream point/station elevation = 678.000(Ft.)
Pipe length = 130.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 8.032(CFS)
Nearest computed pipe diameter = 15.00(In.)

Calculated individual pipe flow = 8.032(CFS)
Normal flow depth in pipe = 9.33(In.)
Flow top width inside pipe = 14.55(In.)
Critical Depth = 13.39(In.)
Pipe flow velocity = 10.02(Ft/s)
Travel time through pipe = 0.22 min.
Time of concentration (TC) = 11.67 min.

Process from Point/Station 115.000 to Point/Station 115.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 11.67 min.
Rainfall intensity = 5.337(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 1.663
Subarea runoff = 0.842(CFS) for 0.293(Ac.)
Total runoff = 8.874(CFS) Total area = 2.771(Ac.)

Process from Point/Station 115.000 to Point/Station 116.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 678.000(Ft.)
Downstream point/station elevation = 674.000(Ft.)
Pipe length = 103.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 8.874(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 8.874(CFS)
Normal flow depth in pipe = 9.22(In.)
Flow top width inside pipe = 14.60(In.)
Critical Depth = 13.82(In.)
Pipe flow velocity = 11.21(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 11.83 min.

Process from Point/Station 116.000 to Point/Station 116.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 11.83 min.
Rainfall intensity = 5.293(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 1.940
Subarea runoff = 1.396(CFS) for 0.463(Ac.)
Total runoff = 10.270(CFS) Total area = 3.234(Ac.)

Process from Point/Station 116.000 to Point/Station 116.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1

Stream flow area = 3.234(Ac.)
Runoff from this stream = 10.270(CFS)
Time of concentration = 11.83 min.
Rainfall intensity = 5.293(In/Hr)

Process from Point/Station 117.000 to Point/Station 118.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 100.000(Ft.)
Highest elevation = 697.000(Ft.)
Lowest elevation = 694.000(Ft.)
Elevation difference = 3.000(Ft.) Slope = 3.000 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.00 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.40 minutes
(for slope value of 3.00 %)
Rainfall intensity (I) = 7.864(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.708(CFS)
Total initial stream area = 0.150(Ac.)

Process from Point/Station 118.000 to Point/Station 119.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 694.000(Ft.)
Downstream point/station elevation = 690.000(Ft.)
Pipe length = 130.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.708(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.708(CFS)
Normal flow depth in pipe = 3.77(In.)
Flow top width inside pipe = 5.80(In.)
Critical Depth = 5.09(In.)
Pipe flow velocity = 5.45(Ft/s)
Travel time through pipe = 0.40 min.
Time of concentration (TC) = 6.80 min.

Process from Point/Station 119.000 to Point/Station 119.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.80 min.
Rainfall intensity = 7.565(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.311
Subarea runoff = 1.643(CFS) for 0.368(Ac.)
Total runoff = 2.351(CFS) Total area = 0.518(Ac.)

Process from Point/Station 119.000 to Point/Station 120.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 690.000(Ft.)
Downstream point/station elevation = 685.000(Ft.)
Pipe length = 128.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.351(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.351(CFS)
Normal flow depth in pipe = 5.65(In.)
Flow top width inside pipe = 8.70(In.)
Critical Depth = 8.16(In.)
Pipe flow velocity = 8.05(Ft/s)
Travel time through pipe = 0.26 min.
Time of concentration (TC) = 7.06 min.

Process from Point/Station 120.000 to Point/Station 120.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.06 min.
Rainfall intensity = 7.380(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.530
Subarea runoff = 1.559(CFS) for 0.365(Ac.)
Total runoff = 3.910(CFS) Total area = 0.883(Ac.)

Process from Point/Station 120.000 to Point/Station 121.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 685.000(Ft.)
Downstream point/station elevation = 680.000(Ft.)
Pipe length = 174.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.910(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.910(CFS)
Normal flow depth in pipe = 7.03(In.)
Flow top width inside pipe = 11.82(In.)
Critical Depth = 10.08(In.)
Pipe flow velocity = 8.18(Ft/s)
Travel time through pipe = 0.35 min.
Time of concentration (TC) = 7.42 min.

Process from Point/Station 121.000 to Point/Station 121.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.42 min.
Rainfall intensity = 7.151(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area

```

(Q=KCIA) is C = 0.600  CA = 0.826
Subarea runoff = 1.994(CFS) for 0.493(Ac.)
Total runoff = 5.904(CFS) Total area = 1.376(Ac.)

+++++
Process from Point/Station 121.000 to Point/Station 122.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 680.000(Ft.)
Downstream point/station elevation = 675.000(Ft.)
Pipe length = 182.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 5.904(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 5.904(CFS)
Normal flow depth in pipe = 9.84(In.)
Flow top width inside pipe = 9.22(In.)
Critical depth could not be calculated.
Pipe flow velocity = 8.57(Ft/s)
Travel time through pipe = 0.35 min.
Time of concentration (TC) = 7.77 min.

+++++
Process from Point/Station 122.000 to Point/Station 122.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 7.77 min.
Rainfall intensity = 6.939(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 1.141
Subarea runoff = 2.015(CFS) for 0.526(Ac.)
Total runoff = 7.919(CFS) Total area = 1.902(Ac.)

+++++
Process from Point/Station 122.000 to Point/Station 116.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 675.000(Ft.)
Downstream point/station elevation = 674.000(Ft.)
Pipe length = 81.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 7.919(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 7.919(CFS)
Normal flow depth in pipe = 10.88(In.)
Flow top width inside pipe = 17.61(In.)
Critical Depth = 13.09(In.)
Pipe flow velocity = 7.10(Ft/s)
Travel time through pipe = 0.19 min.
Time of concentration (TC) = 7.96 min.

+++++
Process from Point/Station 116.000 to Point/Station 116.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
Stream flow area = 1.902(Ac.)
Runoff from this stream = 7.919(CFS)
Time of concentration = 7.96 min.
Rainfall intensity = 6.832(In/Hr)
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	10.270	11.83	5.293
2	7.919	7.96	6.832

Qmax(1) =
 1.000 * 1.000 * 10.270) +
 0.775 * 1.000 * 7.919) + = 16.405
 Qmax(2) =
 1.000 * 0.673 * 10.270) +
 1.000 * 1.000 * 7.919) + = 14.832

Total of 2 streams to confluence:
 Flow rates before confluence point:
 10.270 7.919
 Maximum flow rates at confluence using above data:
 16.405 14.832
 Area of streams before confluence:
 3.234 1.902
 Results of confluence:
 Total flow rate = 16.405(CFS)
 Time of concentration = 11.825 min.
 Effective stream area after confluence = 5.136(Ac.)

 Process from Point/Station 116.000 to Point/Station 93.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 674.000(Ft.)
 Downstream point/station elevation = 665.000(Ft.)
 Pipe length = 186.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 16.405(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 16.405(CFS)
 Normal flow depth in pipe = 11.20(In.)
 Flow top width inside pipe = 17.45(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 14.19(Ft/s)
 Travel time through pipe = 0.22 min.
 Time of concentration (TC) = 12.04 min.

 Process from Point/Station 93.000 to Point/Station 93.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 5.136(Ac.)
 Runoff from this stream = 16.405(CFS)
 Time of concentration = 12.04 min.
 Rainfall intensity = 5.231(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	18.209	10.55	5.696
2	16.405	12.04	5.231

Qmax(1) =
 1.000 * 1.000 * 18.209) +
 1.000 * 0.876 * 16.405) + = 32.584
 Qmax(2) =
 0.918 * 1.000 * 18.209) +
 1.000 * 1.000 * 16.405) + = 33.127

Total of 2 main streams to confluence:
 Flow rates before confluence point:
 18.209 16.405

Maximum flow rates at confluence using above data:

32.584	33.127
Area of streams before confluence:	
5.244	5.136

Results of confluence:

Total flow rate = 33.127(CFS)
Time of concentration = 12.044 min.
Effective stream area after confluence = 10.380(Ac.)

Process from Point/Station 93.000 to Point/Station 93.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 12.04 min.
Rainfall intensity = 5.231(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 6.599
Subarea runoff = 1.388(CFS) for 0.618(Ac.)
Total runoff = 34.516(CFS) Total area = 10.998(Ac.)

Process from Point/Station 93.000 to Point/Station 94.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 665.000(Ft.)
Downstream point/station elevation = 662.000(Ft.)
Pipe length = 20.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 34.516(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 34.516(CFS)
Normal flow depth in pipe = 12.73(In.)
Flow top width inside pipe = 16.38(In.)
Critical depth could not be calculated.
Pipe flow velocity = 25.83(Ft/s)
Travel time through pipe = 0.01 min.
Time of concentration (TC) = 12.06 min.

Process from Point/Station 94.000 to Point/Station 94.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 10.998(Ac.)
Runoff from this stream = 34.516(CFS)
Time of concentration = 12.06 min.
Rainfall intensity = 5.227(In/Hr)

Process from Point/Station 117.000 to Point/Station 118.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000

Sub-Area C Value = 0.350
 Initial subarea total flow distance = 100.000(Ft.)
 Highest elevation = 703.000(Ft.)
 Lowest elevation = 694.000(Ft.)
 Elevation difference = 9.000(Ft.) Slope = 9.000 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 9.00 %, in a development type of
 Permanent Open Space
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 6.90 minutes
 (for slope value of 10.00 %)
 Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
 Subarea runoff = 0.134(CFS)
 Total initial stream area = 0.051(Ac.)

 Process from Point/Station 118.000 to Point/Station 94.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 2.011(CFS)
 Depth of flow = 0.435(Ft.), Average velocity = 7.089(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 1.00
 2 2.00 0.00
 3 4.00 2.00
 Manning's 'N' friction factor = 0.014

 Sub-Channel flow = 2.011(CFS)
 ' ' flow top width = 1.305(Ft.)
 ' ' velocity = 7.089(Ft/s)
 ' ' area = 0.284(Sq.Ft)
 ' ' Froude number = 2.679

Upstream point elevation = 694.000(Ft.)
 Downstream point elevation = 662.000(Ft.)
 Flow length = 722.000(Ft.)
 Travel time = 1.70 min.
 Time of concentration = 8.60 min.
 Depth of flow = 0.435(Ft.)
 Average velocity = 7.089(Ft/s)
 Total irregular channel flow = 2.011(CFS)
 Irregular channel normal depth above invert elev. = 0.435(Ft.)
 Average velocity of channel(s) = 7.089(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Rainfall intensity = 6.501(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.350 CA = 0.586
 Subarea runoff = 3.677(CFS) for 1.624(Ac.)
 Total runoff = 3.811(CFS) Total area = 1.675(Ac.)
 Depth of flow = 0.553(Ft.), Average velocity = 8.318(Ft/s)

 Process from Point/Station 94.000 to Point/Station 94.000
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 1.675(Ac.)

Runoff from this stream = 3.811(CFS)
 Time of concentration = 8.60 min.
 Rainfall intensity = 6.501(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	34.516	12.06	5.227
2	3.811	8.60	6.501

Qmax(1) =
 1.000 * 1.000 * 34.516) +
 0.804 * 1.000 * 3.811) + = 37.580
 Qmax(2) =
 1.000 * 0.713 * 34.516) +
 1.000 * 1.000 * 3.811) + = 28.423

Total of 2 streams to confluence:
 Flow rates before confluence point:
 34.516 3.811
 Maximum flow rates at confluence using above data:
 37.580 28.423
 Area of streams before confluence:
 10.998 1.675
 Results of confluence:
 Total flow rate = 37.580(CFS)
 Time of concentration = 12.057 min.
 Effective stream area after confluence = 12.673(Ac.)

++++++
 Process from Point/Station 94.000 to Point/Station 81.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 656.500(Ft.)
 Downstream point/station elevation = 655.700(Ft.)
 Pipe length = 73.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 37.580(CFS)
 Nearest computed pipe diameter = 30.00(In.)
 Calculated individual pipe flow = 37.580(CFS)
 Normal flow depth in pipe = 21.75(In.)
 Flow top width inside pipe = 26.79(In.)
 Critical Depth = 24.87(In.)
 Pipe flow velocity = 9.86(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 12.18 min.
 End of computations, total study area = 12.673 (Ac.)

Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 10:26 AM

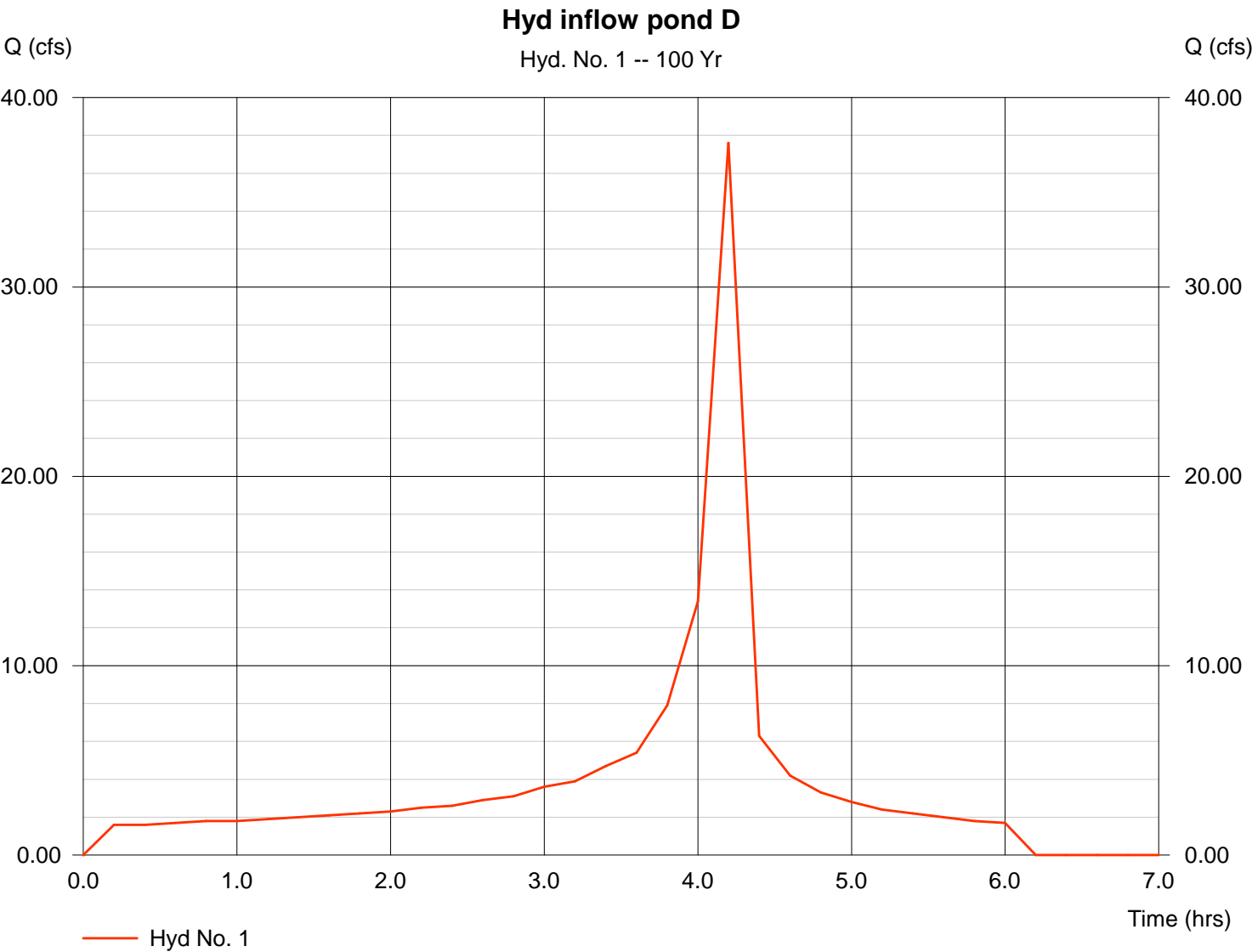
Hyd. No. 1

Hyd inflow pond D

Hydrograph type = Manual
Storm frequency = 100 yrs

Peak discharge = 37.60 cfs
Time interval = 12 min

Hydrograph Volume = 95,976 cuft



Hydrograph Plot

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 10:27 AM

Hyd. No. 2

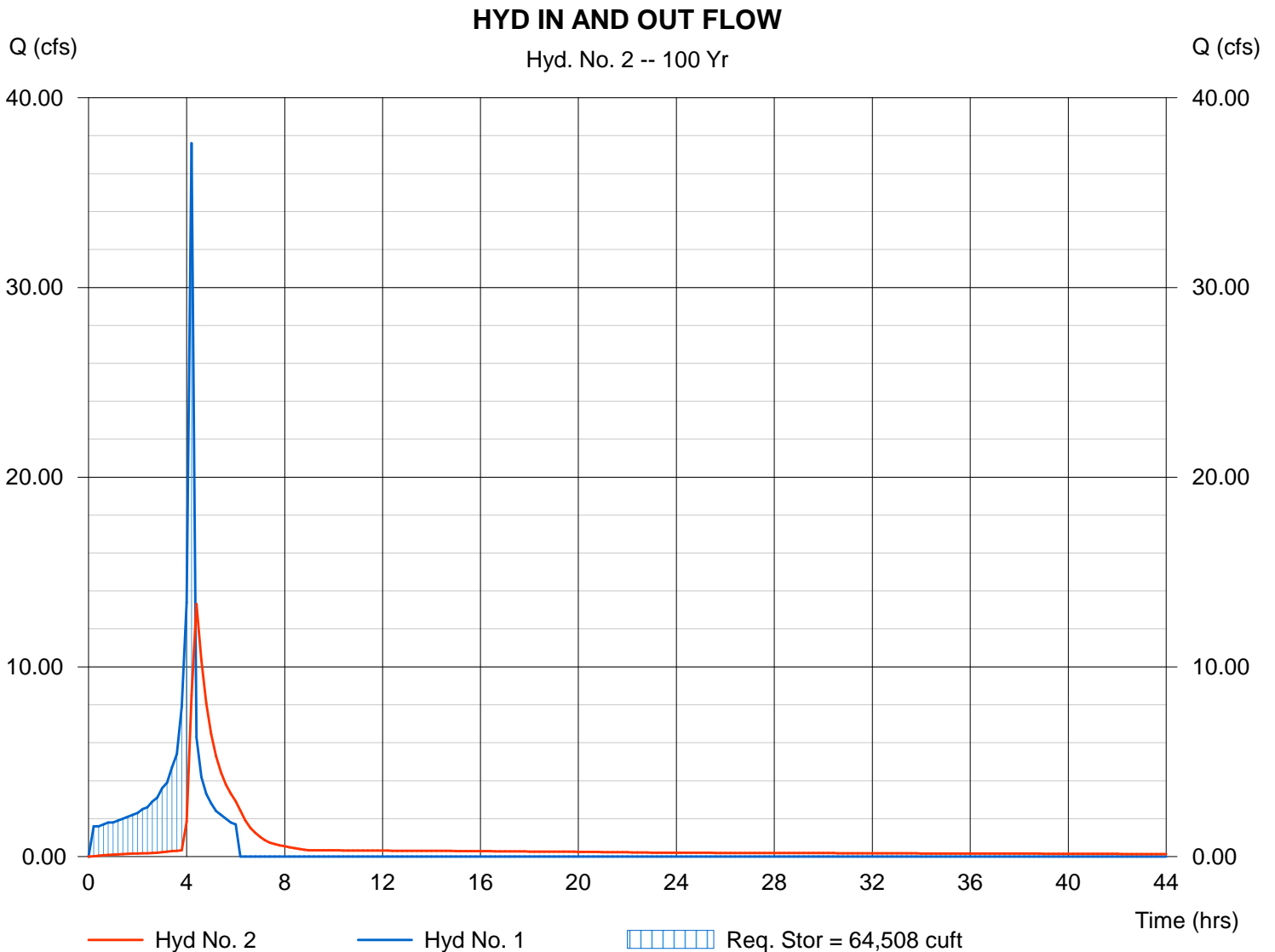
HYD IN AND OUT FLOW

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Inflow hyd. No. = 1
Reservoir name = Bio-pond WQ - D

Peak discharge = 13.32 cfs
Time interval = 12 min
Max. Elevation = 662.98 ft
Max. Storage = 64,508 cuft

Storage Indication method used.

Hydrograph Volume = 95,949 cuft



Pond Report

Hydraflow Hydrographs by Intelisolve

Monday, Jul 22 2013, 10:28 AM

Pond No. 1 - Bio-pond WQ - D

Pond Data

Pond storage is based on known values

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	657.00	00	0	0
2.00	659.00	00	9,632	9,632
4.00	661.00	00	11,008	20,640
4.50	661.50	00	7,009	27,649
5.00	662.00	00	7,319	34,968
6.00	663.00	00	30,004	64,972

Culvert / Orifice Structures

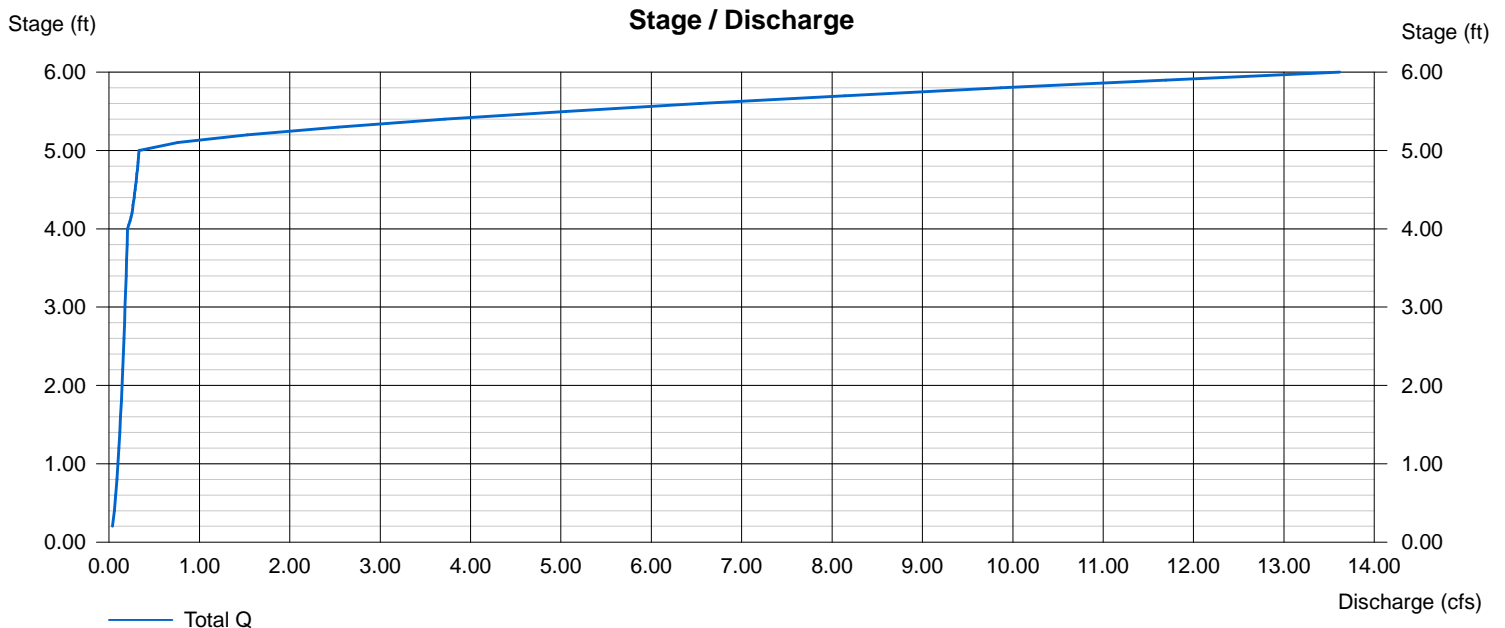
	[A]	[B]	[C]	[D]
Rise (in)	= 18.00	2.00	1.00	0.00
Span (in)	= 18.00	2.00	1.00	0.00
No. Barrels	= 1	1	4	0
Invert El. (ft)	= 657.00	657.00	661.00	0.00
Length (ft)	= 160.00	0.00	0.00	0.00
Slope (%)	= 1.00	0.00	0.00	0.00
N-Value	= .013	.013	.013	.013
Orif. Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	Yes	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 4.00	15.00	0.00	0.00
Crest El. (ft)	= 662.00	663.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Rect	---	---
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Wet area) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.



San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/18/13

OUTFALL 3 - STREET A (NW PORTION), ST B, ST C, AND ST D.
POST DEVELOPMENT AFTER DETENTION
100 Year Storm Event
File Name: D12052OUTFALL3.RD3

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 90.000(Ft.)
Highest elevation = 750.000(Ft.)
Lowest elevation = 745.000(Ft.)
Elevation difference = 5.000(Ft.) Slope = 5.556 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 5.56 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 5.70 minutes
(for slope value of 5.00 %)
Rainfall intensity (I) = 8.474(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.336(CFS)
Total initial stream area = 0.066(Ac.)

Process from Point/Station 2.000 to Point/Station 3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 737.000(Ft.)
Downstream point/station elevation = 732.000(Ft.)
Pipe length = 54.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.336(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.336(CFS)

Normal flow depth in pipe = 1.80(In.)
Flow top width inside pipe = 5.50(In.)
Critical Depth = 3.52(In.)
Pipe flow velocity = 6.76(Ft/s)
Travel time through pipe = 0.13 min.
Time of concentration (TC) = 5.83 min.

Process from Point/Station 3.000 to Point/Station 3.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.83 min.
Rainfall intensity = 8.349(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.077
Subarea runoff = 0.306(CFS) for 0.062(Ac.)
Total runoff = 0.641(CFS) Total area = 0.128(Ac.)

Process from Point/Station 3.000 to Point/Station 4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 732.000(Ft.)
Downstream point/station elevation = 727.000(Ft.)
Pipe length = 54.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.641(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.641(CFS)
Normal flow depth in pipe = 2.55(In.)
Flow top width inside pipe = 5.93(In.)
Critical Depth = 4.88(In.)
Pipe flow velocity = 8.08(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 5.94 min.

Process from Point/Station 4.000 to Point/Station 4.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.94 min.
Rainfall intensity = 8.248(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.115
Subarea runoff = 0.304(CFS) for 0.063(Ac.)
Total runoff = 0.945(CFS) Total area = 0.191(Ac.)

Process from Point/Station 4.000 to Point/Station 5.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 727.000(Ft.)

Downstream point/station elevation = 717.000(Ft.)
Pipe length = 100.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.945(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.945(CFS)
Normal flow depth in pipe = 3.11(In.)
Flow top width inside pipe = 6.00(In.)
Critical Depth = 5.60(In.)
Pipe flow velocity = 9.18(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 6.13 min.

Process from Point/Station 5.000 to Point/Station 5.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.13 min.
Rainfall intensity = 8.089(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.160
Subarea runoff = 0.351(CFS) for 0.076(Ac.)
Total runoff = 1.296(CFS) Total area = 0.267(Ac.)

Process from Point/Station 5.000 to Point/Station 6.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 717.000(Ft.)
Downstream point/station elevation = 710.000(Ft.)
Pipe length = 110.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.296(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.296(CFS)
Normal flow depth in pipe = 4.51(In.)
Flow top width inside pipe = 5.18(In.)
Critical depth could not be calculated.
Pipe flow velocity = 8.17(Ft/s)
Travel time through pipe = 0.22 min.
Time of concentration (TC) = 6.35 min.

Process from Point/Station 6.000 to Point/Station 6.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.35 min.
Rainfall intensity = 7.904(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.205
Subarea runoff = 0.321(CFS) for 0.074(Ac.)
Total runoff = 1.617(CFS) Total area = 0.341(Ac.)

```

*****
Process from Point/Station      6.000 to Point/Station      6.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 0.341(Ac.)
 Runoff from this stream = 1.617(CFS)
 Time of concentration = 6.35 min.
 Rainfall intensity = 7.904(In/Hr)

```

*****
Process from Point/Station      6.100 to Point/Station      6.100
**** USER DEFINED FLOW INFORMATION AT A POINT ****

```

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [UNDISTURBED NATURAL TERRAIN]
 (Permanent Open Space)
 Impervious value, Ai = 0.000
 Sub-Area C Value = 0.350
 Rainfall intensity (I) = 4.747(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 14.00 min. Rain intensity = 4.75(In/Hr)
 Total area = 30.120(Ac.) Total runoff = 53.150(CFS)

```

*****
Process from Point/Station      6.100 to Point/Station      6.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 695.000(Ft.)
 Downstream point/station elevation = 692.400(Ft.)
 Pipe length = 160.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 53.150(CFS)
 Nearest computed pipe diameter = 33.00(In.)
 Calculated individual pipe flow = 53.150(CFS)
 Normal flow depth in pipe = 22.08(In.)
 Flow top width inside pipe = 31.06(In.)
 Critical Depth = 28.62(In.)
 Pipe flow velocity = 12.57(Ft/s)
 Travel time through pipe = 0.21 min.
 Time of concentration (TC) = 14.21 min.

```

*****
Process from Point/Station      6.000 to Point/Station      6.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 30.120(Ac.)
 Runoff from this stream = 53.150(CFS)
 Time of concentration = 14.21 min.
 Rainfall intensity = 4.701(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.617	6.35	7.904
2	53.150	14.21	4.701
Qmax(1) =			
	1.000 *	1.000 *	1.617) +
	1.000 *	0.447 *	53.150) + = 25.367
Qmax(2) =			
	0.595 *	1.000 *	1.617) +
	1.000 *	1.000 *	53.150) + = 54.112

```

+++++
Process from Point/Station      6.000 to Point/Station      13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

+++++
Process from Point/Station      13.000 to Point/Station      13.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

+++++
Process from Point/Station      1.000 to Point/Station      7.000
**** INITIAL AREA EVALUATION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL ]
(10.9 DU/A or Less )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 94.000(Ft.)
Highest elevation = 750.000(Ft.)
Lowest elevation = 745.000(Ft.)
Elevation difference = 5.000(Ft.) Slope = 5.319 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 5.32 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 5.70 minutes
(for slope value of 5.00 %)
Rainfall intensity (I) = 8.474(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.422(CFS)
Total initial stream area = 0.083(Ac.)

```


(Q=KCIA) is C = 0.600 CA = 0.118
Subarea runoff = 0.254(CFS) for 0.053(Ac.)
Total runoff = 0.975(CFS) Total area = 0.197(Ac.)

Process from Point/Station 9.000 to Point/Station 10.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 729.000(Ft.)
Downstream point/station elevation = 722.000(Ft.)
Pipe length = 77.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.975(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.975(CFS)
Normal flow depth in pipe = 3.27(In.)
Flow top width inside pipe = 5.98(In.)
Critical Depth = 5.64(In.)
Pipe flow velocity = 8.92(Ft/s)
Travel time through pipe = 0.14 min.
Time of concentration (TC) = 6.08 min.

Process from Point/Station 10.000 to Point/Station 10.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.08 min.
Rainfall intensity = 8.125(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.151
Subarea runoff = 0.248(CFS) for 0.054(Ac.)
Total runoff = 1.224(CFS) Total area = 0.251(Ac.)

Process from Point/Station 10.000 to Point/Station 11.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 722.000(Ft.)
Downstream point/station elevation = 712.000(Ft.)
Pipe length = 99.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.224(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.224(CFS)
Normal flow depth in pipe = 3.65(In.)
Flow top width inside pipe = 5.86(In.)
Critical depth could not be calculated.
Pipe flow velocity = 9.79(Ft/s)
Travel time through pipe = 0.17 min.
Time of concentration (TC) = 6.25 min.

Process from Point/Station 11.000 to Point/Station 11.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)

Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.25 min.
Rainfall intensity = 7.983(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.191
Subarea runoff = 0.304(CFS) for 0.068(Ac.)
Total runoff = 1.528(CFS) Total area = 0.319(Ac.)

Process from Point/Station 11.000 to Point/Station 12.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 712.000(Ft.)
Downstream point/station elevation = 709.000(Ft.)
Pipe length = 99.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.528(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.528(CFS)
Normal flow depth in pipe = 4.66(In.)
Flow top width inside pipe = 8.99(In.)
Critical Depth = 6.83(In.)
Pipe flow velocity = 6.62(Ft/s)
Travel time through pipe = 0.25 min.
Time of concentration (TC) = 6.50 min.

Process from Point/Station 12.000 to Point/Station 12.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 6.50 min.
Rainfall intensity = 7.784(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.224
Subarea runoff = 0.219(CFS) for 0.055(Ac.)
Total runoff = 1.747(CFS) Total area = 0.374(Ac.)

Process from Point/Station 12.000 to Point/Station 13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 709.000(Ft.)
Downstream point/station elevation = 692.000(Ft.)
Pipe length = 34.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.747(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.747(CFS)
Normal flow depth in pipe = 2.79(In.)
Flow top width inside pipe = 5.98(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.57(Ft/s)
Travel time through pipe = 0.03 min.
Time of concentration (TC) = 6.53 min.

Process from Point/Station 13.000 to Point/Station 13.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 0.374(Ac.)
 Runoff from this stream = 1.747(CFS)
 Time of concentration = 6.53 min.
 Rainfall intensity = 7.761(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	54.112	14.22	4.699
2	1.747	6.53	7.761

Qmax(1) =
 1.000 * 1.000 * 54.112) +
 0.605 * 1.000 * 1.747) + = 55.169

Qmax(2) =
 1.000 * 0.459 * 54.112) +
 1.000 * 1.000 * 1.747) + = 26.600

Total of 2 streams to confluence:
 Flow rates before confluence point:
 54.112 1.747

Maximum flow rates at confluence using above data:
 55.169 26.600

Area of streams before confluence:
 30.461 0.374

Results of confluence:
 Total flow rate = 55.169(CFS)
 Time of concentration = 14.222 min.
 Effective stream area after confluence = 30.835(Ac.)

 Process from Point/Station 13.000 to Point/Station 14.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 692.000(Ft.)
 Downstream point/station elevation = 691.300(Ft.)
 Pipe length = 83.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 55.169(CFS)
 Nearest computed pipe diameter = 36.00(In.)
 Calculated individual pipe flow = 55.169(CFS)
 Normal flow depth in pipe = 26.72(In.)
 Flow top width inside pipe = 31.49(In.)
 Critical Depth = 28.94(In.)
 Pipe flow velocity = 9.81(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 14.36 min.

 Process from Point/Station 14.000 to Point/Station 14.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 The area added to the existing stream causes a
 a lower flow rate of Q = 51.409(CFS)
 therefore the upstream flow rate of Q = 55.169(CFS) is being used
 Time of concentration = 14.36 min.
 Rainfall intensity = 4.669(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.356 CA = 11.011
 Subarea runoff = 0.000(CFS) for 0.066(Ac.)
 Total runoff = 55.169(CFS) Total area = 30.901(Ac.)

```

*****
Process from Point/Station      14.000 to Point/Station      14.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 30.901(Ac.)
 Runoff from this stream = 55.169(CFS)
 Time of concentration = 14.36 min.
 Rainfall intensity = 4.669(In/Hr)

```

*****
Process from Point/Station      6.000 to Point/Station      14.000
**** INITIAL AREA EVALUATION ****

```

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 83.000(Ft.)
 Highest elevation = 715.000(Ft.)
 Lowest elevation = 707.000(Ft.)
 Elevation difference = 8.000(Ft.) Slope = 9.639 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 9.64 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 4.50 minutes
 (for slope value of 10.00 %)
 Calculated TC of 4.500 minutes is less than 5 minutes,
 resetting TC to 5.0 minutes for rainfall intensity calculations
 Rainfall intensity (I) = 9.222(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.365(CFS)
 Total initial stream area = 0.066(Ac.)

```

*****
Process from Point/Station      14.000 to Point/Station      14.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.066(Ac.)
 Runoff from this stream = 0.365(CFS)
 Time of concentration = 4.50 min.
 Rainfall intensity = 9.222(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	55.169	14.36	4.669
2	0.365	4.50	9.222
Qmax(1) =			
	1.000 *	1.000 *	55.169) +
	0.506 *	1.000 *	0.365) + = 55.354
Qmax(2) =			
	1.000 *	0.313 *	55.169) +
	1.000 *	1.000 *	0.365) + = 17.650

Total of 2 streams to confluence:
 Flow rates before confluence point:
 55.169 0.365

Maximum flow rates at confluence using above data:

55.354 17.650
Area of streams before confluence:
30.901 0.066
Results of confluence:
Total flow rate = 55.354(CFS)
Time of concentration = 14.363 min.
Effective stream area after confluence = 30.967(Ac.)

Process from Point/Station 14.000 to Point/Station 19.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 691.300(Ft.)
Downstream point/station elevation = 690.700(Ft.)
Pipe length = 58.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 55.354(CFS)
Nearest computed pipe diameter = 36.00(In.)
Calculated individual pipe flow = 55.354(CFS)
Normal flow depth in pipe = 24.70(In.)
Flow top width inside pipe = 33.41(In.)
Critical Depth = 28.97(In.)
Pipe flow velocity = 10.70(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 14.45 min.

Process from Point/Station 19.000 to Point/Station 19.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 30.967(Ac.)
Runoff from this stream = 55.354(CFS)
Time of concentration = 14.45 min.
Rainfall intensity = 4.650(In/Hr)

Process from Point/Station 12.000 to Point/Station 17.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 74.000(Ft.)
Highest elevation = 713.000(Ft.)
Lowest elevation = 706.000(Ft.)
Elevation difference = 7.000(Ft.) Slope = 9.459 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 9.46 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 4.50 minutes
(for slope value of 10.00 %)
Calculated TC of 4.500 minutes is less than 5 minutes,
resetting TC to 5.0 minutes for rainfall intensity calculations
Rainfall intensity (I) = 9.222(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.315(CFS)
Total initial stream area = 0.057(Ac.)

Process from Point/Station 17.000 to Point/Station 18.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 700.000(Ft.)
Downstream point/station elevation = 695.000(Ft.)
Pipe length = 52.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.315(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.315(CFS)
Normal flow depth in pipe = 1.73(In.)
Flow top width inside pipe = 5.43(In.)
Critical Depth = 3.41(In.)
Pipe flow velocity = 6.72(Ft/s)
Travel time through pipe = 0.13 min.
Time of concentration (TC) = 4.63 min.

Process from Point/Station 18.000 to Point/Station 18.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 4.63 min.
Rainfall intensity = 9.222(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.056
Subarea runoff = 0.205(CFS) for 0.037(Ac.)
Total runoff = 0.520(CFS) Total area = 0.094(Ac.)

Process from Point/Station 18.000 to Point/Station 19.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 695.000(Ft.)
Downstream point/station elevation = 690.700(Ft.)
Pipe length = 38.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.520(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.520(CFS)
Normal flow depth in pipe = 2.16(In.)
Flow top width inside pipe = 5.76(In.)
Critical Depth = 4.41(In.)
Pipe flow velocity = 8.21(Ft/s)
Travel time through pipe = 0.08 min.
Time of concentration (TC) = 4.71 min.

Process from Point/Station 19.000 to Point/Station 19.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.094(Ac.)
Runoff from this stream = 0.520(CFS)
Time of concentration = 4.71 min.
Rainfall intensity = 9.222(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	55.354	14.45	4.650
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Total of 2 streams to confluence:
Flow rates before confluence point:
    55.354      0.520
Maximum flow rates at confluence using above data:
    55.616      18.544
Area of streams before confluence:
    30.967      0.094
Results of confluence:
Total flow rate =      55.616(CFS)
Time of concentration =      14.453 min.
Effective stream area after confluence =      31.061(Ac.)

```

```

Upstream point/station elevation = 690.700(Ft.)
Downstream point/station elevation = 690.000(Ft.)
Pipe length = 41.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 55.616(CFS)
Nearest computed pipe diameter = 33.00(In.)
Calculated individual pipe flow = 55.616(CFS)
Normal flow depth in pipe = 22.43(In.)
Flow top width inside pipe = 30.80(In.)
Critical Depth = 29.11(In.)
Pipe flow velocity = 12.94(Ft/s)
Travel time through pipe = 0.05 min.
Time of concentration (TC) = 14.51 min.

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL          ]
(10.9 DU/A or Less          )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
The area added to the existing stream causes a
a lower flow rate of Q =      51.729(CFS)
therefore the upstream flow rate of Q =      55.616(CFS) is being used
Time of concentration =      14.51 min.
Rainfall intensity =      4.639(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.358      CA =      11.150
Subarea runoff =      0.000(CFS) for      0.073(Ac.)
Total runoff =      55.616(CFS)      Total area =      31.134(Ac.)

```

Upstream point/station elevation = 690.000(Ft.)
Downstream point/station elevation = 687.000(Ft.)
Pipe length = 62.50(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 55.616(CFS)
Nearest computed pipe diameter = 27.00(In.)

Calculated individual pipe flow = 55.616(CFS)
Normal flow depth in pipe = 18.61(In.)
Flow top width inside pipe = 24.99(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.04(Ft/s)
Travel time through pipe = 0.05 min.
Time of concentration (TC) = 14.56 min.

Process from Point/Station 21.000 to Point/Station 21.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 31.134(Ac.)
Runoff from this stream = 55.616(CFS)
Time of concentration = 14.56 min.
Rainfall intensity = 4.628(In/Hr)

Process from Point/Station 18.000 to Point/Station 20.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 101.000(Ft.)
Highest elevation = 701.000(Ft.)
Lowest elevation = 693.000(Ft.)
Elevation difference = 8.000(Ft.) Slope = 7.921 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 7.92 %, in a development type of
10.9 DU/A or Less
In Accordance With Table 3-2
Initial Area Time of Concentration = 4.50 minutes
(for slope value of 10.00 %)
Calculated TC of 4.500 minutes is less than 5 minutes,
resetting TC to 5.0 minutes for rainfall intensity calculations
Rainfall intensity (I) = 9.222(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.404(CFS)
Total initial stream area = 0.073(Ac.)

Process from Point/Station 20.000 to Point/Station 21.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 688.000(Ft.)
Downstream point/station elevation = 687.000(Ft.)
Pipe length = 40.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.404(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.404(CFS)
Normal flow depth in pipe = 2.84(In.)
Flow top width inside pipe = 5.99(In.)
Critical Depth = 3.88(In.)
Pipe flow velocity = 4.41(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 4.65 min.

Process from Point/Station 21.000 to Point/Station 21.000

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 0.073(Ac.)
 Runoff from this stream = 0.404(CFS)
 Time of concentration = 4.65 min.
 Rainfall intensity = 9.222(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	55.616	14.56	4.628
2	0.404	4.65	9.222

Qmax(1) =

1.000 *	1.000 *	55.616) +	
0.502 *	1.000 *	0.404) + =	55.819

Qmax(2) =

1.000 *	0.319 *	55.616) +	
1.000 *	1.000 *	0.404) + =	18.170

Total of 2 streams to confluence:

Flow rates before confluence point:

55.616 0.404

Maximum flow rates at confluence using above data:

55.819 18.170

Area of streams before confluence:

31.134 0.073

Results of confluence:

Total flow rate = 55.819(CFS)

Time of concentration = 14.560 min.

Effective stream area after confluence = 31.207(Ac.)

 Process from Point/Station 21.000 to Point/Station 16.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 687.000(Ft.)
 Downstream point/station elevation = 686.800(Ft.)
 Pipe length = 12.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 55.819(CFS)
 Nearest computed pipe diameter = 33.00(In.)
 Calculated individual pipe flow = 55.819(CFS)
 Normal flow depth in pipe = 22.69(In.)
 Flow top width inside pipe = 30.59(In.)
 Critical Depth = 29.16(In.)
 Pipe flow velocity = 12.82(Ft/s)
 Travel time through pipe = 0.02 min.
 Time of concentration (TC) = 14.58 min.

 Process from Point/Station 16.000 to Point/Station 16.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 The area added to the existing stream causes a
 a lower flow rate of Q = 51.921(CFS)
 therefore the upstream flow rate of Q = 55.819(CFS) is being used
 Time of concentration = 14.58 min.
 Rainfall intensity = 4.625(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area

(Q=KCIA) is C = 0.359 CA = 11.227
Subarea runoff = 0.000(CFS) for 0.054(Ac.)
Total runoff = 55.819(CFS) Total area = 31.261(Ac.)

Process from Point/Station 16.000 to Point/Station 43.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.800(Ft.)
Downstream point/station elevation = 684.000(Ft.)
Pipe length = 12.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 55.819(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 55.819(CFS)
Normal flow depth in pipe = 13.31(In.)
Flow top width inside pipe = 20.23(In.)
Critical depth could not be calculated.
Pipe flow velocity = 34.73(Ft/s)
Travel time through pipe = 0.01 min.
Time of concentration (TC) = 14.58 min.

Process from Point/Station 43.000 to Point/Station 43.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 31.261(Ac.)
Runoff from this stream = 55.819(CFS)
Time of concentration = 14.58 min.
Rainfall intensity = 4.624(In/Hr)

Process from Point/Station 43.000 to Point/Station 43.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 4.036(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 18.00 min. Rain intensity = 4.04(In/Hr)
Total area = 3.835(Ac.) Total runoff = 7.240(CFS)

Process from Point/Station 43.000 to Point/Station 43.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 3.835(Ac.)
Runoff from this stream = 7.240(CFS)
Time of concentration = 18.00 min.
Rainfall intensity = 4.036(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	55.819	14.58	4.624
2	7.240	18.00	4.036

Qmax(1) = 1.000 * 1.000 * 55.819) +

```

      1.000 *      0.810 *      7.240) + =      61.684
Qmax(2) =
      0.873 *      1.000 *      55.819) +
      1.000 *      1.000 *      7.240) + =      55.969

```

```

Total of 2 streams to confluence:
Flow rates before confluence point:
      55.819      7.240
Maximum flow rates at confluence using above data:
      61.684      55.969
Area of streams before confluence:
      31.261      3.835
Results of confluence:
Total flow rate =      61.684(CFS)
Time of concentration =      14.582 min.
Effective stream area after confluence =      35.096(Ac.)

```

```

*****
Process from Point/Station      43.000 to Point/Station      22.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      684.600(Ft.)
Downstream point/station elevation =      680.500(Ft.)
Pipe length =      81.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      61.684(CFS)
Nearest computed pipe diameter =      27.00(In.)
Calculated individual pipe flow =      61.684(CFS)
Normal flow depth in pipe =      19.76(In.)
Flow top width inside pipe =      23.92(In.)
Critical depth could not be calculated.
Pipe flow velocity =      19.79(Ft/s)
Travel time through pipe =      0.07 min.
Time of concentration (TC) =      14.65 min.

```

```

*****
Process from Point/Station      22.000 to Point/Station      22.000
**** SUBAREA FLOW ADDITION ****

```

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL      ]
(10.9 DU/A or Less      )
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration =      14.65 min.
Rainfall intensity =      4.610(In/Hr) for a      100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.386  CA =      13.572
Subarea runoff =      0.879(CFS) for      0.074(Ac.)
Total runoff =      62.563(CFS)      Total area =      35.170(Ac.)

```

```

*****
Process from Point/Station      22.000 to Point/Station      24.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

```

Upstream point/station elevation =      680.500(Ft.)
Downstream point/station elevation =      674.300(Ft.)
Pipe length =      80.00(Ft.)  Manning's N = 0.013
No. of pipes = 1  Required pipe flow =      62.563(CFS)
Nearest computed pipe diameter =      24.00(In.)
Calculated individual pipe flow =      62.563(CFS)
Normal flow depth in pipe =      19.55(In.)
Flow top width inside pipe =      18.66(In.)
Critical depth could not be calculated.
Pipe flow velocity =      22.85(Ft/s)
Travel time through pipe =      0.06 min.

```

Time of concentration (TC) = 14.71 min.

Process from Point/Station 24.000 to Point/Station 24.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 35.170(Ac.)
Runoff from this stream = 62.563(CFS)
Time of concentration = 14.71 min.
Rainfall intensity = 4.598(In/Hr)

Process from Point/Station 20.000 to Point/Station 23.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 191.000(Ft.)
Highest elevation = 693.000(Ft.)
Lowest elevation = 680.000(Ft.)
Elevation difference = 13.000(Ft.) Slope = 6.806 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 6.81 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.75 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (100.000^{.5})] / (6.806^{(1/3)}) = 4.75$
Rainfall intensity (I) = 9.533(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.949(CFS)
Total initial stream area = 0.166(Ac.)

Process from Point/Station 23.000 to Point/Station 24.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 675.500(Ft.)
Downstream point/station elevation = 674.300(Ft.)
Pipe length = 33.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.949(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.949(CFS)
Normal flow depth in pipe = 4.39(In.)
Flow top width inside pipe = 5.31(In.)
Critical Depth = 5.60(In.)
Pipe flow velocity = 6.15(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 4.84 min.

Process from Point/Station 24.000 to Point/Station 24.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.166(Ac.)
Runoff from this stream = 0.949(CFS)
Time of concentration = 4.84 min.
Rainfall intensity = 9.419(In/Hr)

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	62.563	14.71	4.598
2	0.949	4.84	9.419

Qmax(1) =

1.000 *	1.000 *	62.563) +	
0.488 *	1.000 *	0.949) + =	63.027

Qmax(2) =

1.000 *	0.329 *	62.563) +	
1.000 *	1.000 *	0.949) + =	21.530

Total of 2 streams to confluence:

Flow rates before confluence point:

62.563	0.949
--------	-------

Maximum flow rates at confluence using above data:

63.027	21.530
--------	--------

Area of streams before confluence:

35.170	0.166
--------	-------

Results of confluence:

Total flow rate = 63.027(CFS)

Time of concentration = 14.708 min.

Effective stream area after confluence = 35.336(Ac.)

Process from Point/Station 24.000 to Point/Station 25.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 674.300(Ft.)
Downstream point/station elevation = 673.500(Ft.)
Pipe length = 50.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 63.027(CFS)
Nearest computed pipe diameter = 33.00(In.)
Calculated individual pipe flow = 63.027(CFS)
Normal flow depth in pipe = 25.50(In.)
Flow top width inside pipe = 27.66(In.)
Critical Depth = 30.29(In.)
Pipe flow velocity = 12.81(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 14.77 min.

Process from Point/Station 25.000 to Point/Station 25.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 35.336(Ac.)
Runoff from this stream = 63.027(CFS)
Time of concentration = 14.77 min.
Rainfall intensity = 4.585(In/Hr)

Process from Point/Station 25.200 to Point/Station 25.100
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 237.000(Ft.)
Highest elevation = 732.000(Ft.)

Lowest elevation = 710.500(Ft.)
 Elevation difference = 21.500(Ft.) Slope = 9.072 %
 Top of Initial Area Slope adjusted by User to 11.400 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 11.40 %, in a development type of
 Permanent Open Space
 In Accordance With Table 3-2
 Initial Area Time of Concentration = 6.90 minutes
 (for slope value of 10.00 %)
 Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
 Subarea runoff = 6.975(CFS)
 Total initial stream area = 2.660(Ac.)

++++++
 Process from Point/Station 25.100 to Point/Station 25.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 705.000(Ft.)
 Downstream point/station elevation = 673.500(Ft.)
 Pipe length = 193.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 6.975(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 6.975(CFS)
 Normal flow depth in pipe = 5.89(In.)
 Flow top width inside pipe = 12.00(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 18.18(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 7.08 min.

++++++
 Process from Point/Station 25.000 to Point/Station 25.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 2.660(Ac.)
 Runoff from this stream = 6.975(CFS)
 Time of concentration = 7.08 min.
 Rainfall intensity = 7.370(In/Hr)

++++++
 Process from Point/Station 22.000 to Point/Station 25.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 130.000(Ft.)
 Highest elevation = 685.000(Ft.)
 Lowest elevation = 678.000(Ft.)
 Elevation difference = 7.000(Ft.) Slope = 5.385 %
 Top of Initial Area Slope adjusted by User to 5.750 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 5.75 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.02 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5} / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (100.000^{.5}) / (5.750^{(1/3)})] = 5.02$
 Rainfall intensity (I) = 9.194(In/Hr) for a 100.0 year storm

Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 0.530(CFS)
Total initial stream area = 0.096(Ac.)

Process from Point/Station 25.000 to Point/Station 25.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.096(Ac.)
Runoff from this stream = 0.530(CFS)
Time of concentration = 5.02 min.
Rainfall intensity = 9.194(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	63.027	14.77	4.585
2	6.975	7.08	7.370
3	0.530	5.02	9.194

Qmax(1) =
1.000 * 1.000 * 63.027) +
0.622 * 1.000 * 6.975) +
0.499 * 1.000 * 0.530) + = 67.630

Qmax(2) =
1.000 * 0.479 * 63.027) +
1.000 * 1.000 * 6.975) +
0.802 * 1.000 * 0.530) + = 37.591

Qmax(3) =
1.000 * 0.340 * 63.027) +
1.000 * 0.710 * 6.975) +
1.000 * 1.000 * 0.530) + = 26.913

Total of 3 streams to confluence:
Flow rates before confluence point:
63.027 6.975 0.530
Maximum flow rates at confluence using above data:
67.630 37.591 26.913
Area of streams before confluence:
35.336 2.660 0.096
Results of confluence:
Total flow rate = 67.630(CFS)
Time of concentration = 14.773 min.
Effective stream area after confluence = 38.092(Ac.)

Process from Point/Station 25.000 to Point/Station 26.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 673.500(Ft.)
Downstream point/station elevation = 669.000(Ft.)
Pipe length = 111.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 67.630(CFS)
Nearest computed pipe diameter = 30.00(In.)
Calculated individual pipe flow = 67.630(CFS)
Normal flow depth in pipe = 20.65(In.)
Flow top width inside pipe = 27.79(In.)
Critical depth could not be calculated.
Pipe flow velocity = 18.77(Ft/s)
Travel time through pipe = 0.10 min.
Time of concentration (TC) = 14.87 min.

Process from Point/Station 26.000 to Point/Station 26.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 The area added to the existing stream causes a
 a lower flow rate of Q = 67.198(CFS)
 therefore the upstream flow rate of Q = 67.630(CFS) is being used
 Time of concentration = 14.87 min.
 Rainfall intensity = 4.565(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.385 CA = 14.720
 Subarea runoff = 0.000(CFS) for 0.099(Ac.)
 Total runoff = 67.630(CFS) Total area = 38.191(Ac.)

 Process from Point/Station 26.000 to Point/Station 26.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 38.191(Ac.)
 Runoff from this stream = 67.630(CFS)
 Time of concentration = 14.87 min.
 Rainfall intensity = 4.565(In/Hr)

 Process from Point/Station 25.000 to Point/Station 26.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 110.000(Ft.)
 Highest elevation = 678.000(Ft.)
 Lowest elevation = 673.500(Ft.)
 Elevation difference = 4.500(Ft.) Slope = 4.091 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 4.09 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.63 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5} / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (100.000^{.5}) / (4.091^{(1/3)})] = 5.63$
 Rainfall intensity (I) = 8.545(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.508(CFS)
 Total initial stream area = 0.099(Ac.)

 Process from Point/Station 26.000 to Point/Station 26.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.099(Ac.)
 Runoff from this stream = 0.508(CFS)
 Time of concentration = 5.63 min.
 Rainfall intensity = 8.545(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	67.630	14.87	4.565
2	0.508	5.63	8.545

Qmax(1) =

1.000 *	1.000 *	67.630) +	
0.534 *	1.000 *	0.508) + =	67.901

Qmax(2) =

1.000 *	0.378 *	67.630) +	
1.000 *	1.000 *	0.508) + =	26.097

Total of 2 streams to confluence:
Flow rates before confluence point:
67.630 0.508
Maximum flow rates at confluence using above data:
67.901 26.097
Area of streams before confluence:
38.191 0.099
Results of confluence:
Total flow rate = 67.901(CFS)
Time of concentration = 14.872 min.
Effective stream area after confluence = 38.290(Ac.)

Process from Point/Station 26.000 to Point/Station 63.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 669.000(Ft.)
Downstream point/station elevation = 662.000(Ft.)
Pipe length = 148.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 67.901(CFS)
Nearest computed pipe diameter = 30.00(In.)
Calculated individual pipe flow = 67.901(CFS)
Normal flow depth in pipe = 19.59(In.)
Flow top width inside pipe = 28.56(In.)
Critical depth could not be calculated.
Pipe flow velocity = 20.00(Ft/s)
Travel time through pipe = 0.12 min.
Time of concentration (TC) = 15.00 min.

Process from Point/Station 63.000 to Point/Station 63.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 38.290(Ac.)
Runoff from this stream = 67.901(CFS)
Time of concentration = 15.00 min.
Rainfall intensity = 4.541(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 23.000 to Point/Station 27.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 111.000(Ft.)
Highest elevation = 680.000(Ft.)

Lowest elevation = 675.000(Ft.)
 Elevation difference = 5.000(Ft.) Slope = 4.505 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 4.50 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 5.45 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (100.000^{.5})] / (4.505^{(1/3)}) = 5.45$
 Rainfall intensity (I) = 8.724(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.445(CFS)
 Total initial stream area = 0.085(Ac.)

 Process from Point/Station 27.000 to Point/Station 28.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 670.000(Ft.)
 Downstream point/station elevation = 664.000(Ft.)
 Pipe length = 76.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.445(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.445(CFS)
 Normal flow depth in pipe = 2.18(In.)
 Flow top width inside pipe = 5.77(In.)
 Critical Depth = 4.08(In.)
 Pipe flow velocity = 6.90(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 5.63 min.

 Process from Point/Station 28.000 to Point/Station 28.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Time of concentration = 5.63 min.
 Rainfall intensity = 8.539(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.600 CA = 0.085
 Subarea runoff = 0.278(CFS) for 0.056(Ac.)
 Total runoff = 0.722(CFS) Total area = 0.141(Ac.)

 Process from Point/Station 28.000 to Point/Station 29.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 664.000(Ft.)
 Downstream point/station elevation = 663.000(Ft.)
 Pipe length = 66.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.722(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 0.722(CFS)
 Normal flow depth in pipe = 3.70(In.)
 Flow top width inside pipe = 8.86(In.)
 Critical Depth = 4.65(In.)
 Pipe flow velocity = 4.22(Ft/s)
 Travel time through pipe = 0.26 min.
 Time of concentration (TC) = 5.89 min.

Process from Point/Station 29.000 to Point/Station 29.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Time of concentration = 5.89 min.
Rainfall intensity = 8.293(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.600 CA = 0.122
Subarea runoff = 0.288(CFS) for 0.062(Ac.)
Total runoff = 1.010(CFS) Total area = 0.203(Ac.)

Process from Point/Station 29.000 to Point/Station 29.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 663.000(Ft.)
Downstream point/station elevation = 662.500(Ft.)
Pipe length = 32.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.010(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.010(CFS)
Normal flow depth in pipe = 4.44(In.)
Flow top width inside pipe = 9.00(In.)
Critical Depth = 5.53(In.)
Pipe flow velocity = 4.65(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 6.01 min.

Process from Point/Station 29.100 to Point/Station 29.100
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 0.203(Ac.)
Runoff from this stream = 1.010(CFS)
Time of concentration = 6.01 min.
Rainfall intensity = 8.191(In/Hr)

Process from Point/Station 62.000 to Point/Station 62.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 9.00 min. Rain intensity = 6.31(In/Hr)
Total area = 51.810(Ac.) Total runoff = 132.660(CFS)

Process from Point/Station 62.000 to Point/Station 29.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 663.000(Ft.)
Downstream point/station elevation = 662.500(Ft.)
Pipe length = 34.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 132.660(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 132.660(CFS)
Normal flow depth in pipe = 33.52(In.)
Flow top width inside pipe = 39.24(In.)
Critical Depth = 40.96(In.)
Pipe flow velocity = 15.04(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 9.04 min.

Process from Point/Station 29.100 to Point/Station 29.100
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
Stream flow area = 51.810(Ac.)
Runoff from this stream = 132.660(CFS)
Time of concentration = 9.04 min.
Rainfall intensity = 6.295(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1.010	6.01	8.191
2	132.660	9.04	6.295

Qmax(1) =
1.000 * 1.000 * 1.010) +
1.000 * 0.665 * 132.660) + = 89.205
Qmax(2) =
0.768 * 1.000 * 1.010) +
1.000 * 1.000 * 132.660) + = 133.436

Total of 2 streams to confluence:
Flow rates before confluence point:
1.010 132.660
Maximum flow rates at confluence using above data:
89.205 133.436
Area of streams before confluence:
0.203 51.810
Results of confluence:
Total flow rate = 133.436(CFS)
Time of concentration = 9.038 min.
Effective stream area after confluence = 52.013(Ac.)

Process from Point/Station 29.100 to Point/Station 63.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 662.500(Ft.)
Downstream point/station elevation = 662.000(Ft.)
Pipe length = 36.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 133.436(CFS)
Nearest computed pipe diameter = 45.00(In.)
Calculated individual pipe flow = 133.436(CFS)
Normal flow depth in pipe = 34.55(In.)
Flow top width inside pipe = 38.01(In.)
Critical Depth = 41.03(In.)
Pipe flow velocity = 14.67(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 9.08 min.

Process from Point/Station 63.000 to Point/Station 63.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 52.013(Ac.)
Runoff from this stream = 133.436(CFS)
Time of concentration = 9.08 min.
Rainfall intensity = 6.277(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	67.901	15.00	4.541
2	133.436	9.08	6.277

Qmax(1) =
1.000 * 1.000 * 67.901) +
0.723 * 1.000 * 133.436) + = 164.440
Qmax(2) =
1.000 * 0.605 * 67.901) +
1.000 * 1.000 * 133.436) + = 174.545

Total of 2 main streams to confluence:

Flow rates before confluence point:

67.901 133.436

Maximum flow rates at confluence using above data:

164.440 174.545

Area of streams before confluence:

38.290 52.013

Results of confluence:

Total flow rate = 174.545(CFS)

Time of concentration = 9.079 min.

Effective stream area after confluence = 90.303(Ac.)

Process from Point/Station 63.000 to Point/Station 66.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 662.000(Ft.)
Downstream point/station elevation = 661.000(Ft.)
Pipe length = 114.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 174.545(CFS)
Nearest computed pipe diameter = 54.00(In.)
Calculated individual pipe flow = 174.545(CFS)
Normal flow depth in pipe = 41.91(In.)
Flow top width inside pipe = 45.02(In.)
Critical Depth = 46.03(In.)
Pipe flow velocity = 13.18(Ft/s)
Travel time through pipe = 0.14 min.
Time of concentration (TC) = 9.22 min.

Process from Point/Station 66.000 to Point/Station 66.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 90.303(Ac.)
Runoff from this stream = 174.545(CFS)
Time of concentration = 9.22 min.
Rainfall intensity = 6.213(In/Hr)

Process from Point/Station 26.000 to Point/Station 65.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 262.000(Ft.)
 Highest elevation = 673.500(Ft.)
 Lowest elevation = 669.000(Ft.)
 Elevation difference = 4.500(Ft.) Slope = 1.718 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 80.00 (Ft)
 for the top area slope value of 1.72 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.72 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5} / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (80.000^{.5}) / (1.718^{(1/3)})] = 6.72$
 Rainfall intensity (I) = 7.620(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.960(CFS)
 Total initial stream area = 0.210(Ac.)

 Process from Point/Station 65.000 to Point/Station 65.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.210(Ac.)
 Runoff from this stream = 0.960(CFS)
 Time of concentration = 6.72 min.
 Rainfall intensity = 7.620(In/Hr)

 Process from Point/Station 29.000 to Point/Station 64.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Initial subarea total flow distance = 163.000(Ft.)
 Highest elevation = 670.500(Ft.)
 Lowest elevation = 668.500(Ft.)
 Elevation difference = 2.000(Ft.) Slope = 1.227 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 65.00 (Ft)
 for the top area slope value of 1.23 %, in a development type of
 10.9 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 6.78 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5} / (% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (65.000^{.5}) / (1.227^{(1/3)})] = 6.78$
 Rainfall intensity (I) = 7.579(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
 Subarea runoff = 0.950(CFS)
 Total initial stream area = 0.209(Ac.)

 Process from Point/Station 64.000 to Point/Station 66.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 664.000(Ft.)
Downstream point/station elevation = 661.000(Ft.)
Pipe length = 37.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.950(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.950(CFS)
Normal flow depth in pipe = 3.33(In.)
Flow top width inside pipe = 5.96(In.)
Critical Depth = 5.61(In.)
Pipe flow velocity = 8.49(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 6.85 min.

Process from Point/Station 66.000 to Point/Station 66.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.209(Ac.)
Runoff from this stream = 0.950(CFS)
Time of concentration = 6.85 min.
Rainfall intensity = 7.527(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	174.545	9.22	6.213
2	0.960	6.72	7.620
3	0.950	6.85	7.527

Qmax(1) =
1.000 * 1.000 * 174.545) +
0.815 * 1.000 * 0.960) +
0.825 * 1.000 * 0.950) + = 176.113

Qmax(2) =
1.000 * 0.729 * 174.545) +
1.000 * 1.000 * 0.960) +
1.000 * 0.981 * 0.950) + = 129.094

Qmax(3) =
1.000 * 0.743 * 174.545) +
0.988 * 1.000 * 0.960) +
1.000 * 1.000 * 0.950) + = 131.545

Total of 3 streams to confluence:
Flow rates before confluence point:
174.545 0.960 0.950
Maximum flow rates at confluence using above data:
176.113 129.094 131.545
Area of streams before confluence:
90.303 0.210 0.209
Results of confluence:
Total flow rate = 176.113(CFS)
Time of concentration = 9.223 min.
Effective stream area after confluence = 90.722(Ac.)

Process from Point/Station 66.000 to Point/Station 81.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.000(Ft.)
Downstream point/station elevation = 659.680(Ft.)
Pipe length = 132.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 176.113(CFS)
Nearest computed pipe diameter = 54.00(In.)
Calculated individual pipe flow = 176.113(CFS)
Normal flow depth in pipe = 39.89(In.)
Flow top width inside pipe = 47.45(In.)

Critical Depth = 46.20(In.)
Pipe flow velocity = 13.98(Ft/s)
Travel time through pipe = 0.16 min.
Time of concentration (TC) = 9.38 min.

Process from Point/Station 81.000 to Point/Station 81.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 90.722(Ac.)
Runoff from this stream = 176.113(CFS)
Time of concentration = 9.38 min.
Rainfall intensity = 6.146(In/Hr)

Process from Point/Station 516.000 to Point/Station 524.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 180.000(Ft.)
Highest elevation = 671.500(Ft.)
Lowest elevation = 666.000(Ft.)
Elevation difference = 5.500(Ft.) Slope = 3.056 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.06 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.88 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.056^{(1/3)}) = 5.88$
Rainfall intensity (I) = 8.303(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 1.126(CFS)
Total initial stream area = 0.226(Ac.)

Process from Point/Station 524.000 to Point/Station 81.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.500(Ft.)
Downstream point/station elevation = 659.680(Ft.)
Pipe length = 18.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.126(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 1.126(CFS)
Normal flow depth in pipe = 3.46(In.)
Flow top width inside pipe = 5.93(In.)
Critical depth could not be calculated.
Pipe flow velocity = 9.61(Ft/s)
Travel time through pipe = 0.03 min.
Time of concentration (TC) = 5.91 min.

Process from Point/Station 81.000 to Point/Station 81.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 0.226(Ac.)

Runoff from this stream = 1.126(CFS)
Time of concentration = 5.91 min.
Rainfall intensity = 8.274(In/Hr)

Process from Point/Station 521.000 to Point/Station 538.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Initial subarea total flow distance = 179.000(Ft.)
Highest elevation = 671.500(Ft.)
Lowest elevation = 665.700(Ft.)
Elevation difference = 5.800(Ft.) Slope = 3.240 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 3.24 %, in a development type of
10.9 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 5.77 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.6000) * (90.000^{.5})] / (3.240^{(1/3)}) = 5.77$
Rainfall intensity (I) = 8.408(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.600
Subarea runoff = 1.019(CFS)
Total initial stream area = 0.202(Ac.)

Process from Point/Station 538.000 to Point/Station 81.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.000(Ft.)
Downstream point/station elevation = 659.680(Ft.)
Pipe length = 50.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.019(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 1.019(CFS)
Normal flow depth in pipe = 3.84(In.)
Flow top width inside pipe = 8.90(In.)
Critical Depth = 5.56(In.)
Pipe flow velocity = 5.66(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 5.92 min.

Process from Point/Station 81.000 to Point/Station 81.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.202(Ac.)
Runoff from this stream = 1.019(CFS)
Time of concentration = 5.92 min.
Rainfall intensity = 8.272(In/Hr)

Process from Point/Station 94.000 to Point/Station 94.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 3.353(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 24.00 min. Rain intensity = 3.35(In/Hr)
Total area = 12.670(Ac.) Total runoff = 13.320(CFS)

Process from Point/Station 94.000 to Point/Station 81.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 686.500(Ft.)
Downstream point/station elevation = 655.770(Ft.)
Pipe length = 73.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 13.320(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 13.320(CFS)
Normal flow depth in pipe = 6.53(In.)
Flow top width inside pipe = 11.95(In.)
Critical depth could not be calculated.
Pipe flow velocity = 30.47(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 24.04 min.

Process from Point/Station 81.000 to Point/Station 81.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4
Stream flow area = 12.670(Ac.)
Runoff from this stream = 13.320(CFS)
Time of concentration = 24.04 min.
Rainfall intensity = 3.349(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	176.113	9.38	6.146
2	1.126	5.91	8.274
3	1.019	5.92	8.272
4	13.320	24.04	3.349

Qmax(1) =

1.000 *	1.000 *	176.113) +	
0.743 *	1.000 *	1.126) +	
0.743 *	1.000 *	1.019) +	
1.000 *	0.390 *	13.320) + =	182.903

Qmax(2) =

1.000 *	0.631 *	176.113) +	
1.000 *	1.000 *	1.126) +	
1.000 *	1.000 *	1.019) +	
1.000 *	0.246 *	13.320) + =	116.474

Qmax(3) =

1.000 *	0.631 *	176.113) +	
1.000 *	1.000 *	1.126) +	
1.000 *	1.000 *	1.019) +	
1.000 *	0.246 *	13.320) + =	116.519

Qmax(4) =

0.545 *	1.000 *	176.113) +	
0.405 *	1.000 *	1.126) +	
0.405 *	1.000 *	1.019) +	
1.000 *	1.000 *	13.320) + =	110.164

Total of 4 streams to confluence:
Flow rates before confluence point:

176.113	1.126	1.019	13.320
Maximum flow rates at confluence using above data:			
182.903	116.474	116.519	110.164
Area of streams before confluence:			
90.722	0.226	0.202	12.670
Results of confluence:			
Total flow rate = 182.903(CFS)			
Time of concentration = 9.380 min.			
Effective stream area after confluence = 103.820(Ac.)			

Process from Point/Station 81.000 to Point/Station 82.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 655.770(Ft.)
Downstream point/station elevation = 637.000(Ft.)
Pipe length = 172.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 182.903(CFS)
Nearest computed pipe diameter = 36.00(In.)
Calculated individual pipe flow = 182.903(CFS)
Normal flow depth in pipe = 25.03(In.)
Flow top width inside pipe = 33.14(In.)
Critical depth could not be calculated.
Pipe flow velocity = 34.85(Ft/s)
Travel time through pipe = 0.08 min.
Time of concentration (TC) = 9.46 min.
End of computations, total study area = 103.820 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/18/13

FINAL OUTFALL 10 - Las Posas Road: Node 1 TO 6
POST DEVELOPMENT AFTER DETENTION
100 Year Storm Event
File Name: D12052POSTOVERALL.RD3

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 100.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 3.500
24 hour precipitation(inches) = 6.000
P6/P24 = 58.3%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL]
(1.0 DU/A or Less)
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Initial subarea total flow distance = 1012.000(Ft.)
Highest elevation = 1140.000(Ft.)
Lowest elevation = 900.000(Ft.)
Elevation difference = 240.000(Ft.) Slope = 23.715 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 23.72 %, in a development type of
1.0 DU/A or Less
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.32 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.4100) * (100.000^{.5})] / (23.715^{(1/3)}) = 4.32$
The initial area total distance of 1012.00 (Ft.) entered leaves a
remaining distance of 912.00 (Ft.)
Using Figure 3-4, the travel time for this distance is 2.58 minutes
for a distance of 912.00 (Ft.) and a slope of 23.72 %
with an elevation difference of 216.28(Ft.) from the end of the top area
 $Tt = [11.9 * length(Mi)^3] / (elevation change(Ft.))^{.385} * 60(min/hr)$
 $= 2.585 Minutes$
 $Tt = [(11.9 * 0.1727^3) / (216.28)]^{.385} = 2.58$
Total initial area Ti = 4.32 minutes from Figure 3-3 formula plus
2.58 minutes from the Figure 3-4 formula = 6.91 minutes
Rainfall intensity (I) = 7.486(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.410
Subarea runoff = 45.998(CFS)
Total initial stream area = 14.986(Ac.)

```

*****
Process from Point/Station      2.000 to Point/Station      3.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

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```

-----
Estimated mean flow rate at midpoint of channel =    148.425(CFS)
Depth of flow =    1.083(Ft.), Average velocity =    12.664(Ft/s)
***** Irregular Channel Data *****

```

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              10.00
      2             100.00              0.00
      3             200.00              10.00
Manning's 'N' friction factor =    0.020

```

```

-----
Sub-Channel flow =    148.425(CFS)
'      '      flow top width =    21.652(Ft.)
'      '      velocity=    12.664(Ft/s)
'      '      area =    11.720(Sq.Ft)
'      '      Froude number =    3.033

```

```

Upstream point elevation =    900.000(Ft.)
Downstream point elevation =    721.000(Ft.)
Flow length =    2700.000(Ft.)
Travel time =    3.55 min.
Time of concentration =    10.46 min.
Depth of flow =    1.083(Ft.)
Average velocity =    12.664(Ft/s)
Total irregular channel flow =    148.425(CFS)
Irregular channel normal depth above invert elev. =    1.083(Ft.)
Average velocity of channel(s) =    12.664(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL                      ]
(1.0 DU/A or Less                          )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Rainfall intensity =    5.728(In/Hr) for a    100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.410  CA =    43.782
Subarea runoff =    204.795(CFS) for    91.800(Ac.)
Total runoff =    250.793(CFS)      Total area =    106.786(Ac.)
Depth of flow =    1.318(Ft.), Average velocity =    14.439(Ft/s)

```

```

*****
Process from Point/Station      3.000 to Point/Station      4.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

-----
Estimated mean flow rate at midpoint of channel =    307.673(CFS)
Depth of flow =    1.722(Ft.), Average velocity =    10.375(Ft/s)
***** Irregular Channel Data *****

```

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              5.00
      2             100.00              0.00
      3             100.00              5.00
Manning's 'N' friction factor =    0.023

```

```

-----
Sub-Channel flow =    307.673(CFS)
'      '      flow top width =    34.441(Ft.)
'      '      velocity=    10.375(Ft/s)
'      '      area =    29.655(Sq.Ft)
'      '      Froude number =    1.970

```

```

Upstream point elevation =    721.000(Ft.)
Downstream point elevation =    668.000(Ft.)
Flow length =    1575.000(Ft.)
Travel time =    2.53 min.

```

Time of concentration = 12.99 min.
 Depth of flow = 1.722(Ft.)
 Average velocity = 10.375(Ft/s)
 Total irregular channel flow = 307.673(CFS)
 Irregular channel normal depth above invert elev. = 1.722(Ft.)
 Average velocity of channel(s) = 10.375(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [LOW DENSITY RESIDENTIAL]
 (1.0 DU/A or Less)
 Impervious value, Ai = 0.100
 Sub-Area C Value = 0.410
 Rainfall intensity = 4.981(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.410 CA = 73.172
 Subarea runoff = 113.696(CFS) for 71.682(Ac.)
 Total runoff = 364.490(CFS) Total area = 178.468(Ac.)
 Depth of flow = 1.835(Ft.), Average velocity = 10.824(Ft/s)

++++++
 Process from Point/Station 4.000 to Point/Station 4.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 178.468(Ac.)
 Runoff from this stream = 364.490(CFS)
 Time of concentration = 12.99 min.
 Rainfall intensity = 4.981(In/Hr)

++++++
 Process from Point/Station 9.000 to Point/Station 10.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [LOW DENSITY RESIDENTIAL]
 (1.0 DU/A or Less)
 Impervious value, Ai = 0.100
 Sub-Area C Value = 0.410
 Initial subarea total flow distance = 1909.000(Ft.)
 Highest elevation = 1302.000(Ft.)
 Lowest elevation = 820.000(Ft.)
 Elevation difference = 482.000(Ft.) Slope = 25.249 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 100.00 (Ft)
 for the top area slope value of 25.25 %, in a development type of
 1.0 DU/A or Less
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 4.23 minutes
 $TC = [1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})]$
 $TC = [1.8 * (1.1 - 0.4100) * (100.000^{.5})] / (25.249^{(1/3)}) = 4.23$
 The initial area total distance of 1909.00 (Ft.) entered leaves a
 remaining distance of 1809.00 (Ft.)
 Using Figure 3-4, the travel time for this distance is 4.28 minutes
 for a distance of 1809.00 (Ft.) and a slope of 25.25 %
 with an elevation difference of 456.75(Ft.) from the end of the top area
 $Tt = [11.9 * \text{length}(\text{Mi})^3] / (\text{elevation change}(\text{Ft.}))^{.385} * 60(\text{min/hr})$
 $= 4.275 \text{ Minutes}$
 $Tt = [(11.9 * 0.3426^3) / (456.75)]^{.385} = 4.28$
 Total initial area Ti = 4.23 minutes from Figure 3-3 formula plus
 4.28 minutes from the Figure 3-4 formula = 8.51 minutes
 Rainfall intensity (I) = 6.544(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.410
 Subarea runoff = 60.081(CFS)
 Total initial stream area = 22.391(Ac.)

```

*****
Process from Point/Station      10.000 to Point/Station      4.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

-----
Estimated mean flow rate at midpoint of channel =    194.618(CFS)
Depth of flow =    0.918(Ft.), Average velocity =    11.540(Ft/s)
***** Irregular Channel Data *****

```

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              5.00
      2             100.00              0.00
      3             200.00              5.00
Manning's 'N' friction factor =    0.020

```

```

-----
Sub-Channel flow =    194.618(CFS)
'      '      flow top width =    36.731(Ft.)
'      '      velocity=    11.540(Ft/s)
'      '      area =    16.864(Sq.Ft)
'      '      Froude number =    3.001

```

```

Upstream point elevation =    820.000(Ft.)
Downstream point elevation =    668.000(Ft.)
Flow length =    2228.000(Ft.)
Travel time =    3.22 min.
Time of concentration =    11.73 min.
Depth of flow =    0.918(Ft.)
Average velocity =    11.540(Ft/s)
Total irregular channel flow =    194.618(CFS)
Irregular channel normal depth above invert elev. =    0.918(Ft.)
Average velocity of channel(s) =    11.540(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL                      ]
(1.0 DU/A or Less                      )
Impervious value, Ai = 0.100
Sub-Area C Value = 0.410
Rainfall intensity =    5.321(In/Hr) for a    100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.410  CA =    61.845
Subarea runoff =    269.022(CFS) for    128.450(Ac.)
Total runoff =    329.102(CFS)          Total area =    150.841(Ac.)
Depth of flow =    1.118(Ft.), Average velocity =    13.160(Ft/s)

```

```

*****
Process from Point/Station      4.000 to Point/Station      4.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

-----
Along Main Stream number: 1 in normal stream number 2
Stream flow area =    150.841(Ac.)
Runoff from this stream =    329.102(CFS)
Time of concentration =    11.73 min.
Rainfall intensity =    5.321(In/Hr)
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	364.490	12.99	4.981
2	329.102	11.73	5.321
Qmax(1) =			
	1.000 *	1.000 *	364.490) +
	0.936 *	1.000 *	329.102) + =
			672.557
Qmax(2) =			
	1.000 *	0.903 *	364.490) +
	1.000 *	1.000 *	329.102) + =
			658.114

Total of 2 streams to confluence:
Flow rates before confluence point:
364.490 329.102
Maximum flow rates at confluence using above data:
672.557 658.114
Area of streams before confluence:
178.468 150.841
Results of confluence:
Total flow rate = 672.557(CFS)
Time of concentration = 12.991 min.
Effective stream area after confluence = 329.309(Ac.)

Process from Point/Station 4.000 to Point/Station 4.200
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 3.950(Ft.), Average velocity = 6.898(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 16.00
2 100.00 0.00
3 200.00 16.00
Manning's 'N' friction factor = 0.045

Sub-Channel flow = 672.556(CFS)
' ' flow top width = 49.371(Ft.)
' ' velocity = 6.898(Ft/s)
' ' area = 97.500(Sq.Ft)
' ' Froude number = 0.865

Upstream point elevation = 668.000(Ft.)
Downstream point elevation = 656.000(Ft.)
Flow length = 670.000(Ft.)
Travel time = 1.62 min.
Time of concentration = 14.61 min.
Depth of flow = 3.950(Ft.)
Average velocity = 6.898(Ft/s)
Total irregular channel flow = 672.557(CFS)
Irregular channel normal depth above invert elev. = 3.950(Ft.)
Average velocity of channel(s) = 6.898(Ft/s)

Process from Point/Station 4.200 to Point/Station 4.200
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 329.309(Ac.)
Runoff from this stream = 672.557(CFS)
Time of concentration = 14.61 min.
Rainfall intensity = 4.618(In/Hr)

Process from Point/Station 4.100 to Point/Station 4.200
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 887.000(Ft.)
Highest elevation = 835.000(Ft.)
Lowest elevation = 656.000(Ft.)
Elevation difference = 179.000(Ft.) Slope = 20.180 %
Top of Initial Area Slope adjusted by User to 30.000 %

INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 30.00 %, in a development type of
Permanent Open Space
In Accordance With Table 3-2
Initial Area Time of Concentration = 6.90 minutes
(for slope value of 10.00 %)
Rainfall intensity (I) = 7.492(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 48.850(CFS)
Total initial stream area = 18.630(Ac.)

Process from Point/Station 4.200 to Point/Station 4.200
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 18.630(Ac.)
Runoff from this stream = 48.850(CFS)
Time of concentration = 6.90 min.
Rainfall intensity = 7.492(In/Hr)

Process from Point/Station 511.000 to Point/Station 4.200
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 9.00 min. Rain intensity = 6.31(In/Hr)
Total area = 0.944(Ac.) Total runoff = 3.650(CFS)

Process from Point/Station 4.200 to Point/Station 4.200
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.944(Ac.)
Runoff from this stream = 3.650(CFS)
Time of concentration = 9.00 min.
Rainfall intensity = 6.312(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	672.557	14.61	4.618
2	48.850	6.90	7.492
3	3.650	9.00	6.312
Qmax(1) =			
	1.000 *	1.000 *	672.557) +
	0.616 *	1.000 *	48.850) +
	0.732 *	1.000 *	3.650) + = 705.338
Qmax(2) =			
	1.000 *	0.472 *	672.557) +
	1.000 *	1.000 *	48.850) +
	1.000 *	0.767 *	3.650) + = 369.286
Qmax(3) =			
	1.000 *	0.616 *	672.557) +
	0.843 *	1.000 *	48.850) +
	1.000 *	1.000 *	3.650) + = 459.117

Total of 3 streams to confluence:
Flow rates before confluence point:
672.557 48.850 3.650
Maximum flow rates at confluence using above data:
705.338 369.286 459.117
Area of streams before confluence:
329.309 18.630 0.944
Results of confluence:
Total flow rate = 705.338(CFS)
Time of concentration = 14.610 min.
Effective stream area after confluence = 348.883(Ac.)

Process from Point/Station 4.200 to Point/Station 4.300
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 4.839(Ft.), Average velocity = 4.819(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 16.00
2 100.00 0.00
3 200.00 16.00
Manning's 'N' friction factor = 0.045

Sub-Channel flow = 705.338(CFS)
' flow top width = 60.492(Ft.)
' velocity= 4.819(Ft/s)
' area = 146.372(Sq.Ft)
' Froude number = 0.546

Upstream point elevation = 656.000(Ft.)
Downstream point elevation = 654.000(Ft.)
Flow length = 300.000(Ft.)
Travel time = 1.04 min.
Time of concentration = 15.65 min.
Depth of flow = 4.839(Ft.)
Average velocity = 4.819(Ft/s)
Total irregular channel flow = 705.338(CFS)
Irregular channel normal depth above invert elev. = 4.839(Ft.)
Average velocity of channel(s) = 4.819(Ft/s)

Process from Point/Station 4.300 to Point/Station 4.300
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 348.883(Ac.)
Runoff from this stream = 705.338(CFS)
Time of concentration = 15.65 min.
Rainfall intensity = 4.418(In/Hr)

Process from Point/Station 523.000 to Point/Station 4.300
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 8.198(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 6.00 min. Rain intensity = 8.20(In/Hr)
Total area = 0.860(Ac.) Total runoff = 4.100(CFS)

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+++++
Process from Point/Station      4.300 to Point/Station      4.300
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.860(Ac.)
 Runoff from this stream = 4.100(CFS)
 Time of concentration = 6.00 min.
 Rainfall intensity = 8.198(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	705.338	15.65	4.418
2	4.100	6.00	8.198

Qmax(1) =
 1.000 * 1.000 * 705.338) +
 0.539 * 1.000 * 4.100) + = 707.547
 Qmax(2) =
 1.000 * 0.383 * 705.338) +
 1.000 * 1.000 * 4.100) + = 274.561

Total of 2 streams to confluence:
 Flow rates before confluence point:
 705.338 4.100
 Maximum flow rates at confluence using above data:
 707.547 274.561
 Area of streams before confluence:
 348.883 0.860
 Results of confluence:
 Total flow rate = 707.547(CFS)
 Time of concentration = 15.647 min.
 Effective stream area after confluence = 349.743(Ac.)

```

+++++
Process from Point/Station      4.300 to Point/Station      430.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

```

Upstream point/station elevation = 647.000(Ft.)
 Downstream point/station elevation = 641.300(Ft.)
 Pipe length = 83.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 707.547(CFS)
 Nearest computed pipe diameter = 63.00(In.)
 Calculated individual pipe flow = 707.547(CFS)
 Normal flow depth in pipe = 47.16(In.)
 Flow top width inside pipe = 54.67(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 40.69(Ft/s)
 Travel time through pipe = 0.03 min.
 Time of concentration (TC) = 15.68 min.

```

+++++
Process from Point/Station      430.000 to Point/Station      430.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 349.743(Ac.)
 Runoff from this stream = 707.547(CFS)
 Time of concentration = 15.68 min.
 Rainfall intensity = 4.412(In/Hr)

```

+++++
Process from Point/Station      434.000 to Point/Station      430.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

```

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 8.198(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 6.00 min. Rain intensity = 8.20(In/Hr)
 Total area = 1.850(Ac.) Total runoff = 8.780(CFS)

 Process from Point/Station 430.000 to Point/Station 430.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 1.850(Ac.)
 Runoff from this stream = 8.780(CFS)
 Time of concentration = 6.00 min.
 Rainfall intensity = 8.198(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	707.547	15.68	4.412
2	8.780	6.00	8.198

Qmax(1) =
 1.000 * 1.000 * 707.547) +
 0.538 * 1.000 * 8.780) + = 712.272
 Qmax(2) =
 1.000 * 0.383 * 707.547) +
 1.000 * 1.000 * 8.780) + = 279.500

Total of 2 streams to confluence:
 Flow rates before confluence point:
 707.547 8.780
 Maximum flow rates at confluence using above data:
 712.272 279.500
 Area of streams before confluence:
 349.743 1.850
 Results of confluence:
 Total flow rate = 712.272(CFS)
 Time of concentration = 15.681 min.
 Effective stream area after confluence = 351.593(Ac.)

 Process from Point/Station 430.000 to Point/Station 5.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 0.355(Ft.), Average velocity = 3.337(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	25.00
2	60.00	0.00
3	660.00	0.00
4	720.00	20.00

Manning's 'N' friction factor = 0.045

Sub-Channel flow = 712.278(CFS)
 flow top width = 601.918(Ft.)
 velocity = 3.337(Ft/s)
 area = 213.424(Sq.Ft)
 Froude number = 0.988

Upstream point elevation = 641.300(Ft.)
 Downstream point elevation = 631.000(Ft.)
 Flow length = 253.000(Ft.)

Travel time = 1.26 min.
Time of concentration = 16.94 min.
Depth of flow = 0.355(Ft.)
Average velocity = 3.337(Ft/s)
Total irregular channel flow = 712.272(CFS)
Irregular channel normal depth above invert elev. = 0.355(Ft.)
Average velocity of channel(s) = 3.337(Ft/s)

Process from Point/Station 5.000 to Point/Station 5.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 351.593(Ac.)
Runoff from this stream = 712.272(CFS)
Time of concentration = 16.94 min.
Rainfall intensity = 4.197(In/Hr)

Process from Point/Station 82.000 to Point/Station 5.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 9.00 min. Rain intensity = 6.31(In/Hr)
Total area = 103.820(Ac.) Total runoff = 182.900(CFS)

Process from Point/Station 5.000 to Point/Station 5.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 103.820(Ac.)
Runoff from this stream = 182.900(CFS)
Time of concentration = 9.00 min.
Rainfall intensity = 6.312(In/Hr)

Process from Point/Station 648.000 to Point/Station 5.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 5.897(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 10.00 min. Rain intensity = 5.90(In/Hr)
Total area = 15.310(Ac.) Total runoff = 7.160(CFS)

Process from Point/Station 5.000 to Point/Station 5.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 15.310(Ac.)

Runoff from this stream = 7.160(CFS)
 Time of concentration = 10.00 min.
 Rainfall intensity = 5.897(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	712.272	16.94	4.197
2	182.900	9.00	6.312
3	7.160	10.00	5.897

Qmax(1) =
 1.000 * 1.000 * 712.272) +
 0.665 * 1.000 * 182.900) +
 0.712 * 1.000 * 7.160) + = 838.978

Qmax(2) =
 1.000 * 0.531 * 712.272) +
 1.000 * 1.000 * 182.900) +
 1.000 * 0.900 * 7.160) + = 567.655

Qmax(3) =
 1.000 * 0.590 * 712.272) +
 0.934 * 1.000 * 182.900) +
 1.000 * 1.000 * 7.160) + = 598.389

Total of 3 streams to confluence:
 Flow rates before confluence point:
 712.272 182.900 7.160
 Maximum flow rates at confluence using above data:
 838.978 567.655 598.389
 Area of streams before confluence:
 351.593 103.820 15.310
 Results of confluence:
 Total flow rate = 838.978(CFS)
 Time of concentration = 16.945 min.
 Effective stream area after confluence = 470.723(Ac.)

 Process from Point/Station 5.000 to Point/Station 543.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 0.405(Ft.), Average velocity = 3.444(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 25.00
 2 60.00 0.00
 3 660.00 0.00
 4 720.00 20.00
 Manning's 'N' friction factor = 0.045

Sub-Channel flow = 838.982(CFS)
 ' ' flow top width = 602.189(Ft.)
 ' ' velocity = 3.444(Ft/s)
 ' ' area = 243.614(Sq.Ft)
 ' ' Froude number = 0.954

Upstream point elevation = 631.000(Ft.)
 Downstream point elevation = 627.000(Ft.)
 Flow length = 110.000(Ft.)
 Travel time = 0.53 min.
 Time of concentration = 17.48 min.
 Depth of flow = 0.405(Ft.)
 Average velocity = 3.444(Ft/s)
 Total irregular channel flow = 838.978(CFS)
 Irregular channel normal depth above invert elev. = 0.405(Ft.)
 Average velocity of channel(s) = 3.444(Ft/s)

 Process from Point/Station 543.000 to Point/Station 543.000

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 470.723(Ac.)
 Runoff from this stream = 838.978(CFS)
 Time of concentration = 17.48 min.
 Rainfall intensity = 4.114(In/Hr)

 Process from Point/Station 543.000 to Point/Station 543.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [MEDIUM DENSITY RESIDENTIAL]
 (10.9 DU/A or Less)
 Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 7.423(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 7.00 min. Rain intensity = 7.42(In/Hr)
 Total area = 5.790(Ac.) Total runoff = 20.100(CFS)

 Process from Point/Station 543.000 to Point/Station 543.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 5.790(Ac.)
 Runoff from this stream = 20.100(CFS)
 Time of concentration = 7.00 min.
 Rainfall intensity = 7.423(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	838.978	17.48	4.114
2	20.100	7.00	7.423

Qmax(1) =
 1.000 * 1.000 * 838.978) +
 0.554 * 1.000 * 20.100) + = 850.118
 Qmax(2) =
 1.000 * 0.401 * 838.978) +
 1.000 * 1.000 * 20.100) + = 356.128

Total of 2 streams to confluence:
 Flow rates before confluence point:
 838.978 20.100
 Maximum flow rates at confluence using above data:
 850.118 356.128
 Area of streams before confluence:
 470.723 5.790
 Results of confluence:
 Total flow rate = 850.118(CFS)
 Time of concentration = 17.477 min.
 Effective stream area after confluence = 476.513(Ac.)

 Process from Point/Station 543.000 to Point/Station 5.100
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 5.122(Ft.), Average velocity = 9.607(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate

1	0.00	24.00
2	85.00	0.00
3	226.00	44.00

Manning's 'N' friction factor = 0.045

Sub-Channel flow = 850.118(CFS)

'	'	flow top width =	34.553(Ft.)
'	'	velocity=	9.607(Ft/s)
'	'	area =	88.488(Sq.Ft)
'	'	Froude number =	1.058

Upstream point elevation = 627.000(Ft.)

Downstream point elevation = 604.000(Ft.)

Flow length = 900.000(Ft.)

Travel time = 1.56 min.

Time of concentration = 19.04 min.

Depth of flow = 5.122(Ft.)

Average velocity = 9.607(Ft/s)

Total irregular channel flow = 850.118(CFS)

Irregular channel normal depth above invert elev. = 5.122(Ft.)

Average velocity of channel(s) = 9.607(Ft/s)

Process from Point/Station 5.100 to Point/Station 5.100

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 476.513(Ac.)

Runoff from this stream = 850.118(CFS)

Time of concentration = 19.04 min.

Rainfall intensity = 3.893(In/Hr)

Process from Point/Station 243.000 to Point/Station 5.100

**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 1.000

[MEDIUM DENSITY RESIDENTIAL]

(10.9 DU/A or Less)

Impervious value, Ai = 0.450

Sub-Area C Value = 0.600

Rainfall intensity (I) = 6.312(In/Hr) for a 100.0 year storm

User specified values are as follows:

TC = 9.00 min. Rain intensity = 6.31(In/Hr)

Total area = 8.280(Ac.) Total runoff = 24.200(CFS)

Process from Point/Station 5.100 to Point/Station 5.100

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 8.280(Ac.)

Runoff from this stream = 24.200(CFS)

Time of concentration = 9.00 min.

Rainfall intensity = 6.312(In/Hr)

Process from Point/Station 552.000 to Point/Station 5.100

**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 1.000

[MEDIUM DENSITY RESIDENTIAL]

(10.9 DU/A or Less)

Impervious value, Ai = 0.450
 Sub-Area C Value = 0.600
 Rainfall intensity (I) = 7.423(In/Hr) for a 100.0 year storm
 User specified values are as follows:
 TC = 7.00 min. Rain intensity = 7.42(In/Hr)
 Total area = 4.450(Ac.) Total runoff = 13.800(CFS)

 Process from Point/Station 5.100 to Point/Station 5.100
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 4.450(Ac.)
 Runoff from this stream = 13.800(CFS)
 Time of concentration = 7.00 min.
 Rainfall intensity = 7.423(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	850.118	19.04	3.893
2	24.200	9.00	6.312
3	13.800	7.00	7.423

Qmax(1) =
 1.000 * 1.000 * 850.118) +
 0.617 * 1.000 * 24.200) +
 0.524 * 1.000 * 13.800) + = 872.281
 Qmax(2) =
 1.000 * 0.473 * 850.118) +
 1.000 * 1.000 * 24.200) +
 0.850 * 1.000 * 13.800) + = 437.806
 Qmax(3) =
 1.000 * 0.368 * 850.118) +
 1.000 * 0.778 * 24.200) +
 1.000 * 1.000 * 13.800) + = 345.189

Total of 3 streams to confluence:
 Flow rates before confluence point:
 850.118 24.200 13.800
 Maximum flow rates at confluence using above data:
 872.281 437.806 345.189
 Area of streams before confluence:
 476.513 8.280 4.450
 Results of confluence:
 Total flow rate = 872.281(CFS)
 Time of concentration = 19.039 min.
 Effective stream area after confluence = 489.243(Ac.)

 Process from Point/Station 5.100 to Point/Station 5.200
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Depth of flow = 4.968(Ft.), Average velocity = 10.478(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 24.00
 2 85.00 0.00
 3 226.00 44.00
 Manning's 'N' friction factor = 0.045

Sub-Channel flow = 872.282(CFS)
 flow top width = 33.514(Ft.)
 velocity = 10.478(Ft/s)
 area = 83.248(Sq.Ft)
 Froude number = 1.172

Upstream point elevation = 604.000(Ft.)

Downstream point elevation = 592.000(Ft.)
Flow length = 379.000(Ft.)
Travel time = 0.60 min.
Time of concentration = 19.64 min.
Depth of flow = 4.968(Ft.)
Average velocity = 10.478(Ft/s)
Total irregular channel flow = 872.281(CFS)
Irregular channel normal depth above invert elev. = 4.968(Ft.)
Average velocity of channel(s) = 10.478(Ft/s)

Process from Point/Station 5.200 to Point/Station 5.200
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 489.243(Ac.)
Runoff from this stream = 872.281(CFS)
Time of concentration = 19.64 min.
Rainfall intensity = 3.815(In/Hr)

Process from Point/Station 559.000 to Point/Station 5.200
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[MEDIUM DENSITY RESIDENTIAL]
(10.9 DU/A or Less)
Impervious value, Ai = 0.450
Sub-Area C Value = 0.600
Rainfall intensity (I) = 7.423(In/Hr) for a 100.0 year storm
User specified values are as follows:
TC = 7.00 min. Rain intensity = 7.42(In/Hr)
Total area = 4.620(Ac.) Total runoff = 13.000(CFS)

Process from Point/Station 5.200 to Point/Station 5.200
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 4.620(Ac.)
Runoff from this stream = 13.000(CFS)
Time of concentration = 7.00 min.
Rainfall intensity = 7.423(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	872.281	19.64	3.815
2	13.000	7.00	7.423

Qmax(1) =
1.000 * 1.000 * 872.281) +
0.514 * 1.000 * 13.000) + = 878.964

Qmax(2) =
1.000 * 0.356 * 872.281) +
1.000 * 1.000 * 13.000) + = 323.872

Total of 2 streams to confluence:
Flow rates before confluence point:
872.281 13.000
Maximum flow rates at confluence using above data:
878.964 323.872
Area of streams before confluence:
489.243 4.620
Results of confluence:
Total flow rate = 878.964(CFS)

Time of concentration = 19.641 min.
Effective stream area after confluence = 493.863(Ac.)

Process from Point/Station 5.200 to Point/Station 6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 899.153(CFS)
Depth of flow = 5.591(Ft.), Average velocity = 8.756(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 24.00
2 85.00 0.00
3 226.00 44.00

Manning's 'N' friction factor = 0.045

Sub-Channel flow = 899.153(CFS)
' ' flow top width = 37.718(Ft.)
' ' velocity = 8.756(Ft/s)
' ' area = 105.439(Sq.Ft)
' ' Froude number = 0.923

Upstream point elevation = 592.000(Ft.)
Downstream point elevation = 575.000(Ft.)
Flow length = 900.000(Ft.)
Travel time = 1.71 min.
Time of concentration = 21.35 min.
Depth of flow = 5.591(Ft.)
Average velocity = 8.756(Ft/s)
Total irregular channel flow = 899.153(CFS)
Irregular channel normal depth above invert elev. = 5.591(Ft.)
Average velocity of channel(s) = 8.756(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[LOW DENSITY RESIDENTIAL]
(2.0 DU/A or Less)
Impervious value, Ai = 0.200
Sub-Area C Value = 0.460
Rainfall intensity = 3.615(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.463 CA = 267.626
Subarea runoff = 40.386(CFS) for 83.770(Ac.)
Total runoff = 919.350(CFS) Total area = 577.633(Ac.)
Depth of flow = 5.280(Ft.), Average velocity = 8.859(Ft/s)
End of computations, total study area = 577.633 (Ac.)

APPENDIX 5

SWMM CALCULATION

I. MODEL SETUP

Pre-development Model Setup

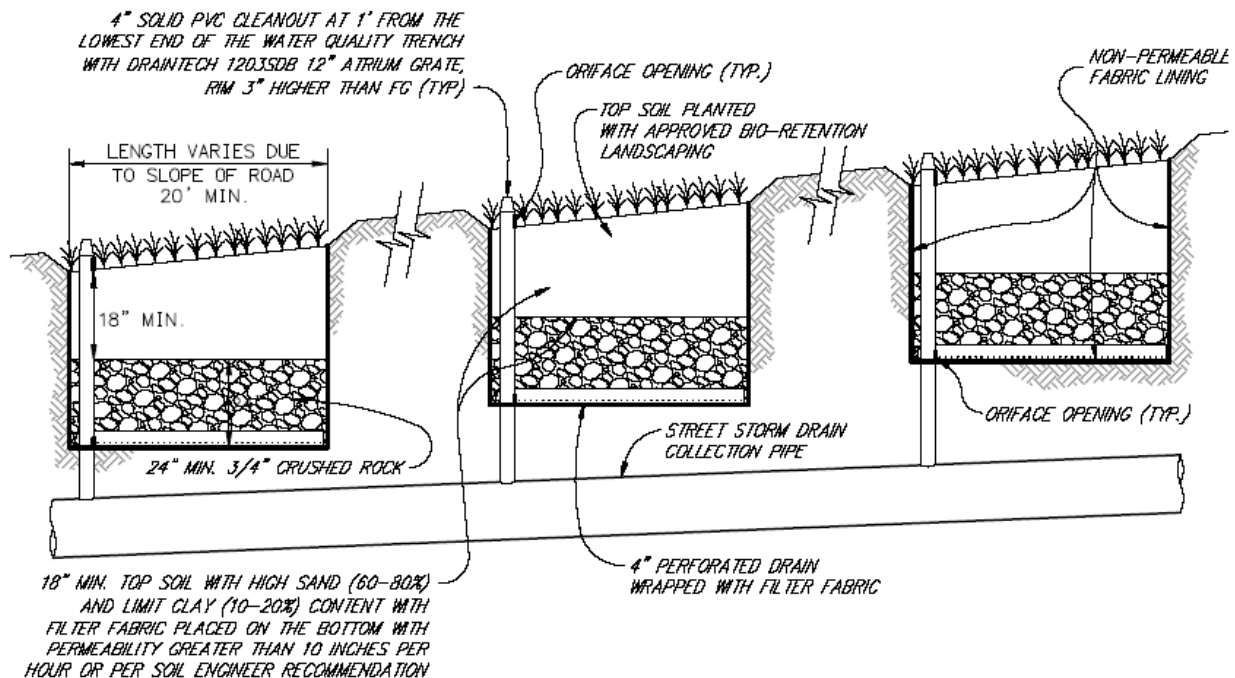
The SWMM model for the pre-development site is depicted in figure 3 and 4 on the next page. It consists of a rain gage “Oceanside” that provides continuous precipitation input to a sub-catchment with its outfall based on the contributing basins.

Imperviousness

The imperviousness parameter in SWMM is the effective or directly connected impervious area, which is typically less than the total imperviousness and is assume a 60% of imperviousness for the pads and 100% impervious for the streets. The effective impervious area is the impervious area that drains directly to the Stormwater conveyance system. The pre-development condition is undeveloped. For the purpose of this preliminary study, the site is assumed to have NO impervious surface in the existing condition.

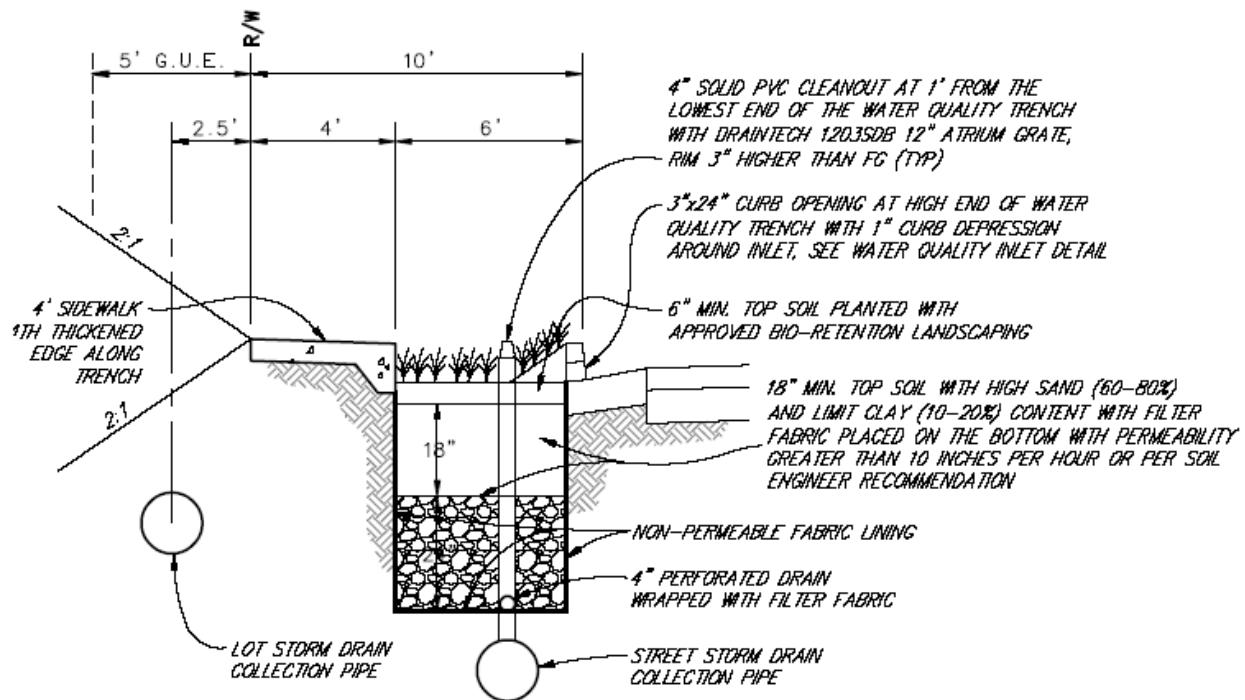
Post-Development Model Setup

Figure 3 and 4 illustrate each contributing basin discharging its overland flow directly into the bio-retention system. Each bio-retention layer section has a similar configuration as seen as in the detail drawing below (this is a typical condition that applies to almost all of the lots). There is no actual elevation entered in the program. The bottom elevation of the bio-retention surface storage is assumed at 0 ft. The pipe outlet between the junction node and the final outfall nodes has minus elevations to avoid a backwater effect.

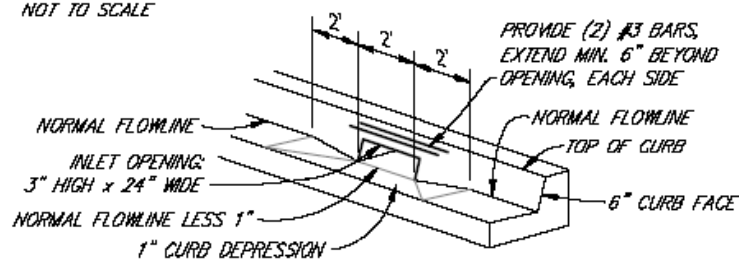


SEE SHEET 2 FOR TYPICAL CROSS-SECTION

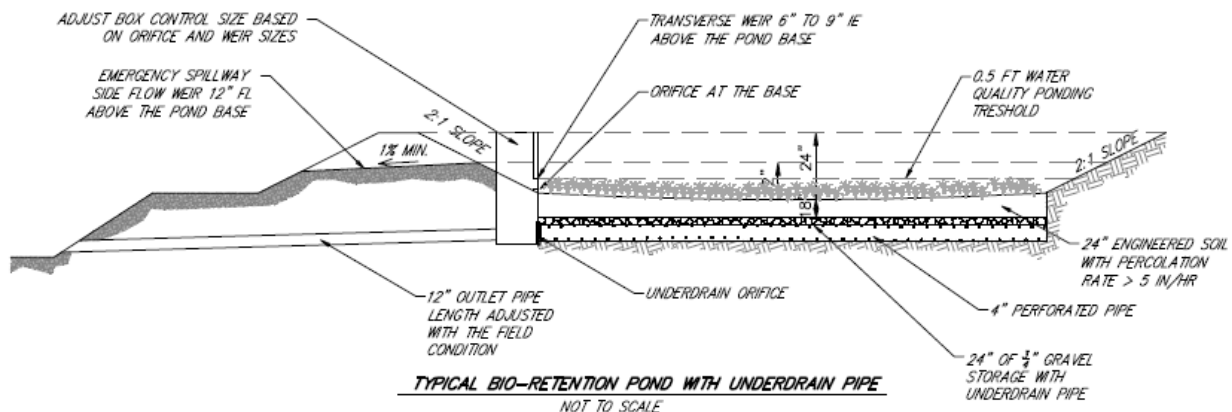
WATER QUALITY TRENCH TYPICAL SECTION
NOT TO SCALE



WATER QUALITY TRENCH CROSS-SECTION
NOT TO SCALE



WATER QUALITY INLET DETAIL
NOT TO SCALE



TYPICAL BIO-RETENTION POND WITH UNDERDRAIN PIPE
NOT TO SCALE

Figure-2. Typical Bio-retention Section

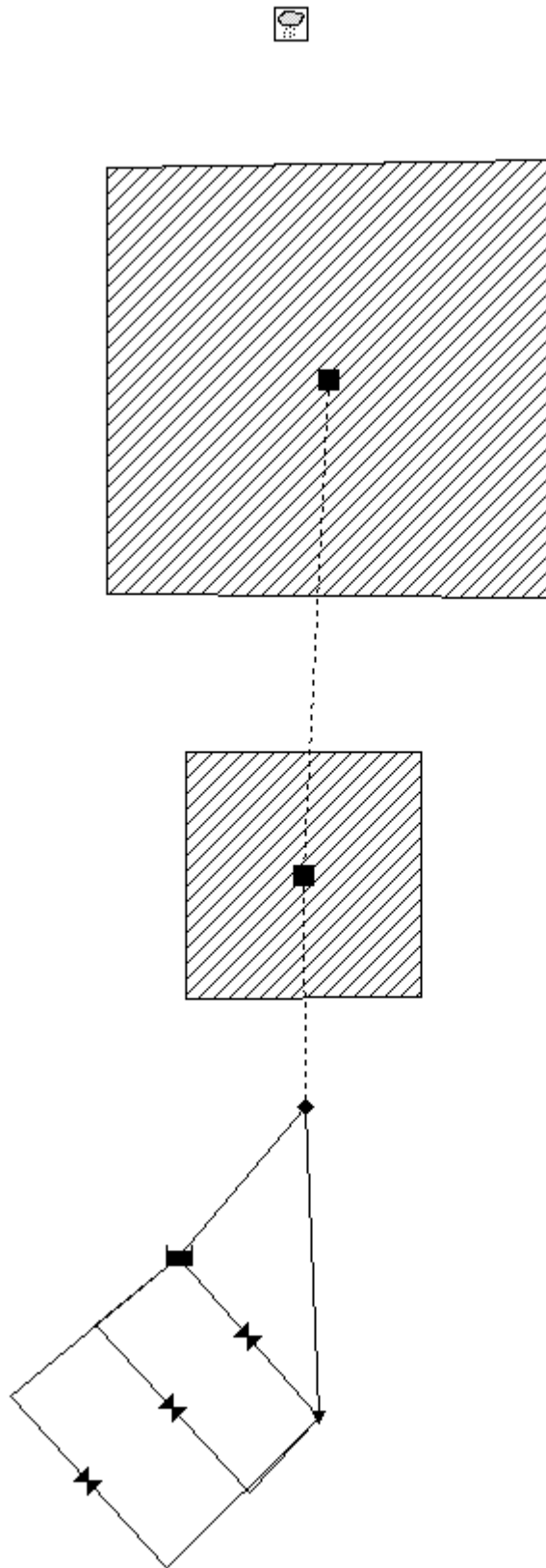


Figure-3. Mitigated Post-Development of SWMM continuous model

II. SYSTEM REPRESENTATION

SWMM is a distributed model, which means that a study area can be subdivided into any number of irregular sub-catchments to best capture the effect that spatial variability in topography, drainage pathways, land cover, and soil characteristics have on runoff generation. For modeling of Hydromodification calculations, there are four main system representations: Rain gage, Sub-catchment (contributing basin or LID area), Nodes and Links.

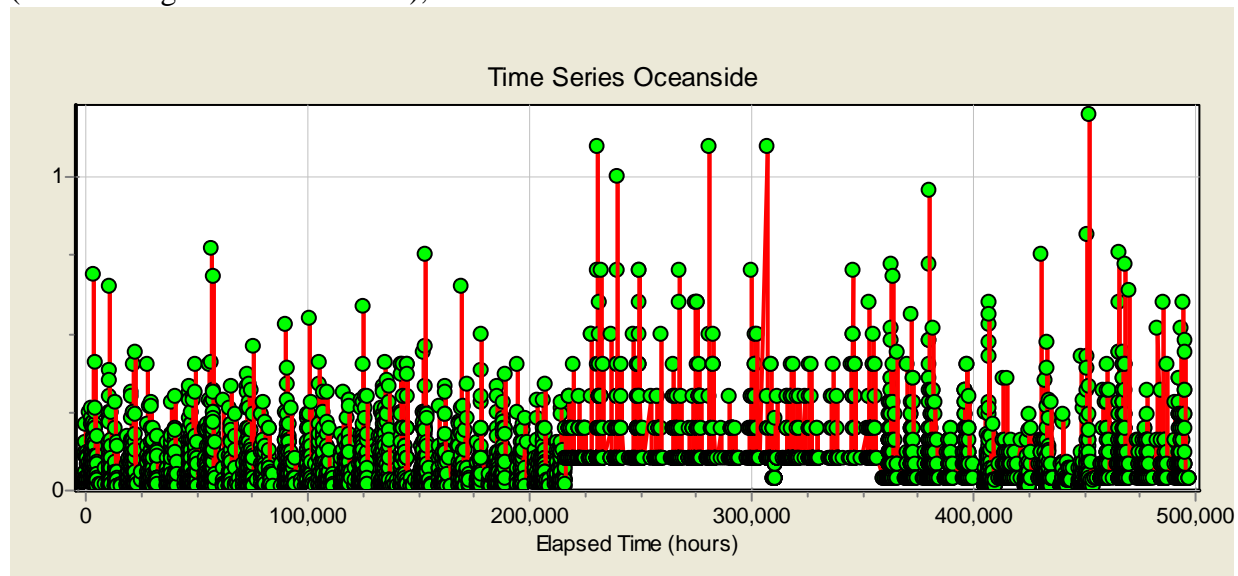


Fig. 4 – Time series rain data, which corresponds to runoff estimates for each of the 508,080 time steps (each date and hour) of the 58-year simulation period. (Inches/hour vs. elapsed time)

Rain Gage

The properties of a rain gage describe the source and format of the precipitation data that are applied to the study area. In this project, the rainfall data consist of a long-term rainfall record stored in a user-defined Time Series labeled as “Oceanside” rain gage station. The Oceanside rain station was chosen due to its data quality and its location to the project site.

The rain gage supplies precipitation data for one or more sub-catchment areas in a study region taken from the Project Clean Water website (www.projectcleanwater.org). This data file contains rainfall intensity, hourly-recorded time interval, and the dates of recorded precipitation each hour. The Oceanside rain data has approximately 58 years of hourly precipitation data from 8/28/1951 to 5/23/2008 and generates 58 years of hourly runoff estimates, which corresponds to runoff estimates for each of the 508,080 time steps (each date and hour) of the 58 year simulation period. See figure 1 for hourly precipitation intensity graph for 58 years in inches.

Sub-catchment (contributing basin or LID area)

A basin is modeled using a sub-catchment object, which contains some of the following properties:

Rain Gage

The rate of stormwater runoff and volume depends directly on the precipitation magnitude and its spatial and temporal distribution over the catchment. Each sub-catchment in SWMM is linked to a rain gage object that describes the format and source of the rainfall input for the sub-catchment.

Area

This area is bounded by the sub-catchment boundary. Its value is determined directly from maps or field surveys of the site or by using SWMM's Auto-length tool when the sub-catchment is drawn to scale on SWMM's study area map. This Project is divided into several sub-catchments based on its outfall. Bio-retention strips are calculated based on the average areas as follows:

0.066 acres

0.085 acres

0.108 acres

0.175 acres

Bio-retention ponds:

0.61 acres (Pond B)

0.285 acres (Pond C)

11.06 acres (Pond D)

1.26 acres (Pond E)

1.55 acres (Pond F)

13.3 acres (Pond G)

0.67 acres (Pond H)

0.48 acres (Pond J)

2.22 acres (Pond K)

Width

Width can be defined as the sub-catchment's area divided by the length of the longest overland flow path that water can travel. When there are several such paths, one would use an average of their lengths to compute a width. If overland flow is visualized as running down –slope off an idealized, rectangular catchment, then the width of the sub-catchment is the physical width of overland flow. In natural areas, true overland flow can only occur for distances of about 500 feet before it begins to consolidate into a small stream flow. In post-development, the true overland flow can be very short before it is collected into open channels. A maximum overland flow of 500 ft is appropriate for a non-urban catchment, while the typical overland flow length is appropriate for non-urban catchments; the typical overland flow length is the length from the back of a representative lot to the center of the street for urban catchments. If the overland flow length varies greatly within a sub-catchment, then an area-weighted average should be used.

Slope

This is the slope of the land surface over which runoff flows and is the same for both the pervious and impervious surfaces. It is the slope of what one considers being the overland flow path or its area-weighted average if there are several paths in the sub-catchment.

Imperviousness

This is the percentage of sub-catchment area covered by impervious surfaces such as sidewalks and roadways or whatever surfaces that rainfall cannot infiltrate. 60% of imperviousness was used for pad areas.

Roughness Coefficient

The roughness coefficient reflects the amount of resistance that overland flow encounters as it runs off of the sub-catchment surface.

Infiltration Model

The pre-development condition is primarily barren land with dirt roads. Some areas have been developed with pavement. Based on the hydrology manual this area was grouped as soil type D. In the model, clay soil was used for the post-development condition and sandy clay loam was used as the pre-development condition for a very conservative approach. Infiltration of rainfall from the pervious area of a sub-catchment into the unsaturated upper soil zone can be described using three different infiltration models: Horton, Green-Ampt, and Curve Number. There is no general agreement on which method of these three is the best.

The Green-Ampt method was chosen to calculate the infiltration of the pervious areas based on the availability of data for this project. It is invoked when editing the infiltration property of a sub-catchment.

Table 1 – Soil Infiltration Parameter

Soil Texture Class	K	Ψ	φ	FC	WP
Sand	4.74	1.93	0.437	0.062	0.024
Loamy Sand	1.18	2.40	0.437	0.105	0.047
Sandy Loam	0.43	4.33	0.453	0.190	0.085
Loam	0.13	3.50	0.463	0.232	0.116
Silt Loam	0.26	6.69	0.501	0.284	0.135
Sandy Clay Loam	0.06	8.66	0.398	0.244	0.136
Clay Loam	0.04	8.27	0.464	0.310	0.187
Silty Clay Loam	0.04	10.63	0.471	0.342	0.210
Sandy Clay	0.02	9.45	0.430	0.321	0.221
Silty Clay	0.02	11.42	0.479	0.371	0.251
Clay	0.01	12.60	0.475	0.378	0.265

K = hydraulic conductivity, in/hr

Ψ = suction head, in.

φ = porosity, fraction

FC = field capacity, fraction

WP = wilting point, fraction

Source: Rawls, W.J. et al., (1983). *J. Hyd. Engr.*, 109:1316.

LID controls

Utilizing LID controls within a SWMM project is a two step process that:

- Creates a set of scale-independent LID controls that can be deployed throughout the study area,
- Assign any desired mix and sizing of these controls to designated sub-catchments.

The LID control type that was selected was a bio-retention cell that contains vegetation grown in an engineered soil mixture placed above a gravel drainage bed. Bio-retention provides storage, infiltration (depending on the soil type) and evaporation of both direct rainfall and runoff captured from surrounding areas. For this project, we do not allow infiltration to the existing/filled soil.

III. CONTINUOUS SIMULATION OPTIONS

Kinematic Wave Routing Model

This routing method solves the continuity equation along with a simplified form of the momentum equation in each conduit. The latter requires that the slope of the water surface be equal to the slope of the conduit.

The maximum flow that can be conveyed through a conduit is the full normal flow value. Any flow in excess of this entering the inlet node is either lost from the system or can pond atop the inlet node and be re-introduced into the conduit as capacity becomes available.

Kinematic wave routing allows flow and area to vary both spatially and temporally within a conduit. This can result in attenuated and delayed outflow hydrographs as inflow is routed through the channel. However this form of routing cannot account for backwater effects, entrance/exit losses, flow reversal, or pressurized flow, and is also restricted to dendritic network layouts. It can usually maintain numerical stability with moderately large time steps, on the order of 1 to 5 minutes. Since the aforementioned effects are not expected to be significant, this alternative can be an accurate and efficient routing method, especially for long-term simulations.

Simulation Dates

These dates determine the starting and ending dates/times of a simulation and are chosen based on the rain data availability.

Start analysis on 01/03/1951

Start Reporting on 01/03/1951

End Analysis on 05/23/2008

Time Steps

The Time Steps establish the length of the time steps used for runoff computation, routing computation and results reporting. Time steps are specified in days and hours: minutes: seconds except for flow routing which is entered as decimal seconds.

Climatology

-Evaporation Data

The available evaporation data for San Diego County that is similar to this project condition is taken from the Chula Vista Evaporation Station Western Regional Climate Center.

Table 2 – Chula Vista Monthly Evaporation data (in/day)

January	February	March	April	May	June
0.094	0.115	0.168	0.202	0.225	0.232
July	Augustus	September	October	November	December
0.254	0.250	0.207	0.167	0.119	0.09

IV. BIO-RETENTION AS LID CONTROL

LID controls are represented by a combination of vertical layers whose properties are defined on a per-unit-area basis. This allows an LID of the same design but differing coverage area to easily be placed within different sub-catchments of a study area. During a simulation, SWMM performs a moisture balance that keeps track of how much water moves between and is stored within each LID layer. If the bio-retention basin is full and water is leaving the upper weir, the flow is divided in two flows: the lower flow discharging from the bottom orifice directly draining to the point of compliance and the upper flow is routed at the top of the bio-retention basin and after routing, discharged to the point of compliance. In this project, we used 100% of the area of this specific sub-catchment for bio-retention. In SWMM a divider was used to model this condition. All sub-catchments in one tributary area were directed to a Flow Divider. A Flow Divider is a drainage system node that diverts inflow to a specific conduit in a prescribed manner such as a cutoff type. A Flow Divider with a cutoff type diverts all inflow above a defined cutoff value, in this case we used an orifice equation: $\text{Discharge} = q = CA[2g(h-H_d)]^{0.5}$.

A detention basin sub routine was added at the top of the bio-retention where a weir is added for control purposes, and the storage curve is also provided, see the next section “Modeling bio-retention surface ponding in SWMM 5.0”. For a bio-retention strip, the drain coefficient is a 0.5 inches underdrain orifice with 24” gravel storage for all bio-retention systems is 0.0124 in/hr and 2 inches for the ponds resulting 0.2243 in/hr.

1. Surface

Storage Depth

When confining walls or berms are present, this is the maximum depth to which water can pond above the surface of the unit before overflow occurs (in inches). In this project, storage depth was assumed as 2” (bio-retention strips) and 6” (bio-retention ponds) to detain the water quality volume.

Vegetation Volume Fraction

It is the fraction of the volume within the storage depth that is filled with vegetation. This is the volume occupied by stems and leaves, not their surface area coverage. Normally this volume can be ignored, but may be as high as 0.1 to 0.2 for very dense vegetative growth. Based on our visual observation in the field, the average type of vegetation for this site is a low-density vegetation type. Therefore, we used 0.1 for the vegetation volume fraction assuming type of vegetation used is a low-density type.

Surface Roughness

Manning's n value for overland flow over the surface of a vegetative swale. We used n=0.025 for brush roughness.

Surface Slope

Slope of porous pavement surface or vegetative swale (percent). We use 0 percent for bio-retention.

2. Soil

Thickness

The thickness of the soil layer (inches). We used a typical value for a rain garden, which is 18 inches for bio-retention strips and 24" for the ponds to promote taller type vegetations.

Porosity

The volume of pore space relative to total volume of soil (as a fraction). We designed it with a soil mix porosity of 0.5 maximum for a good percolation rate (see Table 1 – Soil Infiltration Parameter).

Field Capacity

Volume of pore water relative to total volume after the soil has been allowed to drain fully (as a fraction). We used 0.1 for this soil. Below this level, vertical drainage of water through the soil layer does not occur. (see Table 1 – Soil Infiltration Parameter).

Wilting Point

Volume of pore water relative to total volume for a well-dried soil where only bound water remains (as a fraction). The moisture content of the soil cannot fall below this limit.

We assumed the minimum moisture content within this bio-retention soil is 0.04 (see Table 1 – Soil Infiltration Parameter).

Conductivity

Hydraulic conductivity for the fully saturated soil is 5 inches/hour. This is a design minimum value for percolation rate.

Conductivity Slope

Slope of the curve of log (conductivity) versus soil moisture content (dimensionless). Typical values range from 5 for sands to 15 for silty clay. We designed this soil to have a very good percolation rate therefore the conductivity slope is 5.

Suction Head

The average value of soil capillary suction along the wetting front (inches). This is the same parameter as used in the Green-Ampt infiltration model. Table 1 was utilized to determine the capillary of the soil mix top layer of a bio-retention system. Sandy Loam was considered for approximately 10% clay content and sedimentation collected during a rain event, therefore the suction head will be 2 inches. This is an assumption of a suction head for the soil mix after several years of bio-retention life span.

3. Storage Layer

The Storage Layer page of the LID Control Editor describes the properties of the crushed stone or gravel layer used in bio-retention cells as a bottom storage/drainage layer. The following data fields are displayed:

Height

this is the thickness of a gravel layer (inches). Crushed stone and gravel layers are 24 inches thick.

Void Ratio

The volume of void space relative to the volume of solids in the layer. Typical values range from 0.5 to 0.75 for gravel beds. Note that porosity = void ratio / (1 + void ratio). We designed this void ratio to have a value of 0.60.

Conductivity

The rate at which water infiltrates into the native soil below the layer (in inches/hour). This would typically be the Saturated Hydraulic Conductivity of the surrounding sub-catchment if Green-Ampt infiltration is used. Since this is soil type D, we assumed a slow infiltration rate of the native soil, which is 0.025 or 0 for no infiltration.

Clogging Factor

Total volume of treated runoff it takes to completely clog the bottom of the layer divided by the void volume of the layer. A value of 0 was used to ignore clogging since the system does NOT consider infiltration to the native soils. Clogging progressively reduces the Infiltration Rate in direct proportion to the cumulative volume of runoff treated and may only be of concern for infiltration trenches with permeable bottoms and no under drains. We assumed zero for the clogging factor since the infiltration rate is not considered.

4. Underdrain Layer

LID storage layers can contain an optional underdrain system that collects stored water from the bottom of the layer and conveys it to a conventional storm drain. The Underdrain page of the LID Control Editor describes the properties of this system. It contains the following data entry fields:

Drain Coefficient and Drain Exponent

Coefficient C and exponent n that determines the rate of flow through the underdrain as a function of height of stored water above the drain height. The following equation is used to compute this flow rate (per unit area of the LID unit):

$$q = C(h-Hd)^n$$

where q is the outflow (in/hr), h is the height of stored water (inches), and Hd is the drain height. A typical value for n would be 0.5 (making the drain act like an orifice). A rough estimate for C can be based on the time T that is required to drain a depth D of stored water. For $n = 0.5$, $C = 2D^{1/2}/T$. See table 3 for drain coefficient results.

Drain Offset Height

Height of any underdrain piping above the bottom of a storage layer (inches). In this project, this value was set to 0 as the underdrain piping is at the bottom of the storage layer.

V. RUNNING THE SIMULATION

After setting up all the elements, running the model will take about 10 to 15 minutes on a 2.41 GHz processor. In general, the Run time will depend on the complexity of the watershed being modeled, the routing method used, and the size of the routing time step used. The larger the time steps, the faster the simulation, but the less detailed the results.

Model Results

SWMM's Status Report summarizes overall results for the 58-yr simulation. The runoff continuity error is ranging from -4.5 % to -1.03% and the flow routing continuity error is ranging from -0.018% to 0.13%. When a run completes successfully, the mass continuity errors for runoff, flow routing, and pollutant routing will be displayed in the Run Status window. These errors represent the percent difference between initial storage + total inflow and final storage + total outflow for the entire drainage system. If they exceed some reasonable level, such as 10 percent, then the validity of the analysis results must be questioned. The most common reasons for an excessive continuity error are computational time steps that are too long or conduits that are too short.

In addition to the system continuity error, the Status Report produced by a run will list those nodes of the drainage network that have the largest flow continuity errors. If the error for a node is excessive, then one should first consider if the node in question is of importance to the purpose of the simulation. If it is, then further study is warranted to determine how the error might be reduced.

Bio-retention Surface Storage Outflows

A statistics tool was used to analyze how often and for what periods of time the bio-retention will have a certain discharge and how the magnitudes of the peak discharges during these periods are distributed. This statistics tool can be found on SWMM's main menu bar by selecting Report|Statistics or by clicking the statistics icon (Σ) on SWMM's main toolbar.

The variable to be analyzed is total inflow; the time period used to define events is “**Event-Dependent**”, meaning that separate events will be defined by consecutive reporting periods where certain event threshold conditions are met. Within each such period, the statistic to be analyzed is the **Peak** value of total inflow to the node. The threshold criteria states that a new event begins whenever an inflow of a minimum specific flow rate that occurs at least 24 hours after the last inflow of that minimum amount was recorded.

The SWMM program generates the report for this statistical query, which contains four tabs. The first section is the Summary Statistic; the second is the Event Listing for the variable under study, the third section is Histogram and the last tab is the Frequency Plot. Table 4 below shows how the Peak Flow Frequency and the exceedance frequency tables were generated for the 2 basins based on the Partial Duration Series Criteria:

Table 4 – Partial Duration Series Criteria

SCENARIO	SEPARATION EVENT (HOURS)	FLOW FLOOR (CFS)	NUMBER OF EVENTS
PRE-DEVELOPMENT	24	0	605
POST-DEVELOPMENT (MITIGATED)	24	0	603

A separation event is a time period in which runoff does not exceed a prescribed threshold and sets the minimum number or hours that must occur between the end of a rain event and the start of the next rain event.

Flow Floor is the maximum value for the inter-event time period and it allows for separation of events. This value is typically set as an artificially low flow value to generate peak flow frequency and flow duration at a certain criteria.

The number of events corresponds to the total number of the discrete runoff events generated for the long-term rainfall record. Typically at the same value of flow floor, the post-development (unmitigated) flow will dramatically increase the number of discrete runoff events compared to the pre-development flow.

The SWMM program ranks the partial duration series, the exceedance frequency and the return period. They are computed using the Weibull formula for plotting position. See the flow duration curve and peak flow frequency on the following pages.

To compare the curves of a flow duration series between pre-development and mitigated post-development, the pre-development flow floor is set to a very low number (based on 0.002 cfs/acre) while the others are set with a higher value by trial and error so that the number of discrete runoff events become equal to or less than that of the pre-development. A closer number of events to the pre-development's number of events will generate a closer range of exceedance frequency for the mitigated or unmitigated post-development. It is important to have an equal number of events between the pre- and the mitigated post-development so that the exceedance frequencies have exact similar values. Therefore, flow duration curves between the pre- and the mitigated post-development can be compared equally and correctly.

VI. *RESULT ANALYSIS*

These graphs below were generated from Peak Flow Frequency and Flow Duration Statistics computed by the SWMM program see Appendix A for complete datasets.

For bio-retention with 0.066 acres of impervious tributary area

a. Flow Duration Curve Analysis

Under Pre-Development conditions the minimum geomorphically significant flow rate of 0.5Q2 is 0.039 cfs and from the graph on the previous page, flows would equal or exceed this value about 24.78% of the time. This increase in the duration of the geomorphically significant flow after development illustrates why duration control is closely linked to protecting creeks from accelerated erosion. The mitigated post-development shows that flows exceed 0.039 cfs only 18.71% which is less than the pre-development condition. This means the bio-retention system would counteract the effects of the increased pavement associated with development projects.

SUMMARY STATISTICS

=====

Object System
Variable Runoff (CFS)
Event Period Variable
Event Statistic Peak (CFS)
Event Threshold Runoff > 0.0049 (CFS)
Event Threshold Event Volume > 0.0000 (ft3)
Event Threshold Separation Time >= 24.0 (hr)
Period of Record 01/03/1951 to 05/23/2008

Number of Events 605
Event Frequency* 0.013
Minimum Value 0.005
Maximum Value 0.078
Mean Value 0.016
Std. Deviation 0.011
Skewness Coeff. 2.051

*Fraction of all reporting periods belonging to an event.

SUMMARY STATISTICS

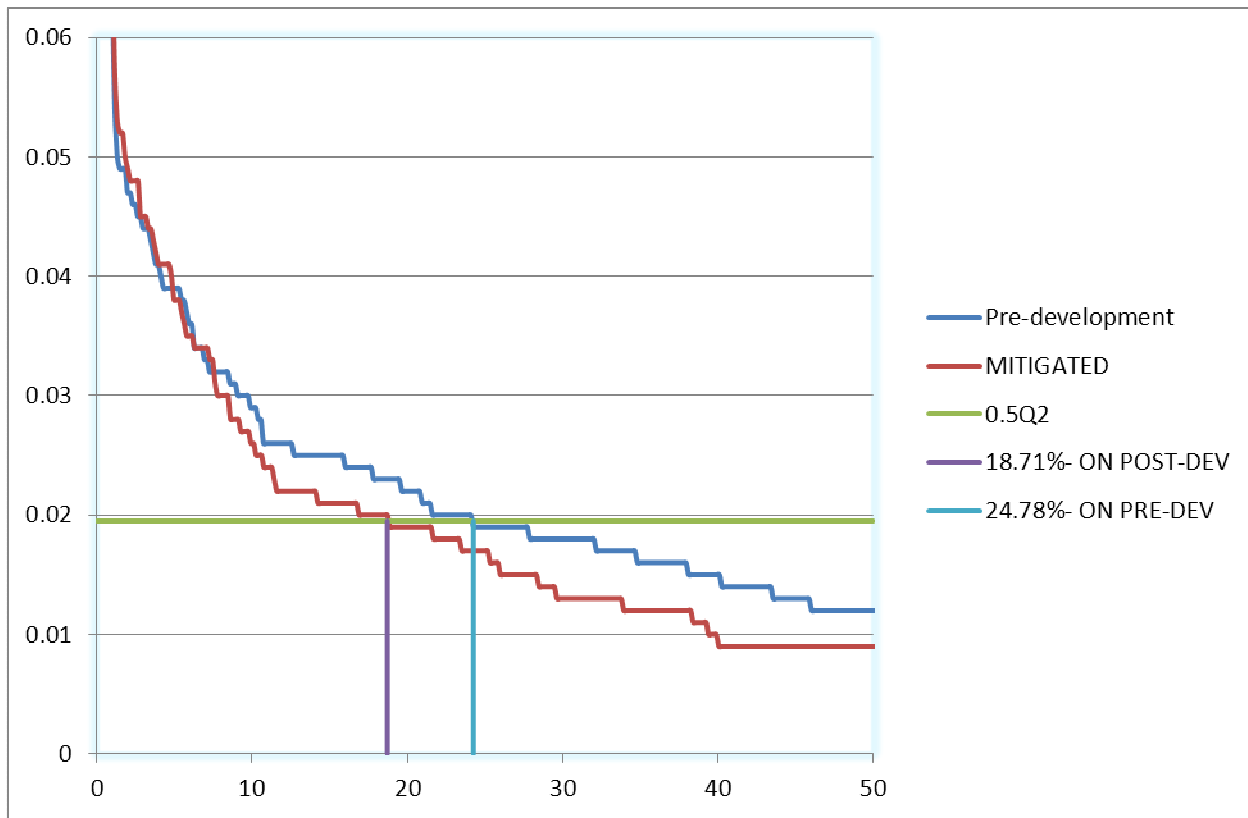
=====

Object Node Out1
Variable Total Inflow (CFS)
Event Period Variable
Event Statistic Peak (CFS)
Event Threshold Total Inflow > 0.0040 (CFS)
Event Threshold Event Volume > 0.0000 (ft3)
Event Threshold Separation Time >= 24.0 (hr)
Period of Record 01/03/1951 to 05/23/2008

Number of Events 603
Event Frequency* 0.012
Minimum Value 0.004
Maximum Value 0.083
Mean Value 0.013
Std. Deviation 0.011
Skewness Coeff. 2.557

*Fraction of all reporting periods belonging to an event.

Figure 5 – Summary Statistics for the pre- and the post-development



Pass or Fail Criteria

To evaluate the difference between Pre-development and the mitigated post-development conditions, a pass or fail analysis table is developed. This table compares the peak flow versus the percent time exceeded on each return period of mitigated post-development at the same exceedance frequency values as the pre-development condition in the flow duration curve.

The minimum comparison is started at the 0.5Q2 threshold to the Q10. The flow duration curve for the mitigated post-development is within 110% of the curve for the existing condition. The additional runoff volume generated from developing the site will be released to the downstream storm drain at a flow rate below the 50% of Q2 lower threshold. The project will neither increase peak flow rates between the Q2 and Q10 nor will it increase the peak flows more than 10% at any range.

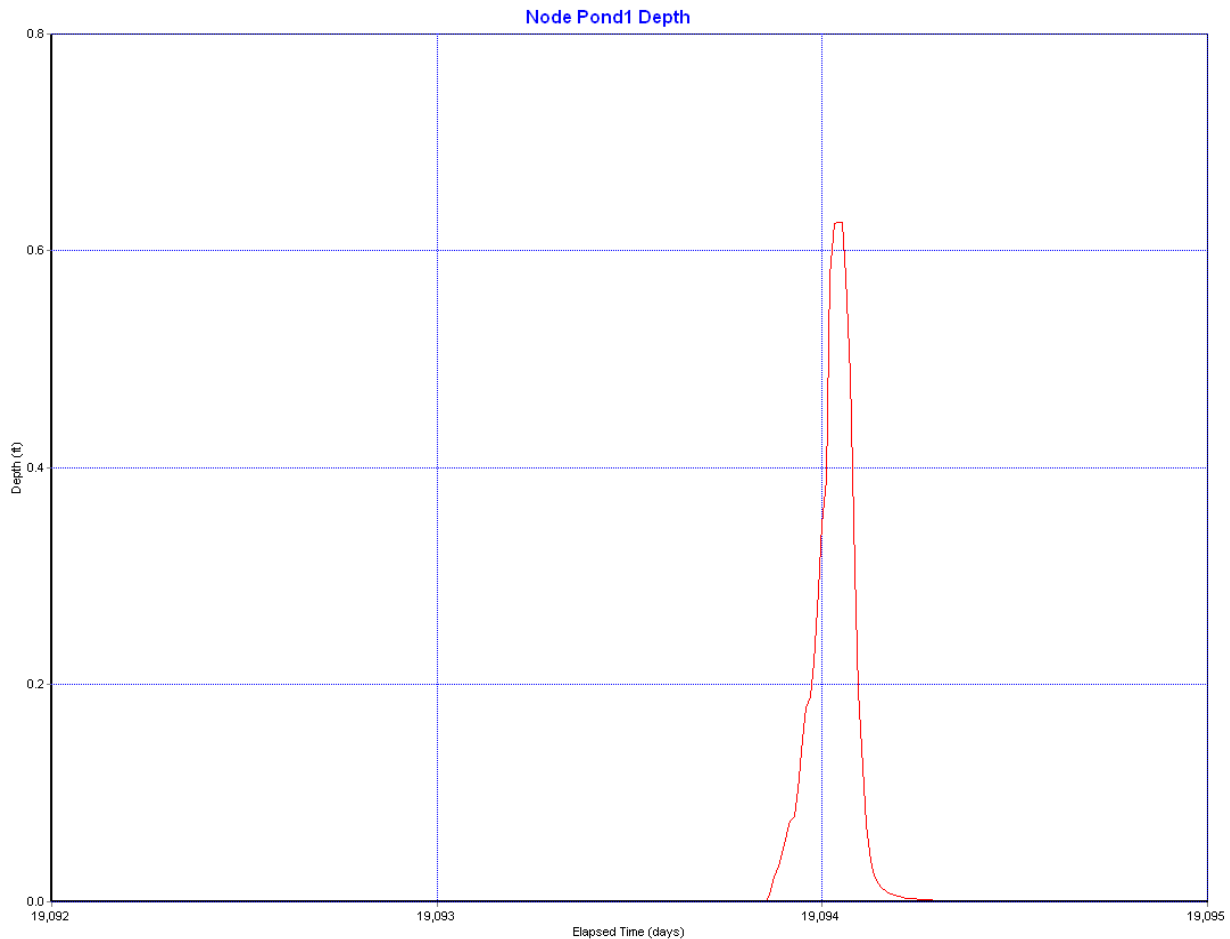
Table 5 –Pass or Fail Criteria

Drawdown Time of Bio-retention Surface Ponding

The drawdown time for hydromodification flow control facilities was calculated by assuming a starting water surface elevation coincident with the peak operating level in the bio-retention facility such as the elevation at the weir or the emergency spillway overflow. In continuous modeling, hundreds of hydrographs were created based on the rain data time series. Therefore, the drawdown time should be analyzed statistically. The statistical query is utilized to evaluate the percentage of exceedance frequency of a certain allowable depth of the ponding on a daily basis. The “Daily” option was chosen for the event period because the drawdown time for water quality purposes is 96 hours maximum.

A time series plot was created from the SWMM program by using the statistic values of the exceedance frequency and the dates when they occur to evaluate the pond draining time. The depth at the highest peak flow (occurs at the 58 year storm event), the designated water quality depth and the most frequent depth (typically > 75% exceedance frequency) were chosen to evaluate at extreme conditions or if the daily duration is greater than 24 hours. The daily duration here refers to the “time to peak” on the specific hydrograph.

Figure – 10. Daily depth versus Exceedance Frequency to evaluate drawdown time



The result for all the three criteria is tabularized as follows:

EXCEEDANCE FREQUENCY	PONDING DEPTH (FT)	DRAWDOWN TIME (DAYS)	MAX. ALLOWABLE DRAWDOWN TIME (DAYS)	PERMIT COMPLIANCE MET
0%	0.62	0.3	4	YES
50%	0.230	0.3	4	YES
75%	0.080	0.3	4	YES
AVERAGE		0.3	4	YES

Table 8 – Drawdown time based on Exceedance frequency

Conclusion: From the above Table 8, the drawdown time for this Hydromodification bio-retention is released no longer than 4 days (96 hours), therefore the bio-retention surface storage will function as an effective LID control and mitigate the potential vector breeding issues.

SWMM PRE-DEV			SWMM POST-DEV			PERMIT COMPLIANCE MET
Return Period (years)	Exceedance Frequency (percent)	Event Peak (CFS)	MITIGATED (CFS)	POST/ PRE (%)	PASS OR FAIL	
58.0	0.17	0.078	0.083	106	PASS	YES
29.0	0.33	0.072	0.076	106	PASS	YES
19.3	0.50	0.071	0.072	101	PASS	YES
14.5	0.66	0.067	0.070	104	PASS	YES
11.6	0.83	0.065	0.069	106	PASS	YES
9.7	0.99	0.063	0.066	105	PASS	YES
8.3	1.16	0.054	0.057	106	PASS	YES
7.3	1.32	0.050	0.053	106	PASS	YES
6.4	1.49	0.049	0.052	106	PASS	YES
5.8	1.65	0.049	0.052	106	PASS	YES
5.3	1.82	0.049	0.050	102	PASS	YES
4.8	1.98	0.047	0.049	104	PASS	YES
4.5	2.15	0.047	0.048	102	PASS	YES
4.1	2.31	0.046	0.048	104	PASS	YES
3.9	2.48	0.046	0.048	104	PASS	YES
3.6	2.64	0.045	0.048	107	PASS	YES
3.4	2.81	0.045	0.045	100	PASS	YES
3.2	2.97	0.044	0.045	102	PASS	YES
3.1	3.14	0.044	0.045	102	PASS	YES
2.9	3.30	0.044	0.044	100	PASS	YES
2.8	3.47	0.043	0.044	102	PASS	YES
2.6	3.63	0.042	0.043	102	PASS	YES
2.5	3.80	0.041	0.042	102	PASS	YES
2.4	3.96	0.041	0.041	100	PASS	YES
2.3	4.13	0.040	0.041	103	PASS	YES
2.2	4.29	0.039	0.041	105	PASS	YES
2.2	4.46	0.039	0.041	105	PASS	YES
2.1	4.62	0.039	0.041	105	PASS	YES
2.0	4.79	0.039	0.040	103	PASS	YES
1.9	4.95	0.039	0.038	97	PASS	YES
1.9	5.12	0.039	0.038	97	PASS	YES
1.8	5.28	0.039	0.038	97	PASS	YES
1.8	5.45	0.038	0.037	97	PASS	YES
1.7	5.61	0.038	0.036	95	PASS	YES
1.7	5.78	0.037	0.035	95	PASS	YES
1.6	5.94	0.036	0.035	97	PASS	YES
1.6	6.11	0.036	0.035	97	PASS	YES
1.5	6.27	0.034	0.034	100	PASS	YES
1.5	6.44	0.034	0.034	100	PASS	YES
1.5	6.60	0.034	0.034	100	PASS	YES
1.4	6.77	0.034	0.034	100	PASS	YES
1.4	6.93	0.033	0.034	103	PASS	YES
1.4	7.10	0.033	0.034	103	PASS	YES

Q10

Q2

1.3	7.26	0.032	0.033	103	PASS	YES
1.3	7.43	0.032	0.033	103	PASS	YES
1.3	7.59	0.032	0.031	97	PASS	YES
1.2	7.76	0.032	0.030	94	PASS	YES
1.2	7.92	0.032	0.030	94	PASS	YES
1.2	8.09	0.032	0.030	94	PASS	YES
1.2	8.25	0.032	0.030	94	PASS	YES
1.1	8.42	0.032	0.030	94	PASS	YES
1.1	8.58	0.031	0.028	90	PASS	YES
1.1	8.75	0.031	0.028	90	PASS	YES
1.1	8.91	0.031	0.028	90	PASS	YES
1.1	9.08	0.030	0.028	93	PASS	YES
1.0	9.24	0.030	0.027	90	PASS	YES
1.0	9.41	0.030	0.027	90	PASS	YES
1.0	9.57	0.030	0.027	90	PASS	YES
1.0	9.74	0.030	0.027	90	PASS	YES
1.0	9.90	0.029	0.026	90	PASS	YES
1.0	10.07	0.029	0.026	90	PASS	YES
0.9	10.23	0.029	0.025	86	PASS	YES
0.9	10.40	0.028	0.025	89	PASS	YES
0.9	10.56	0.028	0.025	89	PASS	YES
0.9	10.73	0.026	0.024	92	PASS	YES
0.9	10.89	0.026	0.024	92	PASS	YES
0.9	11.06	0.026	0.024	92	PASS	YES
0.9	11.22	0.026	0.024	92	PASS	YES
0.8	11.39	0.026	0.023	88	PASS	YES
0.8	11.55	0.026	0.022	85	PASS	YES
0.8	11.72	0.026	0.022	85	PASS	YES
0.8	11.88	0.026	0.022	85	PASS	YES
0.8	12.05	0.026	0.022	85	PASS	YES
0.8	12.21	0.026	0.022	85	PASS	YES
0.8	12.38	0.026	0.022	85	PASS	YES
0.8	12.54	0.026	0.022	85	PASS	YES
0.8	12.71	0.025	0.022	88	PASS	YES
0.7	12.87	0.025	0.022	88	PASS	YES
0.7	13.04	0.025	0.022	88	PASS	YES
0.7	13.20	0.025	0.022	88	PASS	YES
0.7	13.37	0.025	0.022	88	PASS	YES
0.7	13.53	0.025	0.022	88	PASS	YES
0.7	13.70	0.025	0.022	88	PASS	YES
0.7	13.86	0.025	0.022	88	PASS	YES
0.7	14.03	0.025	0.022	88	PASS	YES
0.7	14.19	0.025	0.021	84	PASS	YES
0.7	14.36	0.025	0.021	84	PASS	YES
0.7	14.52	0.025	0.021	84	PASS	YES
0.7	14.69	0.025	0.021	84	PASS	YES
0.6	14.85	0.025	0.021	84	PASS	YES

0.6	15.02	0.025	0.021	84	PASS	YES
0.6	15.18	0.025	0.021	84	PASS	YES
0.6	15.35	0.025	0.021	84	PASS	YES
0.6	15.51	0.025	0.021	84	PASS	YES
0.6	15.68	0.025	0.021	84	PASS	YES
0.6	15.84	0.025	0.021	84	PASS	YES
0.6	16.01	0.024	0.021	88	PASS	YES
0.6	16.17	0.024	0.021	88	PASS	YES
0.6	16.34	0.024	0.021	88	PASS	YES
0.6	16.50	0.024	0.021	88	PASS	YES
0.6	16.67	0.024	0.021	88	PASS	YES
0.6	16.83	0.024	0.020	83	PASS	YES
0.6	17.00	0.024	0.020	83	PASS	YES
0.6	17.16	0.024	0.020	83	PASS	YES
0.6	17.33	0.024	0.020	83	PASS	YES
0.6	17.49	0.024	0.020	83	PASS	YES
0.5	17.66	0.024	0.020	83	PASS	YES
0.5	17.82	0.023	0.020	87	PASS	YES
0.5	17.99	0.023	0.020	87	PASS	YES
0.5	18.15	0.023	0.020	87	PASS	YES
0.5	18.32	0.023	0.020	87	PASS	YES
0.5	18.48	0.023	0.020	87	PASS	YES
0.5	18.65	0.023	0.020	87	PASS	YES
0.5	18.81	0.023	0.019	83	PASS	YES
0.5	18.98	0.023	0.019	83	PASS	YES
0.5	19.14	0.023	0.019	83	PASS	YES
0.5	19.31	0.023	0.019	83	PASS	YES
0.5	19.47	0.023	0.019	83	PASS	YES
0.5	19.64	0.022	0.019	86	PASS	YES
0.5	19.80	0.022	0.019	86	PASS	YES
0.5	19.97	0.022	0.019	86	PASS	YES
0.5	20.13	0.022	0.019	86	PASS	YES
0.5	20.30	0.022	0.019	86	PASS	YES
0.5	20.46	0.022	0.019	86	PASS	YES
0.5	20.63	0.022	0.019	86	PASS	YES
0.5	20.79	0.022	0.019	86	PASS	YES
0.5	20.96	0.021	0.019	90	PASS	YES
0.5	21.12	0.021	0.019	90	PASS	YES
0.5	21.29	0.021	0.019	90	PASS	YES
0.5	21.45	0.021	0.019	90	PASS	YES
0.4	21.62	0.020	0.018	90	PASS	YES
0.4	21.78	0.020	0.018	90	PASS	YES
0.4	21.95	0.020	0.018	90	PASS	YES
0.4	22.11	0.020	0.018	90	PASS	YES
0.4	22.28	0.020	0.018	90	PASS	YES
0.4	22.44	0.020	0.018	90	PASS	YES
0.4	22.61	0.020	0.018	90	PASS	YES

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0.4	22.77	0.020	0.018	90	PASS	YES
0.4	22.94	0.020	0.018	90	PASS	YES
0.4	23.10	0.020	0.018	90	PASS	YES
0.4	23.27	0.020	0.018	90	PASS	YES
0.4	23.43	0.020	0.017	85	PASS	YES
0.4	23.60	0.020	0.017	85	PASS	YES
0.4	23.76	0.020	0.017	85	PASS	YES
0.4	23.93	0.020	0.017	85	PASS	YES
0.4	24.09	0.020	0.017	85	PASS	YES
0.4	24.26	0.019	0.017	89	PASS	YES
0.4	24.42	0.019	0.017	89	PASS	YES
0.4	24.59	0.019	0.017	89	PASS	YES
0.4	24.75	0.019	0.017	89	PASS	YES
0.4	24.92	0.019	0.017	89	PASS	YES
0.4	25.08	0.019	0.017	89	PASS	YES
0.4	25.25	0.019	0.016	84	PASS	YES
0.4	25.41	0.019	0.016	84	PASS	YES
0.4	25.58	0.019	0.016	84	PASS	YES
0.4	25.74	0.019	0.016	84	PASS	YES
0.4	25.91	0.019	0.015	79	PASS	YES
0.4	26.07	0.019	0.015	79	PASS	YES
0.4	26.24	0.019	0.015	79	PASS	YES
0.4	26.40	0.019	0.015	79	PASS	YES
0.4	26.57	0.019	0.015	79	PASS	YES
0.4	26.73	0.019	0.015	79	PASS	YES
0.4	26.90	0.019	0.015	79	PASS	YES
0.4	27.06	0.019	0.015	79	PASS	YES
0.4	27.23	0.019	0.015	79	PASS	YES
0.4	27.39	0.019	0.015	79	PASS	YES
0.4	27.56	0.019	0.015	79	PASS	YES
0.4	27.72	0.019	0.015	79	PASS	YES
0.3	27.89	0.018	0.015	83	PASS	YES
0.3	28.05	0.018	0.015	83	PASS	YES
0.3	28.22	0.018	0.015	83	PASS	YES
0.3	28.38	0.018	0.014	78	PASS	YES
0.3	28.55	0.018	0.014	78	PASS	YES
0.3	28.71	0.018	0.014	78	PASS	YES
0.3	28.88	0.018	0.014	78	PASS	YES
0.3	29.04	0.018	0.014	78	PASS	YES
0.3	29.21	0.018	0.014	78	PASS	YES
0.3	29.37	0.018	0.014	78	PASS	YES
0.3	29.54	0.018	0.013	72	PASS	YES
0.3	29.70	0.018	0.013	72	PASS	YES
0.3	29.87	0.018	0.013	72	PASS	YES
0.3	30.03	0.018	0.013	72	PASS	YES
0.3	30.20	0.018	0.013	72	PASS	YES
0.3	30.36	0.018	0.013	72	PASS	YES

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0.3	30.53	0.018	0.013	72	PASS	YES
0.3	30.69	0.018	0.013	72	PASS	YES
0.3	30.86	0.018	0.013	72	PASS	YES
0.3	31.02	0.018	0.013	72	PASS	YES
0.3	31.19	0.018	0.013	72	PASS	YES
0.3	31.35	0.018	0.013	72	PASS	YES
0.3	31.52	0.018	0.013	72	PASS	YES
0.3	31.68	0.018	0.013	72	PASS	YES
0.3	31.85	0.018	0.013	72	PASS	YES
0.3	32.01	0.018	0.013	72	PASS	YES
0.3	32.18	0.017	0.013	76	PASS	YES
0.3	32.34	0.017	0.013	76	PASS	YES
0.3	32.51	0.017	0.013	76	PASS	YES
0.3	32.67	0.017	0.013	76	PASS	YES
0.3	32.84	0.017	0.013	76	PASS	YES
0.3	33.00	0.017	0.013	76	PASS	YES
0.3	33.17	0.017	0.013	76	PASS	YES
0.3	33.33	0.017	0.013	76	PASS	YES
0.3	33.50	0.017	0.013	76	PASS	YES
0.3	33.66	0.017	0.013	76	PASS	YES
0.3	33.83	0.017	0.012	71	PASS	YES
0.3	33.99	0.017	0.012	71	PASS	YES
0.3	34.16	0.017	0.012	71	PASS	YES
0.3	34.32	0.017	0.012	71	PASS	YES
0.3	34.49	0.017	0.012	71	PASS	YES
0.3	34.65	0.017	0.012	71	PASS	YES
0.3	34.82	0.016	0.012	75	PASS	YES
0.3	34.98	0.016	0.012	75	PASS	YES
0.3	35.15	0.016	0.012	75	PASS	YES
0.3	35.31	0.016	0.012	75	PASS	YES
0.3	35.48	0.016	0.012	75	PASS	YES
0.3	35.64	0.016	0.012	75	PASS	YES
0.3	35.81	0.016	0.012	75	PASS	YES
0.3	35.97	0.016	0.012	75	PASS	YES
0.3	36.14	0.016	0.012	75	PASS	YES
0.3	36.30	0.016	0.012	75	PASS	YES
0.3	36.47	0.016	0.012	75	PASS	YES
0.3	36.63	0.016	0.012	75	PASS	YES
0.3	36.80	0.016	0.012	75	PASS	YES
0.3	36.96	0.016	0.012	75	PASS	YES
0.3	37.13	0.016	0.012	75	PASS	YES
0.3	37.29	0.016	0.012	75	PASS	YES
0.3	37.46	0.016	0.012	75	PASS	YES
0.3	37.62	0.016	0.012	75	PASS	YES
0.3	37.79	0.016	0.012	75	PASS	YES
0.3	37.95	0.016	0.012	75	PASS	YES
0.3	38.12	0.015	0.012	80	PASS	YES

0.3	38.28	0.015	0.011	73	PASS	YES
0.3	38.45	0.015	0.011	73	PASS	YES
0.3	38.61	0.015	0.011	73	PASS	YES
0.3	38.94	0.015	0.011	73	PASS	YES
0.3	38.94	0.015	0.011	73	PASS	YES
0.2	39.11	0.015	0.011	73	PASS	YES
0.2	39.27	0.015	0.010	67	PASS	YES
0.2	39.44	0.015	0.010	67	PASS	YES
0.2	39.60	0.015	0.010	67	PASS	YES
0.2	39.77	0.015	0.010	67	PASS	YES
0.2	39.93	0.015	0.009	60	PASS	YES
0.2	40.10	0.015	0.009	60	PASS	YES
0.2	40.26	0.014	0.009	64	PASS	YES
0.2	40.43	0.014	0.009	64	PASS	YES
0.2	40.59	0.014	0.009	64	PASS	YES
0.2	40.76	0.014	0.009	64	PASS	YES
0.2	40.92	0.014	0.009	64	PASS	YES
0.2	41.09	0.014	0.009	64	PASS	YES
0.2	41.25	0.014	0.009	64	PASS	YES
0.2	41.42	0.014	0.009	64	PASS	YES
0.2	41.58	0.014	0.009	64	PASS	YES
0.2	41.75	0.014	0.009	64	PASS	YES
0.2	41.91	0.014	0.009	64	PASS	YES
0.2	42.08	0.014	0.009	64	PASS	YES
0.2	42.24	0.014	0.009	64	PASS	YES
0.2	42.41	0.014	0.009	64	PASS	YES
0.2	42.57	0.014	0.009	64	PASS	YES
0.2	42.74	0.014	0.009	64	PASS	YES
0.2	43.07	0.014	0.009	64	PASS	YES
0.2	43.07	0.014	0.009	64	PASS	YES
0.2	43.23	0.014	0.009	64	PASS	YES
0.2	43.40	0.014	0.009	64	PASS	YES
0.2	43.56	0.013	0.009	69	PASS	YES
0.2	43.73	0.013	0.009	69	PASS	YES
0.2	43.89	0.013	0.009	69	PASS	YES
0.2	44.06	0.013	0.009	69	PASS	YES
0.2	44.22	0.013	0.009	69	PASS	YES
0.2	44.39	0.013	0.009	69	PASS	YES
0.2	44.55	0.013	0.009	69	PASS	YES
0.2	44.72	0.013	0.009	69	PASS	YES
0.2	44.88	0.013	0.009	69	PASS	YES
0.2	45.05	0.013	0.009	69	PASS	YES
0.2	45.21	0.013	0.009	69	PASS	YES
0.2	45.38	0.013	0.009	69	PASS	YES
0.2	45.54	0.013	0.009	69	PASS	YES
0.2	45.71	0.013	0.009	69	PASS	YES
0.2	45.87	0.013	0.009	69	PASS	YES

0.1Q2

0.2	46.04	0.012	0.009	75	PASS	YES
0.2	46.20	0.012	0.009	75	PASS	YES
0.2	46.37	0.012	0.009	75	PASS	YES
0.2	46.53	0.012	0.009	75	PASS	YES
0.2	46.70	0.012	0.009	75	PASS	YES
0.2	46.86	0.012	0.009	75	PASS	YES
0.2	47.03	0.012	0.009	75	PASS	YES
0.2	47.19	0.012	0.009	75	PASS	YES
0.2	47.36	0.012	0.009	75	PASS	YES
0.2	47.52	0.012	0.009	75	PASS	YES
0.2	47.69	0.012	0.009	75	PASS	YES
0.2	47.85	0.012	0.009	75	PASS	YES
0.2	48.02	0.012	0.009	75	PASS	YES
0.2	48.18	0.012	0.009	75	PASS	YES
0.2	48.35	0.012	0.009	75	PASS	YES
0.2	48.51	0.012	0.009	75	PASS	YES
0.2	48.68	0.012	0.009	75	PASS	YES
0.2	48.84	0.012	0.009	75	PASS	YES
0.2	49.01	0.012	0.009	75	PASS	YES
0.2	49.17	0.012	0.009	75	PASS	YES
0.2	49.34	0.012	0.009	75	PASS	YES
0.2	49.50	0.012	0.009	75	PASS	YES
0.2	49.67	0.012	0.009	75	PASS	YES
0.2	49.83	0.012	0.009	75	PASS	YES
0.2	50.00	0.012	0.009	75	PASS	YES
0.2	50.17	0.012	0.009	75	PASS	YES
0.2	50.33	0.012	0.009	75	PASS	YES
0.2	50.50	0.012	0.009	75	PASS	YES
0.2	50.66	0.012	0.009	75	PASS	YES
0.2	50.83	0.012	0.009	75	PASS	YES
0.2	50.99	0.012	0.009	75	PASS	YES
0.2	51.16	0.012	0.009	75	PASS	YES
0.2	51.32	0.012	0.009	75	PASS	YES
0.2	51.49	0.012	0.009	75	PASS	YES
0.2	51.65	0.012	0.009	75	PASS	YES
0.2	51.82	0.012	0.009	75	PASS	YES
0.2	51.98	0.012	0.009	75	PASS	YES
0.2	52.15	0.012	0.009	75	PASS	YES
0.2	52.31	0.012	0.009	75	PASS	YES
0.2	52.48	0.012	0.009	75	PASS	YES
0.2	52.64	0.012	0.009	75	PASS	YES
0.2	52.81	0.012	0.009	75	PASS	YES
0.2	52.97	0.012	0.009	75	PASS	YES
0.2	53.14	0.012	0.009	75	PASS	YES
0.2	53.30	0.012	0.009	75	PASS	YES
0.2	53.47	0.012	0.009	75	PASS	YES
0.2	53.63	0.012	0.009	75	PASS	YES

0.2	53.80	0.012	0.009	75	PASS	YES
0.2	53.96	0.012	0.009	75	PASS	YES
0.2	54.13	0.012	0.009	75	PASS	YES
0.2	54.29	0.012	0.009	75	PASS	YES
0.2	54.46	0.012	0.009	75	PASS	YES
0.2	54.62	0.012	0.009	75	PASS	YES
0.2	54.79	0.012	0.009	75	PASS	YES
0.2	54.95	0.012	0.009	75	PASS	YES
0.2	55.12	0.012	0.009	75	PASS	YES
0.2	55.28	0.012	0.009	75	PASS	YES
0.2	55.45	0.012	0.009	75	PASS	YES
0.2	55.61	0.012	0.009	75	PASS	YES
0.2	55.78	0.011	0.009	82	PASS	YES
0.2	55.94	0.011	0.009	82	PASS	YES
0.2	56.11	0.011	0.008	73	PASS	YES
0.2	56.27	0.011	0.008	73	PASS	YES
0.2	56.44	0.011	0.008	73	PASS	YES
0.2	56.60	0.011	0.008	73	PASS	YES
0.2	56.77	0.011	0.008	73	PASS	YES
0.2	56.93	0.011	0.008	73	PASS	YES
0.2	57.10	0.011	0.008	73	PASS	YES
0.2	57.26	0.011	0.008	73	PASS	YES
0.2	57.43	0.011	0.008	73	PASS	YES
0.2	57.59	0.011	0.008	73	PASS	YES
0.2	57.76	0.011	0.008	73	PASS	YES
0.2	57.92	0.011	0.008	73	PASS	YES
0.2	58.09	0.011	0.008	73	PASS	YES
0.2	58.25	0.011	0.008	73	PASS	YES
0.2	58.42	0.011	0.008	73	PASS	YES
0.2	58.58	0.011	0.008	73	PASS	YES
0.2	58.75	0.011	0.008	73	PASS	YES
0.2	58.91	0.011	0.008	73	PASS	YES
0.2	59.08	0.011	0.008	73	PASS	YES
0.2	59.24	0.011	0.008	73	PASS	YES
0.2	59.41	0.011	0.008	73	PASS	YES
0.2	59.57	0.011	0.008	73	PASS	YES
0.2	59.74	0.011	0.008	73	PASS	YES
0.2	59.90	0.011	0.008	73	PASS	YES
0.2	60.07	0.011	0.008	73	PASS	YES
0.2	60.23	0.011	0.008	73	PASS	YES
0.2	60.40	0.011	0.008	73	PASS	YES
0.2	60.56	0.011	0.008	73	PASS	YES
0.2	60.73	0.011	0.008	73	PASS	YES
0.2	60.89	0.011	0.008	73	PASS	YES
0.2	61.06	0.011	0.008	73	PASS	YES
0.2	61.22	0.011	0.008	73	PASS	YES
0.2	61.39	0.010	0.008	80	PASS	YES

0.2	61.55	0.010	0.008	80	PASS	YES
0.2	61.72	0.010	0.008	80	PASS	YES
0.2	61.88	0.010	0.008	80	PASS	YES
0.2	62.05	0.010	0.008	80	PASS	YES
0.2	62.21	0.010	0.008	80	PASS	YES
0.2	62.38	0.010	0.008	80	PASS	YES
0.2	62.54	0.010	0.008	80	PASS	YES
0.2	62.71	0.010	0.008	80	PASS	YES
0.2	62.87	0.010	0.007	70	PASS	YES
0.2	63.04	0.010	0.007	70	PASS	YES
0.2	63.20	0.010	0.007	70	PASS	YES
0.2	63.37	0.010	0.007	70	PASS	YES
0.2	63.53	0.010	0.007	70	PASS	YES
0.2	63.70	0.010	0.007	70	PASS	YES
0.2	63.86	0.010	0.007	70	PASS	YES
0.2	64.03	0.010	0.007	70	PASS	YES
0.2	64.19	0.010	0.007	70	PASS	YES
0.2	64.36	0.010	0.007	70	PASS	YES
0.2	64.52	0.010	0.007	70	PASS	YES
0.2	64.69	0.010	0.007	70	PASS	YES
0.2	64.85	0.010	0.007	70	PASS	YES
0.2	65.02	0.010	0.007	70	PASS	YES
0.2	65.18	0.010	0.007	70	PASS	YES
0.2	65.35	0.010	0.007	70	PASS	YES
0.2	65.51	0.010	0.007	70	PASS	YES
0.2	65.68	0.010	0.007	70	PASS	YES
0.2	65.84	0.010	0.007	70	PASS	YES
0.1	66.01	0.010	0.007	70	PASS	YES
0.1	66.17	0.010	0.007	70	PASS	YES
0.1	66.34	0.010	0.007	70	PASS	YES
0.1	66.50	0.009	0.007	78	PASS	YES
0.1	66.67	0.009	0.007	78	PASS	YES
0.1	66.83	0.009	0.007	78	PASS	YES
0.1	67.00	0.009	0.007	78	PASS	YES
0.1	67.16	0.009	0.007	78	PASS	YES
0.1	67.33	0.009	0.007	78	PASS	YES
0.1	67.49	0.009	0.007	78	PASS	YES
0.1	67.66	0.009	0.007	78	PASS	YES
0.1	67.82	0.009	0.007	78	PASS	YES
0.1	67.99	0.009	0.007	78	PASS	YES
0.1	68.15	0.009	0.007	78	PASS	YES
0.1	68.32	0.009	0.007	78	PASS	YES
0.1	68.48	0.009	0.007	78	PASS	YES
0.1	68.65	0.009	0.007	78	PASS	YES
0.1	68.81	0.009	0.007	78	PASS	YES
0.1	68.98	0.009	0.007	78	PASS	YES
0.1	69.14	0.009	0.007	78	PASS	YES

0.1	69.31	0.009	0.007	78	PASS	YES
0.1	69.47	0.009	0.007	78	PASS	YES
0.1	69.64	0.009	0.006	67	PASS	YES
0.1	69.80	0.009	0.006	67	PASS	YES
0.1	69.97	0.009	0.006	67	PASS	YES
0.1	70.13	0.009	0.006	67	PASS	YES
0.1	70.30	0.009	0.006	67	PASS	YES
0.1	70.46	0.009	0.006	67	PASS	YES
0.1	70.63	0.009	0.006	67	PASS	YES
0.1	70.79	0.009	0.006	67	PASS	YES
0.1	70.96	0.009	0.006	67	PASS	YES
0.1	71.12	0.009	0.006	67	PASS	YES
0.1	71.29	0.009	0.006	67	PASS	YES
0.1	71.45	0.009	0.006	67	PASS	YES
0.1	71.62	0.009	0.006	67	PASS	YES
0.1	71.78	0.009	0.006	67	PASS	YES
0.1	71.95	0.009	0.006	67	PASS	YES
0.1	72.11	0.008	0.006	75	PASS	YES
0.1	72.28	0.008	0.006	75	PASS	YES
0.1	72.44	0.008	0.006	75	PASS	YES
0.1	72.61	0.008	0.006	75	PASS	YES
0.1	72.77	0.008	0.006	75	PASS	YES
0.1	72.94	0.008	0.006	75	PASS	YES
0.1	73.10	0.008	0.006	75	PASS	YES
0.1	73.27	0.008	0.006	75	PASS	YES
0.1	73.43	0.008	0.006	75	PASS	YES
0.1	73.60	0.008	0.006	75	PASS	YES
0.1	73.76	0.008	0.006	75	PASS	YES
0.1	73.93	0.008	0.006	75	PASS	YES
0.1	74.09	0.008	0.006	75	PASS	YES
0.1	74.26	0.008	0.006	75	PASS	YES
0.1	74.42	0.008	0.006	75	PASS	YES
0.1	74.59	0.008	0.006	75	PASS	YES
0.1	74.75	0.008	0.006	75	PASS	YES
0.1	74.92	0.007	0.006	86	PASS	YES
0.1	75.08	0.007	0.006	86	PASS	YES
0.1	75.25	0.007	0.006	86	PASS	YES
0.1	75.41	0.007	0.006	86	PASS	YES
0.1	75.58	0.007	0.006	86	PASS	YES
0.1	75.74	0.007	0.006	86	PASS	YES
0.1	75.91	0.007	0.006	86	PASS	YES
0.1	76.07	0.007	0.006	86		

APPENDIX 6

WATER SURFACE CALCULATION WITH HECRAS

HEC-RAS Version 4.1.0 Jan 2010
U.S. Army Corps of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

```

X      X  XXXXXX      XXXX      XXXX      XX      XXXX
X      X  X          X  X      X  X      X  X      X
X      X  X          X          X  X      X  X      X
XXXXXXXX XXXX      X      XXX XXXX      XXXXXX      XXXX
X      X  X          X          X  X      X  X      X
X      X  X          X  X      X  X      X  X      X
X      X  XXXXXX      XXXX      X  X      X  X      XXXXX

```

PROJECT DATA

Project Title: PRE-DEVELOPMENT
Project File : PRE-DEVELOPMENT.prj
Run Date and Time: 2/19/2013 9:43:12 AM

Project in English units

PLAN DATA

Plan Title: Plan 07

Plan File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.p07

Geometry Title: geo-post-dev

Geometry File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.g02

Flow Title : pre-dev flow

Flow File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.f01

Plan Summary Information:

Number of:	Cross Sections =	18	Multiple Openings =	0
	Culverts =	1	Inline Structures =	0
	Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance =	0.01
Critical depth calculation tolerance =	0.01
Maximum number of iterations =	20
Maximum difference tolerance =	0.3
Flow tolerance factor =	0.001

Computation Options

Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: pre-dev flow

Flow File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.f01

Flow Data (cfs)

River	Reach	RS	100 yr
Agua Hedionda	SM Highlands	18	362.1
Agua Hedionda	SM Highlands	13	674.7
Agua Hedionda	SM Highlands	6	924

Boundary Conditions

River	Reach	Profile	Upstream
Downstream			
Agua Hedionda	SM Highlands	100 yr	
Critical			

GEOMETRY DATA

Geometry Title: geo-post-dev

Geometry File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.g02

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 18

INPUT

Description:

Station	Elevation	Data	num=	16						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	734.4	42.56	732.64	87	732	109.57	729.92	146.3	729	
212.31	715	265.43	704.95	291.31	703	367.1	705.93	368.78	705.24	
375.71	709	388.24	710	398.89	715	489.05	716	517.58	729	
600	749.7									

Manning's n	Values	num=	3							
Sta	n Val	Sta	n Val	Sta	n Val					
0	.03	146.3	.035	398.89	.03					

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.	
	146.3	398.89		251	201	149.5		.1	.3	

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	705.30	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.47	Wt. n-Val.		0.035	
W.S. Elev (ft)	704.83	Reach Len. (ft)	251.00	201.00	149.50
Crit W.S. (ft)	704.83	Flow Area (sq ft)		65.81	
E.G. Slope (ft/ft)	0.018894	Area (sq ft)		65.81	
Q Total (cfs)	362.10	Flow (cfs)		362.10	
Top Width (ft)	71.77	Top Width (ft)		71.77	
Vel Total (ft/s)	5.50	Avg. Vel. (ft/s)		5.50	
Max Chl Dpth (ft)	1.83	Hydr. Depth (ft)		0.92	
Conv. Total (cfs)	2634.3	Conv. (cfs)		2634.3	
Length Wtd. (ft)	201.00	Wetted Per. (ft)		71.88	
Min Ch El (ft)	703.00	Shear (lb/sq ft)		1.08	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	3.75	Cum Volume (acre-ft)		21.97	
C & E Loss (ft)	0.00	Cum SA (acres)		8.40	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 17

INPUT

Description:

Station	Elevation	Data	num=	14						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	714.61	38.49	710.59	147.06	709.2	192.29	706.35	204.23	706.36	
246.05	700	272.27	696	297.8	693.33	315.3	695.57	338.11	695.98	
414.27	702.97	437.9	711.01	522.35	713.98	600.01	732.47			

Manning's n	Values	num=	3							
Sta	n Val	Sta	n Val	Sta	n Val					
0	.03	204.23	.035	414.27	.03					

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.	
	204.23	414.27		170	200	230		.1	.3	

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	696.46	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.51	Wt. n-Val.		0.035	
W.S. Elev (ft)	695.96	Reach Len. (ft)	170.00	200.00	230.00
Crit W.S. (ft)	695.96	Flow Area (sq ft)		63.44	
E.G. Slope (ft/ft)	0.018420	Area (sq ft)		63.44	
Q Total (cfs)	362.10	Flow (cfs)		362.10	
Top Width (ft)	64.05	Top Width (ft)		64.05	
Vel Total (ft/s)	5.71	Avg. Vel. (ft/s)		5.71	
Max Chl Dpth (ft)	2.63	Hydr. Depth (ft)		0.99	
Conv. Total (cfs)	2668.0	Conv. (cfs)		2668.0	
Length Wtd. (ft)	200.00	Wetted Per. (ft)		64.34	
Min Ch El (ft)	693.33	Shear (lb/sq ft)		1.13	
Alpha	1.00	Stream Power (lb/ft s)	600.01	0.00	0.00
Frctn Loss (ft)	3.60	Cum Volume (acre-ft)		21.67	
C & E Loss (ft)	0.01	Cum SA (acres)		8.08	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 16

INPUT

Description:

Station Elevation Data		num= 11									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	720.8	22.87	715	85.69	704.95	142.68	699.56	257.7	690.78		
299.85	685.21	332.6	686.18	371.62	692	425.35	693.86	540.3	712.74		
600	718.48										

Manning's n Values		num= 3					
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	142.68	.035	425.35	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	142.68	425.35		201	201	.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	687.62	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.58	Wt. n-Val.		0.035	
W.S. Elev (ft)	687.04	Reach Len. (ft)	201.00	201.00	201.00
Crit W.S. (ft)	687.04	Flow Area (sq ft)		59.32	
E.G. Slope (ft/ft)	0.017607	Area (sq ft)		59.32	
Q Total (cfs)	362.10	Flow (cfs)		362.10	
Top Width (ft)	52.40	Top Width (ft)		52.40	
Vel Total (ft/s)	6.10	Avg. Vel. (ft/s)		6.10	
Max Chl Dpth (ft)	1.83	Hydr. Depth (ft)		1.13	
Conv. Total (cfs)	2728.9	Conv. (cfs)		2728.9	
Length Wtd. (ft)	201.00	Wetted Per. (ft)		52.60	
Min Ch El (ft)	685.21	Shear (lb/sq ft)		1.24	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	3.22	Cum Volume (acre-ft)		21.39	
C & E Loss (ft)	0.01	Cum SA (acres)		7.81	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 15

INPUT

Description:

Station	Elevation	Data	num=	11							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	719.45	144.68	698.46	194.72	689.85	292.93	676	305.15	675.72		
360.63	680.2	392.5	689	423.4	687.33	477.9	691.35	534.95	692.56		
600	696.86										

Manning's n	Values	num=	3								
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	194.72	.035	392.5	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	194.72	392.5		164	203		.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	678.33	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.53	Wt. n-Val.		0.035	
W.S. Elev (ft)	677.80	Reach Len. (ft)	164.00	203.00	238.00
Crit W.S. (ft)	677.73	Flow Area (sq ft)		61.94	
E.G. Slope (ft/ft)	0.014611	Area (sq ft)		61.94	
Q Total (cfs)	362.10	Flow (cfs)		362.10	
Top Width (ft)	50.72	Top Width (ft)		50.72	
Vel Total (ft/s)	5.85	Avg. Vel. (ft/s)		5.85	
Max Chl Dpth (ft)	2.08	Hydr. Depth (ft)		1.22	
Conv. Total (cfs)	2995.6	Conv. (cfs)		2995.6	
Length Wtd. (ft)	203.00	Wetted Per. (ft)		50.94	
Min Ch El (ft)	675.72	Shear (lb/sq ft)		1.11	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	3.35	Cum Volume (acre-ft)		21.11	
C & E Loss (ft)	0.02	Cum SA (acres)		7.58	

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 14

INPUT

Description:

Station	Elevation	Data	num=	12							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	700.97	46.34	698.99	123.59	692.64	229.32	680	313.98	673.84		
356.38	672.9	380.56	675	403.47	680	437.9	695	476.6	702		
547.73	716	600	724.22								

Manning's n	Values	num=	3								
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	229.32	.035	437.9	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	229.32	437.9		336	221		.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	674.97	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.48	Wt. n-Val.		0.035	
W.S. Elev (ft)	674.49	Reach Len. (ft)	336.00	221.00	89.00
Crit W.S. (ft)	674.49	Flow Area (sq ft)		65.22	
E.G. Slope (ft/ft)	0.018734	Area (sq ft)		65.22	
Q Total (cfs)	362.10	Flow (cfs)		362.10	
Top Width (ft)	69.74	Top Width (ft)		69.74	
Vel Total (ft/s)	5.55	Avg. Vel. (ft/s)		5.55	
Max Chl Dpth (ft)	1.59	Hydr. Depth (ft)		0.94	
Conv. Total (cfs)	2645.6	Conv. (cfs)		2645.6	

Length Wtd. (ft)	221.00	Wetted Per. (ft)		69.85
Min Ch El (ft)	672.90	Shear (lb/sq ft)		1.09
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00
Frctn Loss (ft)	4.18	Cum Volume (acre-ft)		20.81
C & E Loss (ft)	0.00	Cum SA (acres)		7.30

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth
for the water surface and continued on with the calculations.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than
0.7 or greater than 1.4.
This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross
section. This may indicate the
need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to
critical depth, the calculated
water surface came back below critical depth. This indicates that there is not a valid
subcritical answer. The program
defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 13

INPUT

Description:

Station	Elevation	Data	num=	8							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	709.87	63.6	705	122.95	689.01	200.96	670	290.39	668.56		
376.99	672	500.83	701.72	600	719.32						

Manning's n Values			num=	3
Sta	n Val	Sta	n Val	Sta
0	.03	122.95	.035	500.83

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	122.95	500.83		200	200	.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	670.72	Element		Left OB	Channel	Right OB
Vel Head (ft)	0.47	Wt. n-Val.			0.035	
W.S. Elev (ft)	670.24	Reach Len. (ft)	200.00	200.00	200.00	
Crit W.S. (ft)	670.24	Flow Area (sq ft)		122.03		
E.G. Slope (ft/ft)	0.019004	Area (sq ft)		122.03		
Q Total (cfs)	674.70	Flow (cfs)		674.70		
Top Width (ft)	132.83	Top Width (ft)		132.83		
Vel Total (ft/s)	5.53	Avg. Vel. (ft/s)		5.53		
Max Chl Dpth (ft)	1.68	Hydr. Depth (ft)		0.92		
Conv. Total (cfs)	4894.3	Conv. (cfs)		4894.3		
Length Wtd. (ft)	200.00	Wetted Per. (ft)		132.90		
Min Ch El (ft)	668.56	Shear (lb/sq ft)		1.09		
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00	
Frctn Loss (ft)	0.84	Cum Volume (acre-ft)		20.34		
C & E Loss (ft)	0.10	Cum SA (acres)		6.78		

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth
for the water surface and continued on with the calculations.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than
0.7 or greater than 1.4.
This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross
section. This may indicate the
need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to
critical depth, the calculated
water surface came back below critical depth. This indicates that there is not a valid
subcritical answer. The program
defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 12

INPUT

Description:

Station		Elevation Data		num=		11					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	707.64	39.3	700	88.81	686.43	153.24	674.83	203.44	670.05		
229.59	666	314.09	663.29	367.99	669.93	428.54	688.61	504.8	705.92		
600	715.97										

Manning's n Values

Sta		n Val		num=		3					
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	153.24	.035	367.99	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	153.24	367.99		200	200		.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	666.95	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.13	Wt. n-Val.		0.035	
W.S. Elev (ft)	666.83	Reach Len. (ft)	200.00	200.00	200.00
Crit W.S. (ft)	665.64	Flow Area (sq ft)		237.28	
E.G. Slope (ft/ft)	0.001785	Area (sq ft)		237.28	
Q Total (cfs)	674.70	Flow (cfs)		674.70	
Top Width (ft)	118.54	Top Width (ft)		118.54	
Vel Total (ft/s)	2.84	Avg. Vel. (ft/s)		2.84	
Max Chl Dpth (ft)	3.54	Hydr. Depth (ft)		2.00	
Conv. Total (cfs)	15970.9	Conv. (cfs)		15970.9	
Length Wtd. (ft)	200.00	Wetted Per. (ft)		118.87	
Min Ch El (ft)	663.29	Shear (lb/sq ft)		0.22	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	0.87	Cum Volume (acre-ft)		19.51	
C & E Loss (ft)	0.04	Cum SA (acres)		6.21	

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 11

INPUT

Description:

Station		Elevation Data		num=		11					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	707.64	86.22	687.22	164.31	674.29	204.06	670	229.59	666		
313.1	663.29	341.94	665	369.82	670.46	428.54	688.61	508.15	706.43		
600	715.97										

Manning's n Values

Sta		n Val		num=		3					
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	164.31	.04	369.82	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	164.31	369.82		223	202		.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	666.03	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.58	Wt. n-Val.		0.040	
W.S. Elev (ft)	665.46	Reach Len. (ft)	223.00	202.00	180.00
Crit W.S. (ft)	665.46	Flow Area (sq ft)		110.85	
E.G. Slope (ft/ft)	0.022816	Area (sq ft)		110.85	
Q Total (cfs)	674.70	Flow (cfs)		674.70	
Top Width (ft)	98.00	Top Width (ft)		98.00	
Vel Total (ft/s)	6.09	Avg. Vel. (ft/s)		6.09	
Max Chl Dpth (ft)	2.17	Hydr. Depth (ft)		1.13	
Conv. Total (cfs)	4466.8	Conv. (cfs)		4466.8	
Length Wtd. (ft)	202.00	Wetted Per. (ft)		98.13	
Min Ch El (ft)	663.29	Shear (lb/sq ft)		1.61	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	0.07	Cum Volume (acre-ft)		18.71	
C & E Loss (ft)	0.17	Cum SA (acres)		5.71	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.
Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 10

INPUT

Description:

Station Elevation Data			num= 9								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
7.61	699.57	33.88	691.15	109.68	675	156.53	668.82	229.75	656		
360.07	656	425.32	674.44	486.5	688.78	600	689				

Manning's n Values			num= 3								
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
7.61	.03	156.53	.04	425.32	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	156.53	425.32		138	206	267	.1 .3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	660.63	Element		Left OB	Channel	Right OB					
Vel Head (ft)	0.01	Wt. n-Val.			0.040						
W.S. Elev (ft)	660.62	Reach Len. (ft)	138.00		206.00	267.00					
Crit W.S. (ft)		Flow Area (sq ft)			699.99						
E.G. Slope (ft/ft)	0.000105	Area (sq ft)			699.99						
Q Total (cfs)	674.70	Flow (cfs)			674.70						
Top Width (ft)	173.01	Top Width (ft)			173.01						
Vel Total (ft/s)	0.96	Avg. Vel. (ft/s)			0.96						
Max Chl Dpth (ft)	4.62	Hydr. Depth (ft)			4.05						
Conv. Total (cfs)	65761.3	Conv. (cfs)			65761.3						
Length Wtd. (ft)	206.00	Wetted Per. (ft)			174.05						
Min Ch El (ft)	656.00	Shear (lb/sq ft)			0.03						
Alpha	1.00	Stream Power (lb/ft s)	600.00		0.00	0.00					
Frctn Loss (ft)	0.02	Cum Volume (acre-ft)			16.83						
C & E Loss (ft)	0.00	Cum SA (acres)			5.08						

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 9

INPUT

Description:

Station Elevation Data			num= 12								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	712.95	5.98	710	115.62	710	187.3	675	207.52	670		
240.74	656	392.94	656	414.44	665	459	675.27	487.2	679.95		
574.16	679.13	580.28	682								

Manning's n Values			num= 3								
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	187.3	.04	459	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	187.3	459		144	202	677	.1 .3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	660.61	Element		Left OB	Channel	Right OB					
Vel Head (ft)	0.01	Wt. n-Val.			0.040						
W.S. Elev (ft)	660.60	Reach Len. (ft)	144.00		202.00	677.00					
Crit W.S. (ft)		Flow Area (sq ft)			750.02						

E.G. Slope (ft/ft)	0.000085	Area (sq ft)	750.02
Q Total (cfs)	674.70	Flow (cfs)	674.70
Top Width (ft)	174.09	Top Width (ft)	174.09
Vel Total (ft/s)	0.90	Avg. Vel. (ft/s)	0.90
Max Chl Dpth (ft)	4.60	Hydr. Depth (ft)	4.31
Conv. Total (cfs)	73249.6	Conv. (cfs)	73249.6
Length Wtd. (ft)	202.00	Wetted Per. (ft)	175.94
Min Ch El (ft)	656.00	Shear (lb/sq ft)	0.02
Alpha	1.00	Stream Power (lb/ft s)	580.28
Frctn Loss (ft)	0.00	Cum Volume (acre-ft)	13.40
C & E Loss (ft)	0.00	Cum SA (acres)	4.26

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 8

INPUT

Description:

Station Elevation Data		num=	14								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	710	89.94	710	137.54	684.23	188.84	670.63	237.78	655.63		
345.23	646.36	394.69	655.76	429.46	656.43	451.45	663.15	482.96	662.26		
515.68	665.79	526.53	668.84	538.31	669.65	581.5	670.03				

Manning's n Values		num=	3				
Sta	n Val	Sta	n Val	Sta	n Val		
0	.03	188.84	.035	451.45	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	188.84	451.45		240	202	612	.3
							.5

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	660.60	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.00	Wt. n-Val.		0.035	
W.S. Elev (ft)	660.60	Reach Len. (ft)	240.00	202.00	612.00
Crit W.S. (ft)	649.66	Flow Area (sq ft)		1729.62	
E.G. Slope (ft/ft)	0.000006	Area (sq ft)		1729.62	
Q Total (cfs)	674.70	Flow (cfs)		674.70	
Top Width (ft)	221.55	Top Width (ft)		221.55	
Vel Total (ft/s)	0.39	Avg. Vel. (ft/s)		0.39	
Max Chl Dpth (ft)	14.24	Hydr. Depth (ft)		7.81	
Conv. Total (cfs)	286688.6	Conv. (cfs)		286688.6	
Length Wtd. (ft)	202.00	Wetted Per. (ft)		224.21	
Min Ch El (ft)	646.36	Shear (lb/sq ft)		0.00	
Alpha	1.00	Stream Power (lb/ft s)	581.50	0.00	0.00
Frctn Loss (ft)		Cum Volume (acre-ft)		7.65	
C & E Loss (ft)		Cum SA (acres)		3.34	

CULVERT

RIVER: Agua Hedionda
REACH: SM Highlands RS: 7.5

INPUT

Description:

Distance from Upstream XS = 90
Deck/Roadway Width = 88
Weir Coefficient = 2.6
Upstream Deck/Roadway Coordinates

num=		10									
Sta	Hi	Cord	Lo	Cord	Sta	Hi	Cord	Lo	Cord		
0	680		89.94	675	137.5	670					
189	669		238	667	310	663.82					
395	667		429.5	669	483	670					
600	675										

Upstream Bridge Cross Section Data

Station Elevation Data		num=	14								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	710	89.94	710	137.54	684.23	188.84	670.63	237.78	655.63		
345.23	646.36	394.69	655.76	429.46	656.43	451.45	663.15	482.96	662.26		

515.68 665.79 526.53 668.84 538.31 669.65 581.5 670.03

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .03 188.84 .035 451.45 .03

Bank Sta: Left Right Coeff Contr. Expan.
188.84 451.45 .3 .5

Downstream Deck/Roadway Coordinates
num= 10
Sta Hi Cord Lo Cord Sta Hi Cord Lo Cord Sta Hi Cord Lo Cord
0 680 89.94 675 137.5 670
189 669 238 667 310 663.82
395 667 429.5 669 483 670
600 675

Downstream Bridge Cross Section Data
Station Elevation Data num= 10
Sta Elev Sta Elev Sta Elev Sta Elev Sta Elev
0 688.21 68.13 676.53 189.82 665.81 203.13 659.96 302.09 636.8
343.57 638.65 411.35 639.86 472.13 638.22 527.67 665.85 580.09 665.88

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .03 203.13 .035 527.67 .03

Bank Sta: Left Right Coeff Contr. Expan.
203.13 527.67 .3 .5

Upstream Embankment side slope = 0 horiz. to 1.0 vertical
Downstream Embankment side slope = 0 horiz. to 1.0 vertical
Maximum allowable submergence for weir flow = .98
Elevation at which weir flow begins =
Energy head used in spillway design =
Spillway height used in design =
Weir crest shape = Broad Crested

Number of Culverts = 1

Culvert Name Shape Rise Span
Culvert #1 Circular 7
FHWA Chart # 1 - Concrete Pipe Culvert
FHWA Scale # 3 - Groove end entrance; pipe projecting from fill
Solution Criteria = Highest U.S. EG
Culvert Upstrm Dist Length Top n Bottom n Depth Blocked Entrance Loss Coef Exit Loss
Coef
90 102 .013 .013 0 .5 1
Upstream Elevation = 646.36
Centerline Station = 345.23
Downstream Elevation = 636.8
Centerline Station = 300

CULVERT OUTPUT Profile #100 yr Culv Group: Culvert #1

Q Culv Group (cfs)	674.70	Culv Full Len (ft)	
# Barrels	1	Culv Vel US (ft/s)	17.53
Q Barrel (cfs)	674.70	Culv Vel DS (ft/s)	31.40
E.G. US. (ft)	660.60	Culv Inv El Up (ft)	646.36
W.S. US. (ft)	660.60	Culv Inv El Dn (ft)	636.80
E.G. DS (ft)	639.84	Culv Frctn Ls (ft)	2.28
W.S. DS (ft)	639.38	Culv Exit Loss (ft)	16.09
Delta EG (ft)	20.76	Culv Entr Loss (ft)	2.39
Delta WS (ft)	21.22	Q Weir (cfs)	
E.G. IC (ft)	660.60	Weir Sta Lft (ft)	
E.G. OC (ft)	660.50	Weir Sta Rgt (ft)	
Culvert Control	Inlet	Weir Submerg	
Culv WS Inlet (ft)	653.36	Weir Max Depth (ft)	
Culv WS Outlet (ft)	640.62	Weir Avg Depth (ft)	
Culv Nml Depth (ft)	2.83	Weir Flow Area (sq ft)	
Culv Crt Depth (ft)	6.49	Min El Weir Flow (ft)	663.83

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section

downstream of the culvert has supercritical flow.

Note: The flow in the culvert is entirely supercritical.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 7

INPUT

Description:

Station Elevation Data			num= 10								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	688.21	68.13	676.53	189.82	665.81	203.13	659.96	302.09	636.8		
343.57	638.65	411.35	639.86	472.13	638.22	527.67	665.85	580.09	665.88		

Manning's n Values			num= 3								
Sta	n Val	Sta	n Val	Sta	n Val						
0	.03	203.13	.035	527.67	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	203.13	527.67		299	226	141	.3	.5

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	639.84	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.46	Wt. n-Val.		0.035	
W.S. Elev (ft)	639.38	Reach Len. (ft)	299.00	226.00	141.00
Crit W.S. (ft)	639.38	Flow Area (sq ft)		124.25	
E.G. Slope (ft/ft)	0.019084	Area (sq ft)		124.25	
Q Total (cfs)	674.70	Flow (cfs)		674.70	
Top Width (ft)	138.84	Top Width (ft)		138.84	
Vel Total (ft/s)	5.43	Avg. Vel. (ft/s)		5.43	
Max Chl Dpth (ft)	2.58	Hydr. Depth (ft)		0.89	
Conv. Total (cfs)	4884.0	Conv. (cfs)		4884.0	
Length Wtd. (ft)	226.00	Wetted Per. (ft)		139.48	
Min Ch El (ft)	636.80	Shear (lb/sq ft)		1.06	
Alpha	1.00	Stream Power (lb/ft s)	580.09	0.00	0.00
Frctn Loss (ft)	3.90	Cum Volume (acre-ft)		3.94	
C & E Loss (ft)	0.09	Cum SA (acres)		2.51	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the

need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program

defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 6

INPUT

Description:

Station Elevation Data			num= 15								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	646.12	39.1	646.12	63.94	656.12	70.61	656.12	78.77	652.45		
150.24	643.59	202.82	636.47	254.54	632	309.92	630.37	328.81	631.28		
367.26	638.48	417.21	661.27	512.01	662.17	542.62	670.46	600	675.2		

Manning's n Values			num= 3								
Sta	n Val	Sta	n Val	Sta	n Val						
0	.03	150.24	.035	367.26	.03						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	150.24	367.26		114	296	522	.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	633.51	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.75	Wt. n-Val.		0.035	
W.S. Elev (ft)	632.76	Reach Len. (ft)	114.00	296.00	522.00
Crit W.S. (ft)	632.76	Flow Area (sq ft)		133.31	
E.G. Slope (ft/ft)	0.016080	Area (sq ft)		133.31	
Q Total (cfs)	924.00	Flow (cfs)		924.00	

Top Width (ft)	91.03	Top Width (ft)	91.03
Vel Total (ft/s)	6.93	Avg. Vel. (ft/s)	6.93
Max Chl Dpth (ft)	2.39	Hydr. Depth (ft)	1.46
Conv. Total (cfs)	7286.6	Conv. (cfs)	7286.6
Length Wtd. (ft)	296.00	Wetted Per. (ft)	91.25
Min Ch El (ft)	630.37	Shear (lb/sq ft)	1.47
Alpha	1.00	Stream Power (lb/ft s)	600.00
Frctn Loss (ft)	4.64	Cum Volume (acre-ft)	3.27
C & E Loss (ft)	0.01	Cum SA (acres)	1.91

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 5

INPUT

Description:

Station Elevation Data		num=	18						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
5.35	691	78.22	656.12	95.46	656.12	110.9	649.73	119.07	648.46
129.96	649.59	147.98	656.12	153.98	656.12	181.21	642.51	239.77	625
265.97	622	291.22	625.01	310.41	625.2	347.9	635	390.74	647.99
414.77	645.32	489.97	645.08	590.71	710.45				

Manning's n Values		num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
5.35	.03	181.21	.035	390.74	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	181.21	390.74		249	202	154	.1

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	626.54	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.84	Wt. n-Val.		0.035	
W.S. Elev (ft)	625.70	Reach Len. (ft)	249.00	202.00	154.00
Crit W.S. (ft)	625.70	Flow Area (sq ft)		125.46	
E.G. Slope (ft/ft)	0.015259	Area (sq ft)		125.46	
Q Total (cfs)	924.00	Flow (cfs)		924.00	
Top Width (ft)	74.86	Top Width (ft)		74.86	
Vel Total (ft/s)	7.37	Avg. Vel. (ft/s)		7.37	
Max Chl Dpth (ft)	3.70	Hydr. Depth (ft)		1.68	
Conv. Total (cfs)	7480.1	Conv. (cfs)		7480.1	
Length Wtd. (ft)	202.00	Wetted Per. (ft)		75.38	
Min Ch El (ft)	622.00	Shear (lb/sq ft)		1.59	
Alpha	1.00	Stream Power (lb/ft s)	590.71	0.00	0.00
Frctn Loss (ft)	3.12	Cum Volume (acre-ft)		2.39	
C & E Loss (ft)	0.01	Cum SA (acres)		1.35	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 4

INPUT

Description:

Station	Elevation	Data	num=	12						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	689	77.66	689	168.69	648.92	171.18	636.81	257.14	620	
304.78	617.02	338.76	618	420.47	641.26	425.47	638.82	525.12	637.28	
589.71	675.77	600	676.63							

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.03	171.18	.035	420.47	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	171.18	420.47		262	206		.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	620.40	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.81	Wt. n-Val.		0.035	
W.S. Elev (ft)	619.59	Reach Len. (ft)	262.00	206.00	149.00
Crit W.S. (ft)	619.59	Flow Area (sq ft)		128.14	
E.G. Slope (ft/ft)	0.015656	Area (sq ft)		128.14	
Q Total (cfs)	924.00	Flow (cfs)		924.00	
Top Width (ft)	80.71	Top Width (ft)		80.71	
Vel Total (ft/s)	7.21	Avg. Vel. (ft/s)		7.21	
Max Chl Dpth (ft)	2.57	Hydr. Depth (ft)		1.59	
Conv. Total (cfs)	7384.8	Conv. (cfs)		7384.8	
Length Wtd. (ft)	206.00	Wetted Per. (ft)		81.02	
Min Ch El (ft)	617.02	Shear (lb/sq ft)		1.55	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	3.12	Cum Volume (acre-ft)		1.80	
C & E Loss (ft)	0.01	Cum SA (acres)		0.99	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 3

INPUT

Description:

Station	Elevation	Data	num=	9						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	679.69	61.42	660.18	131.25	638.04	214.06	617.82	293.57	609.91	
388.1	622.78	468.95	631.79	576.7	629.46	600	641.86			

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.03	131.25	.035	388.1	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	131.25	388.1		399	240		.1	.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	614.54	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.93	Wt. n-Val.		0.035	
W.S. Elev (ft)	613.62	Reach Len. (ft)	399.00	240.00	89.00
Crit W.S. (ft)	613.62	Flow Area (sq ft)		119.50	
E.G. Slope (ft/ft)	0.014702	Area (sq ft)		119.50	
Q Total (cfs)	924.00	Flow (cfs)		924.00	
Top Width (ft)	64.48	Top Width (ft)		64.48	
Vel Total (ft/s)	7.73	Avg. Vel. (ft/s)		7.73	
Max Chl Dpth (ft)	3.71	Hydr. Depth (ft)		1.85	
Conv. Total (cfs)	7620.5	Conv. (cfs)		7620.5	
Length Wtd. (ft)	240.00	Wetted Per. (ft)		64.92	
Min Ch El (ft)	609.91	Shear (lb/sq ft)		1.69	

Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	3.53	Cum Volume (acre-ft)		1.22	
C & E Loss (ft)	0.01	Cum SA (acres)		0.64	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 2

INPUT

Description:

Station Elevation Data		num=	14							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	659.48	18.83	658	70.32	662.82	138.41	661	194.46	633.27	
247.88	610	293.92	605	299.01	603.51	335.08	609.99	414.94	620.39	
447.36	626.37	542.94	625.5	563.04	638.46	600	642.32			

Manning's n Values		num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
0	.03	194.46	.035	414.94	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	194.46	414.94		310	212	114	.1
							.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	608.97	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.02	Wt. n-Val.		0.035	
W.S. Elev (ft)	607.96	Reach Len. (ft)	310.00	212.00	114.00
Crit W.S. (ft)	607.96	Flow Area (sq ft)		114.11	
E.G. Slope (ft/ft)	0.014699	Area (sq ft)		114.11	
Q Total (cfs)	924.00	Flow (cfs)		924.00	
Top Width (ft)	57.06	Top Width (ft)		57.06	
Vel Total (ft/s)	8.10	Avg. Vel. (ft/s)		8.10	
Max Chl Dpth (ft)	4.45	Hydr. Depth (ft)		2.00	
Conv. Total (cfs)	7621.3	Conv. (cfs)		7621.3	
Length Wtd. (ft)	212.00	Wetted Per. (ft)		57.83	
Min Ch El (ft)	603.51	Shear (lb/sq ft)		1.81	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)	3.16	Cum Volume (acre-ft)		0.57	
C & E Loss (ft)	0.04	Cum SA (acres)		0.31	

Warning: The energy equation could not be balanced within the specified number of iterations.
The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 1

INPUT

Description:

Station Elevation Data		num=	10							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	637.79	185.1	638.02	210.62	625	261.76	604.26	291.83	601.15	
332.51	601	345.96	605	394.7	613.21	500.66	622	600	639.56	

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .03 210.62 .035 394.7 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 210.62 394.7 0 0 0 .1 .3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	604.19	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.89	Wt. n-Val.		0.035	
W.S. Elev (ft)	603.30	Reach Len. (ft)			
Crit W.S. (ft)	603.30	Flow Area (sq ft)		121.88	
E.G. Slope (ft/ft)	0.015127	Area (sq ft)		121.88	
Q Total (cfs)	924.00	Flow (cfs)		924.00	
Top Width (ft)	69.23	Top Width (ft)		69.23	
Vel Total (ft/s)	7.58	Avg. Vel. (ft/s)		7.58	
Max Chl Dpth (ft)	2.30	Hydr. Depth (ft)		1.76	
Conv. Total (cfs)	7512.6	Conv. (cfs)		7512.6	
Length Wtd. (ft)		Wetted Per. (ft)		69.67	
Min Ch El (ft)	601.00	Shear (lb/sq ft)		1.65	
Alpha	1.00	Stream Power (lb/ft s)	600.00	0.00	0.00
Frctn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

SUMMARY OF MANNING'S N VALUES

River: Agua Hedionda

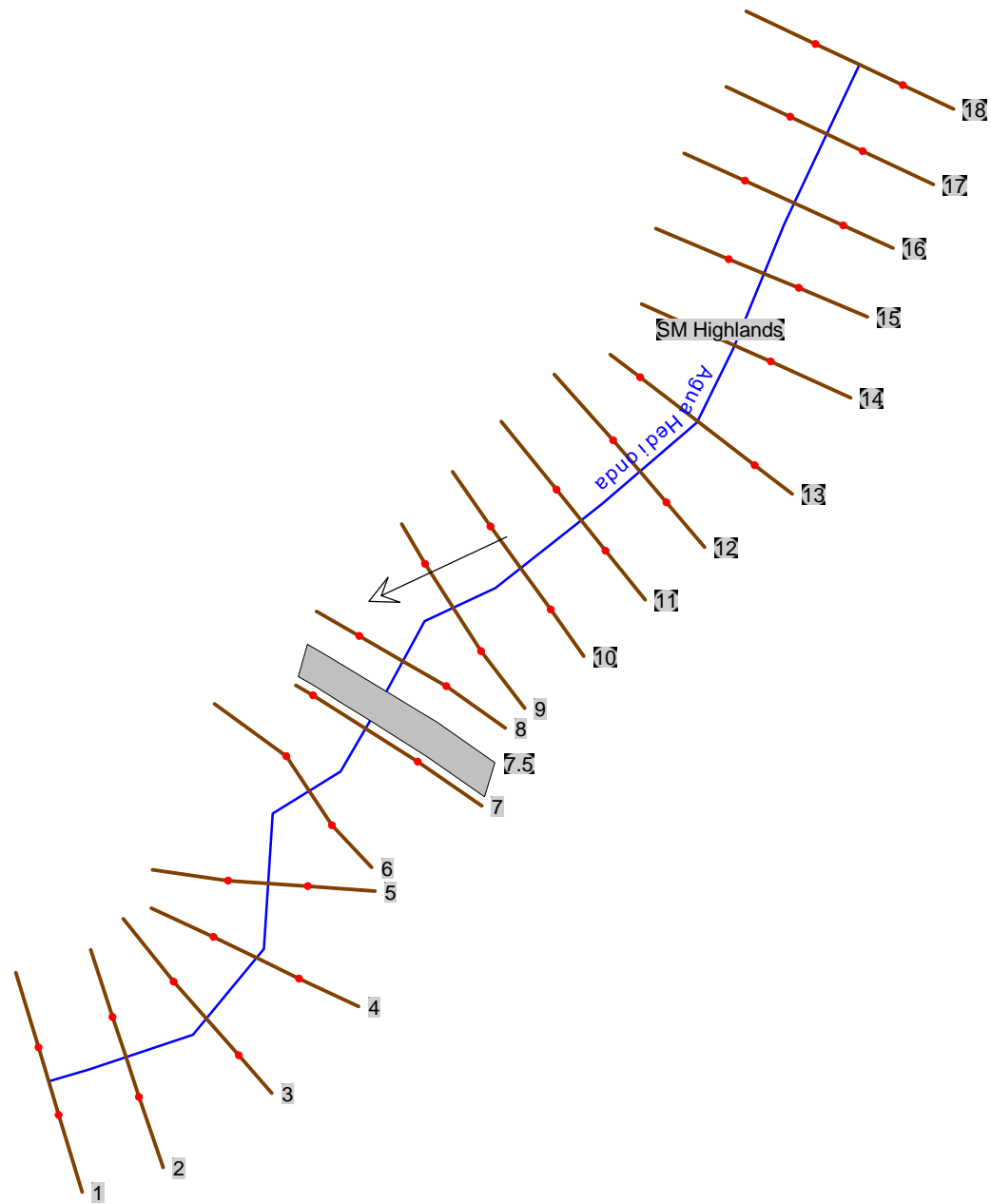
Reach	River Sta.	n1	n2	n3
SM Highlands	18	.03	.035	.03
SM Highlands	17	.03	.035	.03
SM Highlands	16	.03	.035	.03
SM Highlands	15	.03	.035	.03
SM Highlands	14	.03	.035	.03
SM Highlands	13	.03	.035	.03
SM Highlands	12	.03	.035	.03
SM Highlands	11	.03	.04	.03
SM Highlands	10	.03	.04	.03
SM Highlands	9	.03	.04	.03
SM Highlands	8	.03	.035	.03
SM Highlands	7.5	Culvert		
SM Highlands	7	.03	.035	.03
SM Highlands	6	.03	.035	.03
SM Highlands	5	.03	.035	.03
SM Highlands	4	.03	.035	.03
SM Highlands	3	.03	.035	.03
SM Highlands	2	.03	.035	.03
SM Highlands	1	.03	.035	.03

SUMMARY OF REACH LENGTHS

River: Agua Hedionda

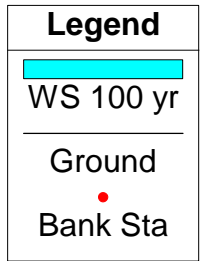
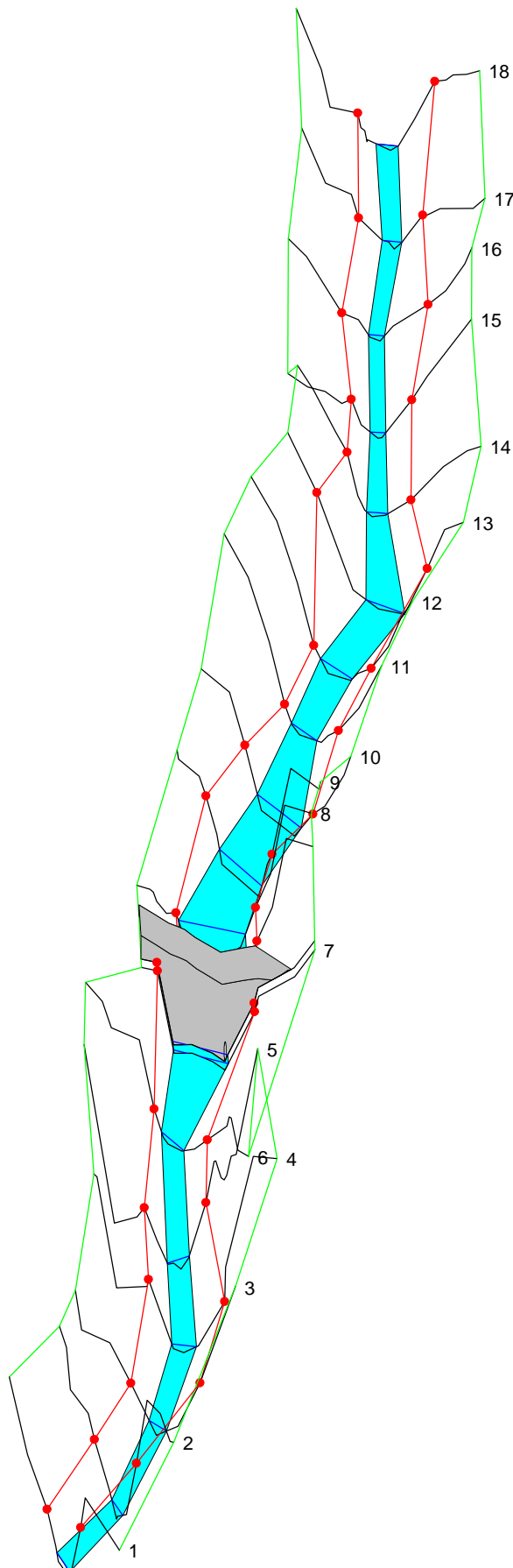
Reach	River Sta.	Left	Channel	Right
SM Highlands	18	251	201	149.5
SM Highlands	17	170	200	230
SM Highlands	16	201	201	201
SM Highlands	15	164	203	238
SM Highlands	14	336	221	89
SM Highlands	13	200	200	200
SM Highlands	12	200	200	200
SM Highlands	11	223	202	180
SM Highlands	10	138	206	267
SM Highlands	9	144	202	677
SM Highlands	8	240	202	612
SM Highlands	7.5	Culvert		
SM Highlands	7	299	226	141
SM Highlands	6	114	296	522
SM Highlands	5	249	202	154
SM Highlands	4	262	206	149
SM Highlands	3	399	240	89

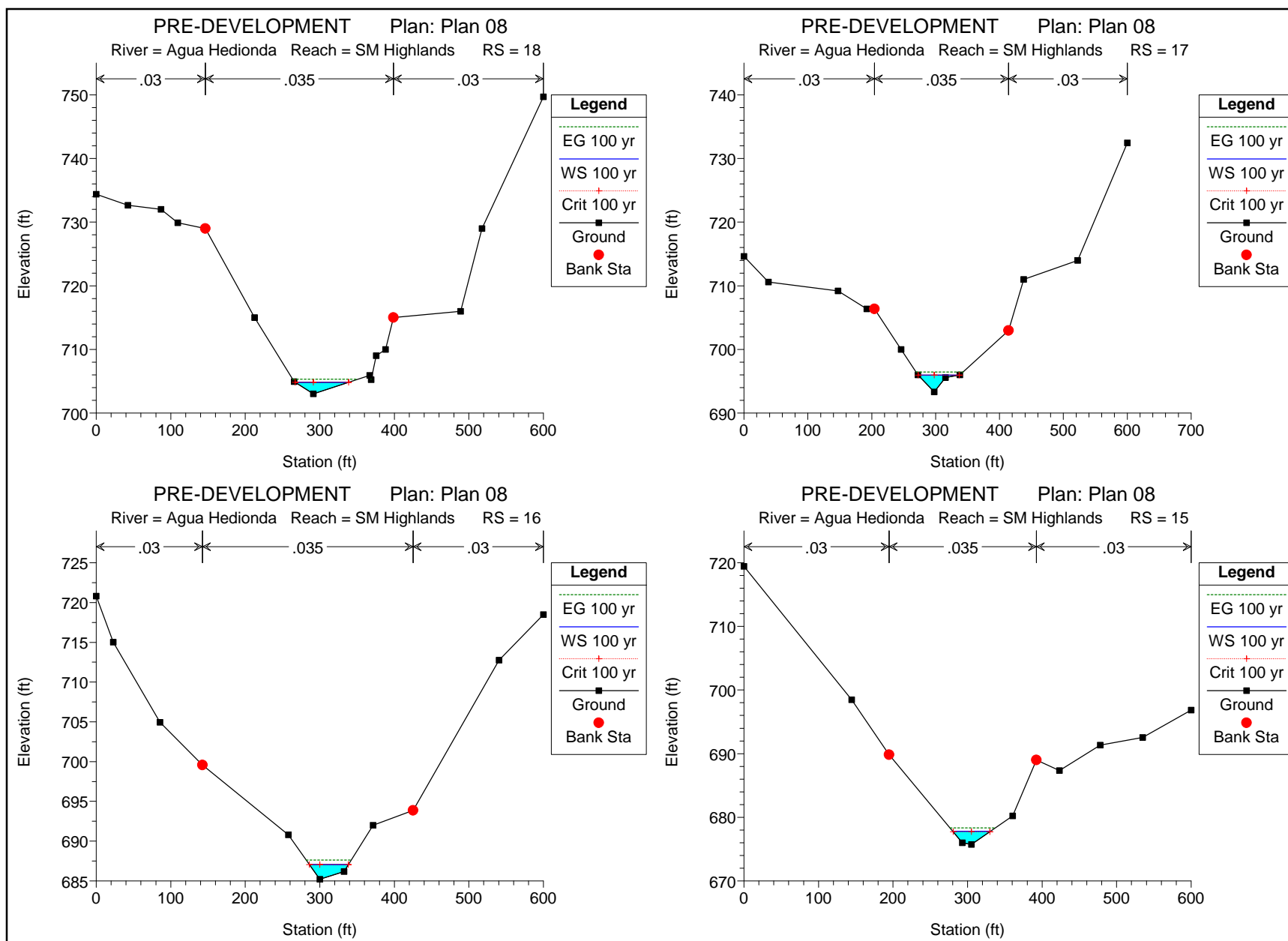
SM Highlands	2	310	212	114
SM Highlands	1	0	0	0

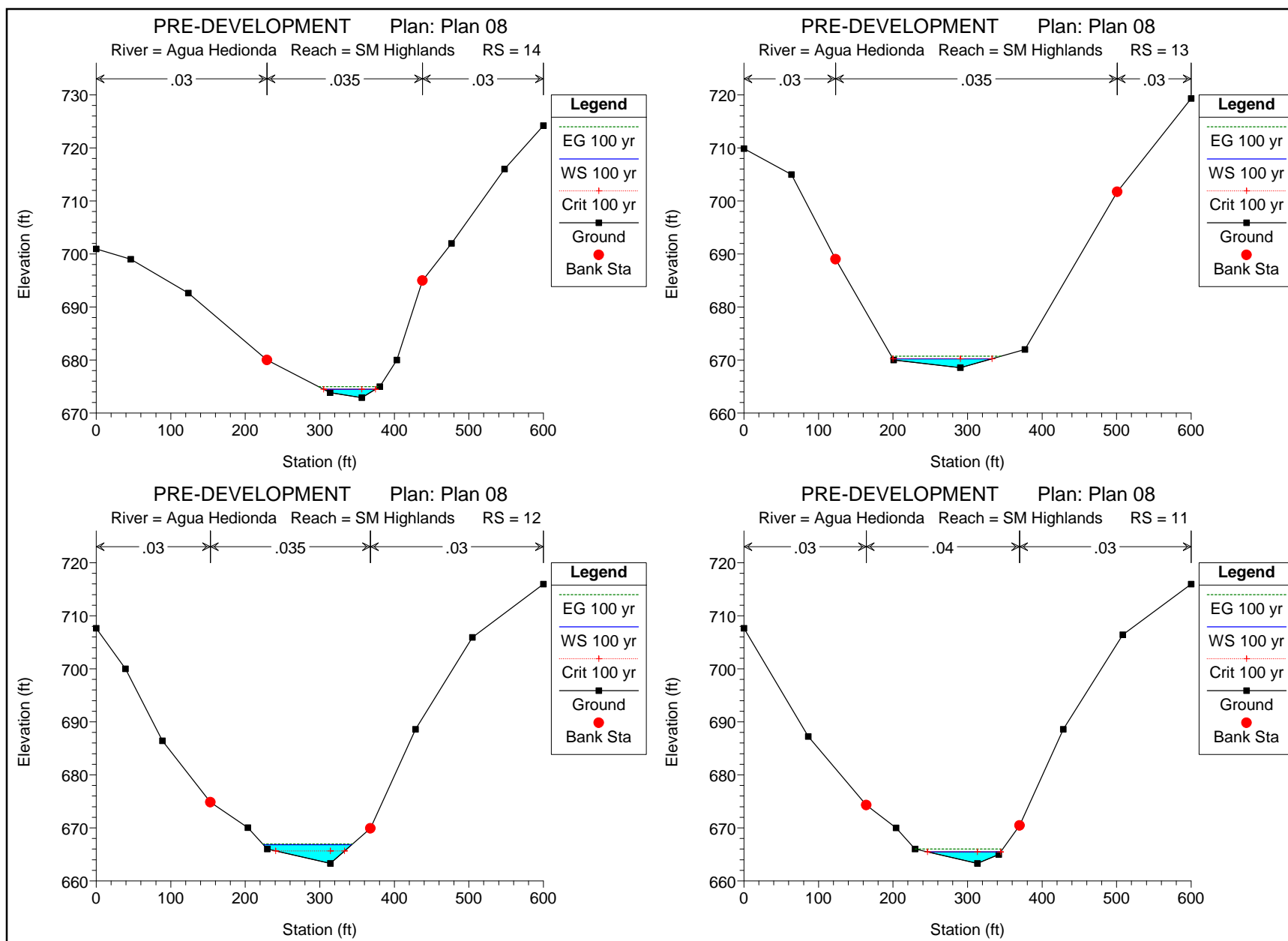


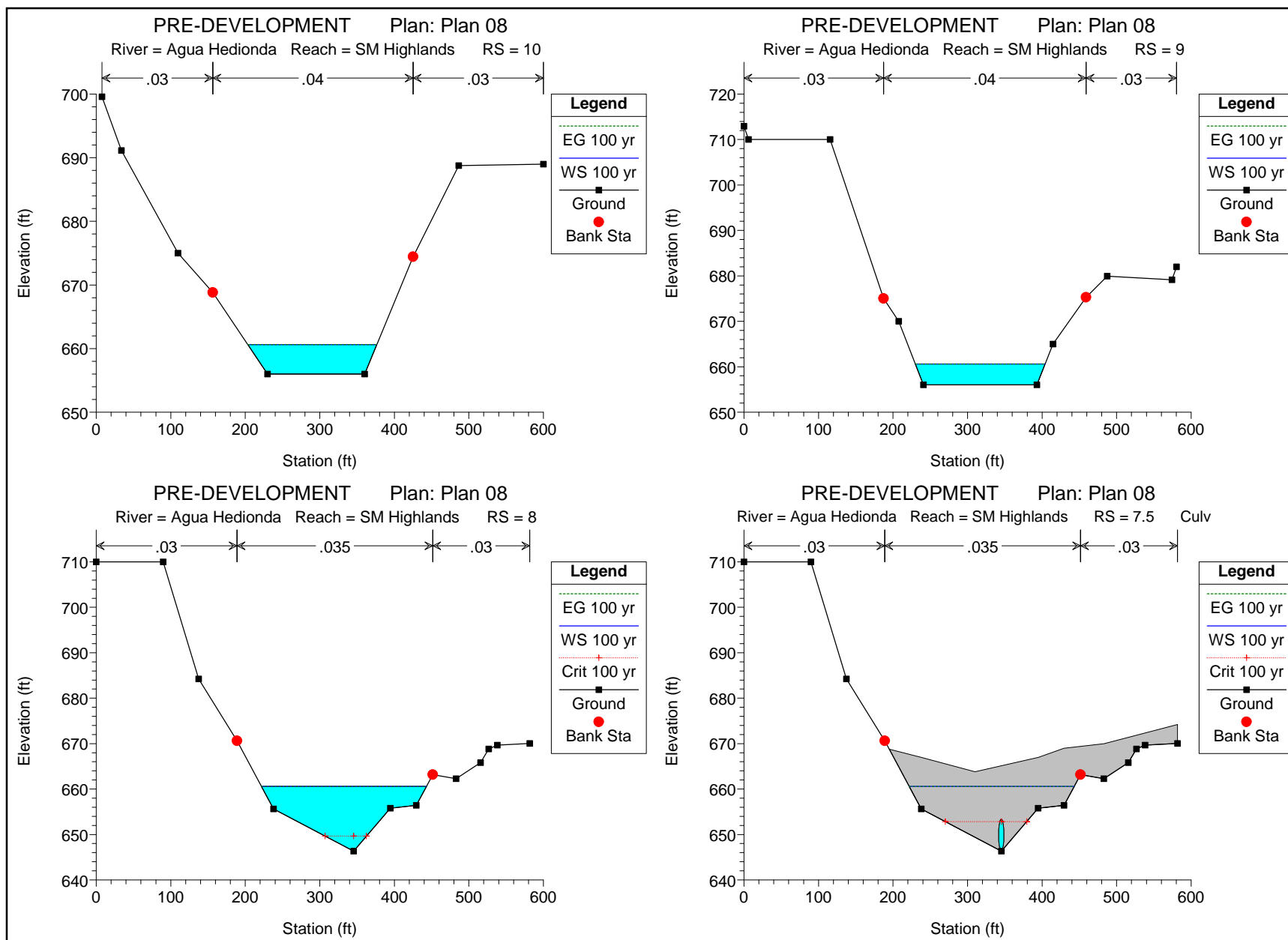
None of the XS's are Geo-Referenced [Geo-Ref user entered XS] [Geo-Ref interpolated XS] [Non Geo-Ref user entered XS] [Non Geo-Ref interpolated XS]

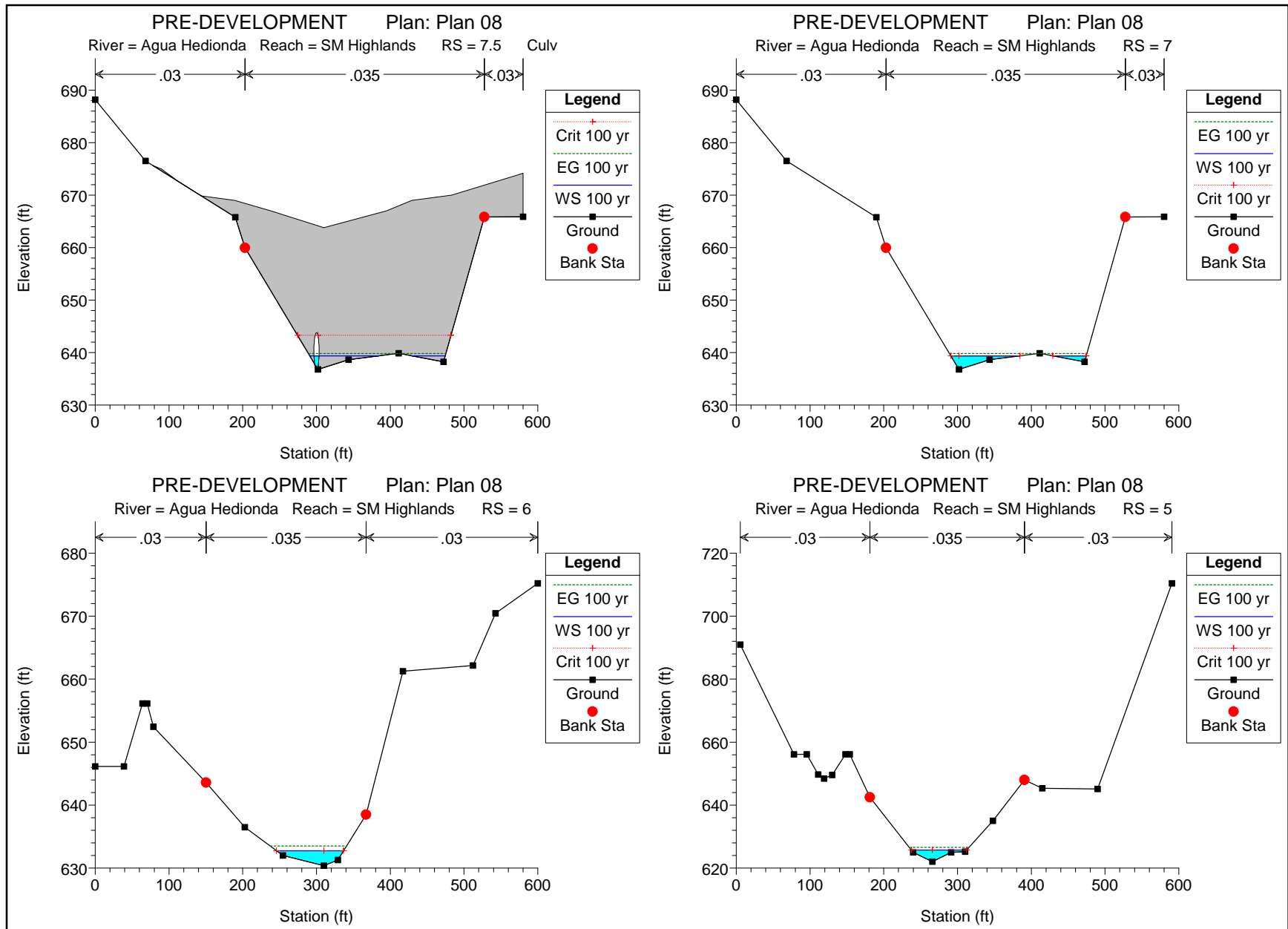
PRE-DEVELOPMENT Plan: Plan 07 2/19/2013
Geom: geo-post-dev Flow: pre-dev flow

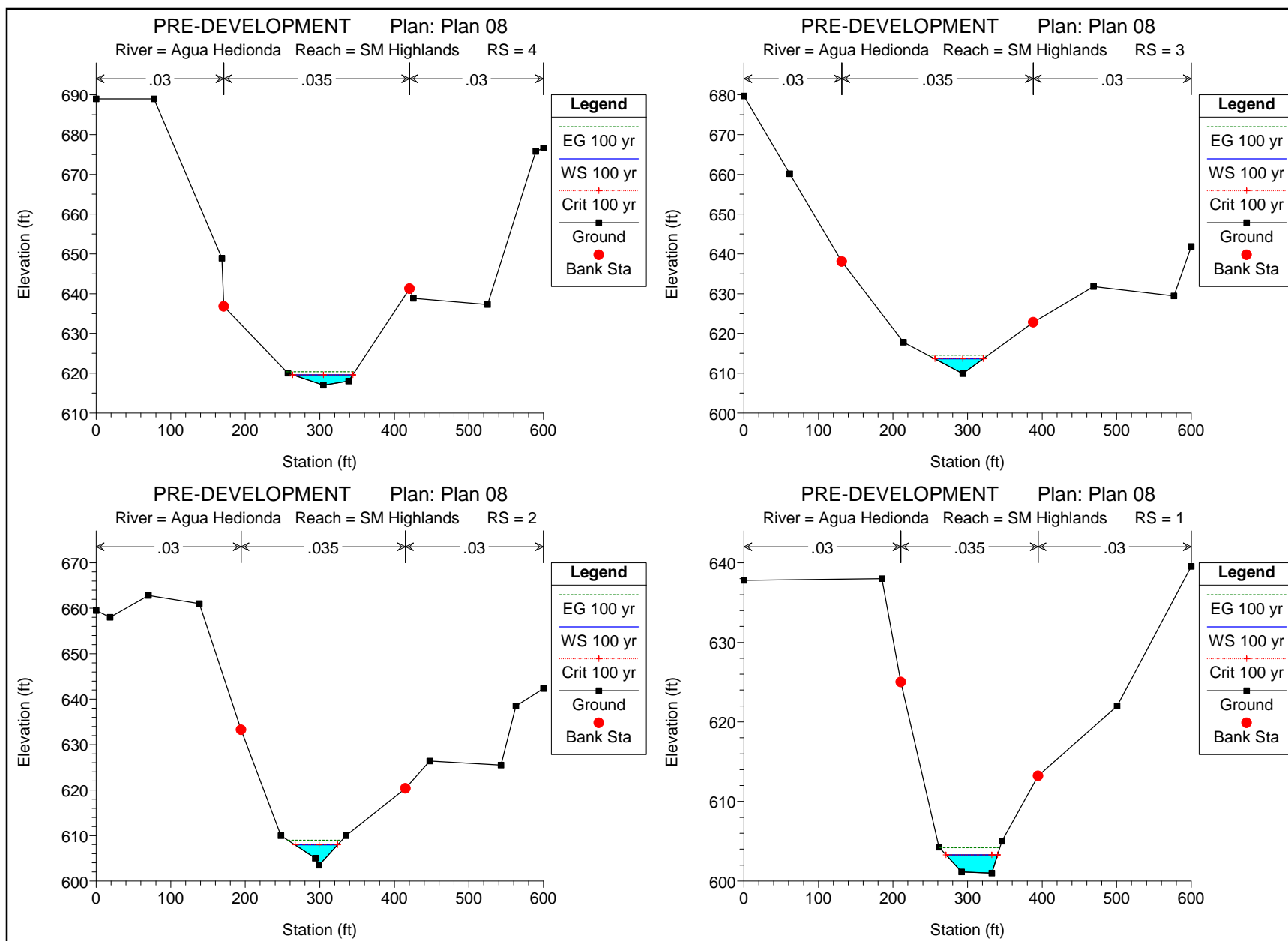






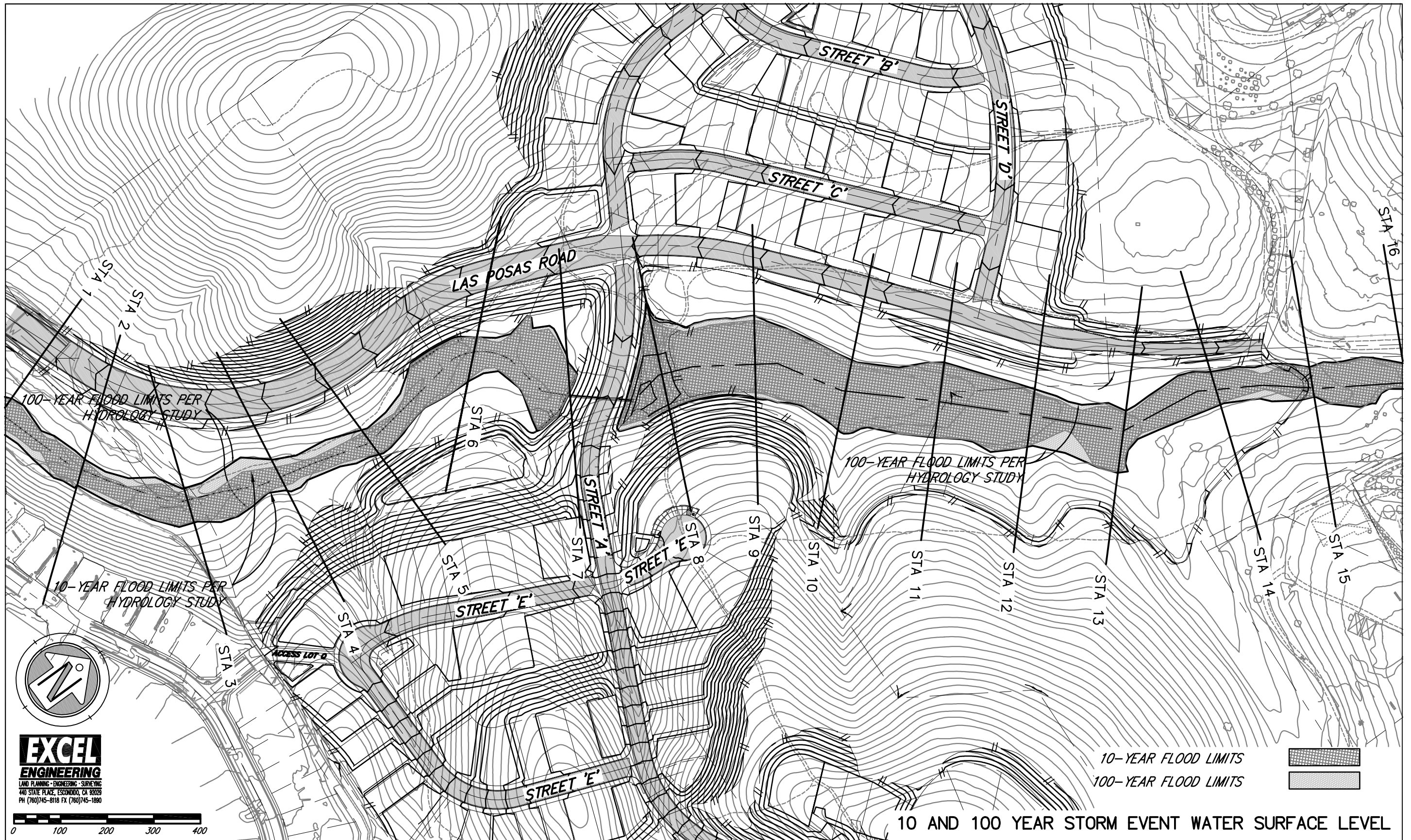






HEC-RAS Plan: Plan 06 River: Agua Hedionda Reach: SM Highlands Profile: 100 yr

Reach	River Sta	Profile	W.S. Elev
			(ft)
SM Highlands	18	100 yr	704.83
SM Highlands	17	100 yr	695.96
SM Highlands	16	100 yr	687.04
SM Highlands	15	100 yr	677.80
SM Highlands	14	100 yr	674.49
SM Highlands	13	100 yr	670.24
SM Highlands	12	100 yr	666.83
SM Highlands	11	100 yr	665.45
SM Highlands	10	100 yr	658.15
SM Highlands	9	100 yr	657.79
SM Highlands	8	100 yr	656.51
SM Highlands	7	100 yr	638.85
SM Highlands	6	100 yr	632.76
SM Highlands	5	100 yr	625.70
SM Highlands	4	100 yr	619.59
SM Highlands	3	100 yr	613.62
SM Highlands	2	100 yr	607.96
SM Highlands	1	100 yr	603.30



HEC-RAS CALCULATION Agua Hedionda Profile: 10 yr

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
SM Highlands	18	100 yr	362.1	703	704.83	704.83	705.3	0.018894	5.5	65.81	71.77	1.01
SM Highlands	17	100 yr	362.1	693.33	695.96	695.96	696.46	0.01842	5.71	63.44	64.05	1.01
SM Highlands	16	100 yr	362.1	685.21	687.04	687.04	687.62	0.017607	6.1	59.32	52.4	1.01
SM Highlands	15	100 yr	362.1	675.72	677.8	677.73	678.33	0.014611	5.85	61.94	50.72	0.93
SM Highlands	14	100 yr	362.1	672.9	674.49	674.49	674.97	0.018734	5.55	65.22	69.74	1.01
SM Highlands	13	100 yr	674.7	668.56	670.24	670.24	670.72	0.019004	5.53	122.03	132.83	1.02
SM Highlands	12	100 yr	674.7	663.29	666.83	665.64	666.95	0.001785	2.84	237.28	118.54	0.35
SM Highlands	11	100 yr	674.7	663.29	665.46	665.46	666.03	0.022816	6.09	110.85	98	1.01
SM Highlands	10	100 yr	674.7	656	660.62		660.63	0.000105	0.96	699.99	173.01	0.08
SM Highlands	9	100 yr	674.7	656	660.6		660.61	0.000085	0.9	750.02	174.09	0.08
SM Highlands	8	100 yr	674.7	646.36	660.6	649.66	660.6	0.000006	0.39	1729.62	221.55	0.02
SM Highlands	7.5		Culvert									
SM Highlands	7	100 yr	674.7	636.8	639.38	639.38	639.84	0.019084	5.43	124.25	138.84	1.01
SM Highlands	6	100 yr	924	630.37	632.76	632.76	633.51	0.01608	6.93	133.31	91.03	1.01
SM Highlands	5	100 yr	924	622	625.7	625.7	626.54	0.015259	7.37	125.46	74.86	1
SM Highlands	4	100 yr	924	617.02	619.59	619.59	620.4	0.015656	7.21	128.14	80.71	1.01
SM Highlands	3	100 yr	924	609.91	613.62	613.62	614.54	0.014702	7.73	119.5	64.48	1
SM Highlands	2	100 yr	924	603.51	607.96	607.96	608.97	0.014699	8.1	114.11	57.06	1.01
SM Highlands	1	100 yr	924	601	603.3	603.3	604.19	0.015127	7.58	121.88	69.23	1.01

HEC-RAS Version 4.1.0 Jan 2010
U.S. Army Corps of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

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X      X  XXXXXX   XXXX      XXXX      XX      XXXX
X      X  X        X   X      X   X      X   X      X
X      X  X        X        X   X      X   X      X
XXXXXXXX XXXX      X        XXX XXXX      XXXXXX   XXXX
X      X  X        X        X   X      X   X          X
X      X  X        X   X      X   X      X   X          X
X      X  XXXXXX   XXXX      X   X      X   X      XXXXX

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PROJECT DATA

Project Title: PRE-DEVELOPMENT
Project File : PRE-DEVELOPMENT.prj
Run Date and Time: 3/27/2013 1:00:41 PM

Project in English units

PLAN DATA

Plan Title: Plan 08
Plan File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.p08

Geometry Title: geo-post-dev
Geometry File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.g02

Flow Title : pre-dev flow
Flow File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.f01

Plan Summary Information:

Number of:	Cross Sections =	18	Multiple Openings =	0
	Culverts =	1	Inline Structures =	0
	Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance	=	0.01
Critical depth calculation tolerance	=	0.01
Maximum number of iterations	=	20
Maximum difference tolerance	=	0.3
Flow tolerance factor	=	0.001

Computation Options

Critical depth computed only where necessary
Conveyance Calculation Method: At breaks in n values only

Friction Slope Method: Average Conveyance
 Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: pre-dev flow
 Flow File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.f01

Flow Data (cfs)

River	Reach	RS	100 yr
Agua Hedionda	SM Highlands	18	362.1
Agua Hedionda	SM Highlands	13	674.7
Agua Hedionda	SM Highlands	6	924

Boundary Conditions

River	Reach	Profile	Upstream
Downstream			
Agua Hedionda	SM Highlands	100 yr	
Critical			

GEOMETRY DATA

Geometry Title: geo-post-dev
 Geometry File : q:\12\12052\TM\TM1\HYD\HECRAS\CROSS SECTION\PRE-DEVELOPMENT.g02

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 18

INPUT

Description:

Station	Elevation	Data	num=	16					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
Elev									
0	734.4	42.56	732.64	87	732	109.57	729.92	146.3	
729									
212.31	715	265.43	704.95	291.31	703	367.1	705.93	368.78	
705.24									
375.71	709	388.24	710	398.89	715	489.05	716	517.58	
729									
600	749.7								

Manning's n Values	num=	3
Sta n Val	Sta n Val	Sta n Val
0 .03	146.3 .035	398.89 .03

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff Contr.
Expan.					
146.3	398.89	251	201	149.5	.1
.3					

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	705.30	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.47	Wt. n-Val.	
0.035			
W.S. Elev (ft)	704.83	Reach Len. (ft)	251.00
201.00 149.50			
Crit W.S. (ft)	704.83	Flow Area (sq ft)	
65.81			
E.G. Slope (ft/ft)	0.018894	Area (sq ft)	
65.81			
Q Total (cfs)	362.10	Flow (cfs)	
362.10			
Top Width (ft)	71.77	Top Width (ft)	
71.77			
Vel Total (ft/s)	5.50	Avg. Vel. (ft/s)	
5.50			
Max Chl Dpth (ft)	1.83	Hydr. Depth (ft)	
0.92			
Conv. Total (cfs)	2634.3	Conv. (cfs)	
2634.3			
Length Wtd. (ft)	201.00	Wetted Per. (ft)	
71.88			
Min Ch El (ft)	703.00	Shear (lb/sq ft)	
1.08			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00 0.00			
Frctn Loss (ft)	3.75	Cum Volume (acre-ft)	
21.97			
C & E Loss (ft)	0.00	Cum SA (acres)	
8.40			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program

defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 17

INPUT

Description:

Station		Elevation Data		num=		14			
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	714.61	38.49	710.59	147.06	709.2	192.29	706.35	204.23	706.36
246.05	700	272.27	696	297.8	693.33	315.3	695.57	338.11	695.98
414.27	702.97	437.9	711.01	522.35	713.98	600.01	732.47		

Manning's n Values		num=		3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.03	204.23	.035	414.27	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.	204.23	414.27	170	200	230	.1
	.3					

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	696.46	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.51	Wt. n-Val.	
0.035			
W.S. Elev (ft)	695.96	Reach Len. (ft)	170.00
200.00 230.00			
Crit W.S. (ft)	695.96	Flow Area (sq ft)	
63.44			
E.G. Slope (ft/ft)	0.018420	Area (sq ft)	
63.44			
Q Total (cfs)	362.10	Flow (cfs)	
362.10			
Top Width (ft)	64.05	Top Width (ft)	
64.05			
Vel Total (ft/s)	5.71	Avg. Vel. (ft/s)	
5.71			
Max Chl Dpth (ft)	2.63	Hydr. Depth (ft)	
0.99			
Conv. Total (cfs)	2668.0	Conv. (cfs)	
2668.0			
Length Wtd. (ft)	200.00	Wetted Per. (ft)	
64.34			
Min Ch El (ft)	693.33	Shear (lb/sq ft)	
1.13			

Alpha	1.00	Stream Power (lb/ft s)	600.01
0.00 0.00			
Frctn Loss (ft)	3.60	Cum Volume (acre-ft)	
21.67			
C & E Loss (ft)	0.01	Cum SA (acres)	
8.08			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the

need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 16

INPUT

Description:

Station Elevation Data	num=	11							
Sta Elev Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev	Sta Elev
Elev									
0 720.8 22.87 715	85.69 704.95 142.68 699.56 257.7								
690.78									
299.85 685.21 332.6 686.18 371.62	692 425.35 693.86 540.3								
712.74									
600 718.48									

Manning's n Values	num=	3			
Sta n Val Sta n Val	Sta n Val	Sta n Val	Sta n Val	Sta n Val	Sta n Val
0 .03 142.68 .035	425.35 .03				

Bank Sta: Left Right	Lengths: Left Channel	Right	Coeff Contr.
Expan.			
142.68 425.35	201 201 201	.1	
.3			

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	687.62	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.58	Wt. n-Val.	
0.035			
W.S. Elev (ft)	687.04	Reach Len. (ft)	201.00
201.00 201.00			

Crit W.S. (ft)	687.04	Flow Area (sq ft)	
59.32			
E.G. Slope (ft/ft)	0.017607	Area (sq ft)	
59.32			
Q Total (cfs)	362.10	Flow (cfs)	
362.10			
Top Width (ft)	52.40	Top Width (ft)	
52.40			
Vel Total (ft/s)	6.10	Avg. Vel. (ft/s)	
6.10			
Max Chl Dpth (ft)	1.83	Hydr. Depth (ft)	
1.13			
Conv. Total (cfs)	2728.9	Conv. (cfs)	
2728.9			
Length Wtd. (ft)	201.00	Wetted Per. (ft)	
52.60			
Min Ch El (ft)	685.21	Shear (lb/sq ft)	
1.24			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)	3.22	Cum Volume (acre-ft)	
21.39			
C & E Loss (ft)	0.01	Cum SA (acres)	
7.81			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 15

INPUT

Description:

Station	Elevation	Data	num=	11	Sta	Elev	Sta	Elev	Sta
Elev	0	719.45	144.68	698.46	194.72	689.85	292.93	676	305.15
675.72	360.63	680.2	392.5	689	423.4	687.33	477.9	691.35	534.95
692.56	600	696.86							

Manning's n Values		num=		3
Sta	n Val	Sta	n Val	Sta n Val
0	.03	194.72	.035	392.5 .03

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff Contr.
Expan.					
194.72	392.5	164	203	238	.1
.3					

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	678.33	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.53	Wt. n-Val.	
0.035			
W.S. Elev (ft)	677.80	Reach Len. (ft)	164.00
203.00 238.00			
Crit W.S. (ft)	677.73	Flow Area (sq ft)	
61.94			
E.G. Slope (ft/ft)	0.014611	Area (sq ft)	
61.94			
Q Total (cfs)	362.10	Flow (cfs)	
362.10			
Top Width (ft)	50.72	Top Width (ft)	
50.72			
Vel Total (ft/s)	5.85	Avg. Vel. (ft/s)	
5.85			
Max Chl Dpth (ft)	2.08	Hydr. Depth (ft)	
1.22			
Conv. Total (cfs)	2995.6	Conv. (cfs)	
2995.6			
Length Wtd. (ft)	203.00	Wetted Per. (ft)	
50.94			
Min Ch El (ft)	675.72	Shear (lb/sq ft)	
1.11			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00 0.00			
Frctn Loss (ft)	3.35	Cum Volume (acre-ft)	
21.11			
C & E Loss (ft)	0.02	Cum SA (acres)	
7.58			

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 14

INPUT

Description:

Station Elevation Data				num=	12				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	700.97	46.34	698.99	123.59	692.64	229.32	680	313.98	
673.84									
356.38	672.9	380.56	675	403.47	680	437.9	695	476.6	
702									
547.73	716	600	724.22						

Manning's n Values				num=	3				
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	229.32	.035	437.9	.03				

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.
Expan.	229.32	437.9		336	221	89	.1
							.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	674.97	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.48	Wt. n-Val.	
0.035			
W.S. Elev (ft)	674.49	Reach Len. (ft)	336.00
221.00	89.00		
Crit W.S. (ft)	674.49	Flow Area (sq ft)	
65.22			
E.G. Slope (ft/ft)	0.018734	Area (sq ft)	
65.22			
Q Total (cfs)	362.10	Flow (cfs)	
362.10			
Top Width (ft)	69.74	Top Width (ft)	
69.74			
Vel Total (ft/s)	5.55	Avg. Vel. (ft/s)	
5.55			
Max Chl Dpth (ft)	1.59	Hydr. Depth (ft)	
0.94			
Conv. Total (cfs)	2645.6	Conv. (cfs)	
2645.6			
Length Wtd. (ft)	221.00	Wetted Per. (ft)	
69.85			
Min Ch El (ft)	672.90	Shear (lb/sq ft)	
1.09			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)	4.18	Cum Volume (acre-ft)	
20.81			
C & E Loss (ft)	0.00	Cum SA (acres)	
7.30			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 13

INPUT

Description:

Station	Elevation	Data	num=	8					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	709.87	63.6	705	122.95	689.01	200.96	670	290.39	
668.56									
376.99	672	500.83	701.72	600	719.32				

Manning's n	Values	num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
0	.03	122.95	.035	500.83	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.
Expan.							
	122.95	500.83		200	200	200	.1
.3							

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	670.72	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.47	Wt. n-Val.	
0.035			
W.S. Elev (ft)	670.24	Reach Len. (ft)	200.00
200.00	200.00		
Crit W.S. (ft)	670.24	Flow Area (sq ft)	
122.03			
E.G. Slope (ft/ft)	0.019004	Area (sq ft)	
122.03			
Q Total (cfs)	674.70	Flow (cfs)	
674.70			

Top Width (ft)	132.83	Top Width (ft)	
132.83			
Vel Total (ft/s)	5.53	Avg. Vel. (ft/s)	
5.53			
Max Chl Dpth (ft)	1.68	Hydr. Depth (ft)	
0.92			
Conv. Total (cfs)	4894.3	Conv. (cfs)	
4894.3			
Length Wtd. (ft)	200.00	Wetted Per. (ft)	
132.90			
Min Ch El (ft)	668.56	Shear (lb/sq ft)	
1.09			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)	0.84	Cum Volume (acre-ft)	
20.34			
C & E Loss (ft)	0.10	Cum SA (acres)	
6.78			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 12

INPUT

Description:

Station Elevation Data				num=	11				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	
Elev									
0	707.64	39.3	700	88.81	686.43	153.24	674.83	203.44	
670.05									
229.59	666	314.09	663.29	367.99	669.93	428.54	688.61	504.8	
705.92									
600	715.97								

Manning's n Values

num= 3

Sta	n Val	Sta	n Val	Sta	n Val
-----	-------	-----	-------	-----	-------

0	.03	153.24	.035	367.99	.03	
Bank Sta: Left	Right	Lengths: Left Channel		Right	Coeff Contr.	
Expan.						
153.24	367.99	200	200	200	.1	
.3						

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	666.95	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.13	Wt. n-Val.	
0.035			
W.S. Elev (ft)	666.83	Reach Len. (ft)	200.00
200.00 200.00			
Crit W.S. (ft)	665.64	Flow Area (sq ft)	
237.28			
E.G. Slope (ft/ft)	0.001785	Area (sq ft)	
237.28			
Q Total (cfs)	674.70	Flow (cfs)	
674.70			
Top Width (ft)	118.54	Top Width (ft)	
118.54			
Vel Total (ft/s)	2.84	Avg. Vel. (ft/s)	
2.84			
Max Chl Dpth (ft)	3.54	Hydr. Depth (ft)	
2.00			
Conv. Total (cfs)	15970.9	Conv. (cfs)	
15970.9			
Length Wtd. (ft)	200.00	Wetted Per. (ft)	
118.87			
Min Ch El (ft)	663.29	Shear (lb/sq ft)	
0.22			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00 0.00			
Frctn Loss (ft)	0.87	Cum Volume (acre-ft)	
19.51			
C & E Loss (ft)	0.04	Cum SA (acres)	
6.21			

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 11

INPUT

Description:

Station Elevation Data num= 11

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	707.64	86.22	687.22	164.31	674.29	204.06	670	229.59	
313.1	663.29	341.94	665	369.82	670.46	428.54	688.61	508.15	
600	715.97								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.03	164.31	.04	369.82	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.	164.31	369.82	223	202	180	.1
	.3					

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	666.03	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.58	Wt. n-Val.	
0.040			
W.S. Elev (ft)	665.46	Reach Len. (ft)	223.00
202.00 180.00			
Crit W.S. (ft)	665.46	Flow Area (sq ft)	
110.85			
E.G. Slope (ft/ft)	0.022816	Area (sq ft)	
110.85			
Q Total (cfs)	674.70	Flow (cfs)	
674.70			
Top Width (ft)	98.00	Top Width (ft)	
98.00			
Vel Total (ft/s)	6.09	Avg. Vel. (ft/s)	
6.09			
Max Chl Dpth (ft)	2.17	Hydr. Depth (ft)	
1.13			
Conv. Total (cfs)	4466.8	Conv. (cfs)	
4466.8			
Length Wtd. (ft)	202.00	Wetted Per. (ft)	
98.13			
Min Ch El (ft)	663.29	Shear (lb/sq ft)	
1.61			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00 0.00			
Frctn Loss (ft)	0.07	Cum Volume (acre-ft)	
18.71			
C & E Loss (ft)	0.17	Cum SA (acres)	
5.71			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m).
This may indicate the need for additional cross sections.
Warning: The conveyance ratio (upstream conveyance divided by downstream
conveyance) is less than 0.7 or greater than 1.4.
This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the
current and previous cross section. This may indicate the
need for additional cross sections.
Warning: During the standard step iterations, when the assumed water
surface was set equal to critical depth, the calculated
water surface came back below critical depth. This indicates
that there is not a valid subcritical answer. The program
defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 10

INPUT

Description:

Station Elevation Data				num=	9				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
7.61	699.57	33.88	691.15	109.68	675	156.53	668.82	229.75	
656									
360.07	656	425.32	674.44	486.5	688.78	600	689		

Manning's n Values				num=	3				
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
7.61	.03	156.53	.04	425.32	.03				

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.						
	156.53	425.32		138	206	267
						.1
						.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	660.63	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.01	Wt. n-Val.	
0.040			
W.S. Elev (ft)	660.62	Reach Len. (ft)	138.00
206.00	267.00		
Crit W.S. (ft)		Flow Area (sq ft)	
699.99			
E.G. Slope (ft/ft)	0.000105	Area (sq ft)	
699.99			
Q Total (cfs)	674.70	Flow (cfs)	
674.70			
Top Width (ft)	173.01	Top Width (ft)	
173.01			

Vel Total (ft/s)	0.96	Avg. Vel. (ft/s)	
0.96			
Max Chl Dpth (ft)	4.62	Hydr. Depth (ft)	
4.05			
Conv. Total (cfs)	65761.3	Conv. (cfs)	
65761.3			
Length Wtd. (ft)	206.00	Wetted Per. (ft)	
174.05			
Min Ch El (ft)	656.00	Shear (lb/sq ft)	
0.03			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)	0.02	Cum Volume (acre-ft)	
16.83			
C & E Loss (ft)	0.00	Cum SA (acres)	
5.08			

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 9

INPUT

Description:

Station Elevation Data				num=	12				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
Elev									
0	712.95	5.98	710	115.62	710	187.3	675	207.52	
670									
240.74	656	392.94	656	414.44	665	459	675.27	487.2	
679.95									
574.16	679.13	580.28	682						

Manning's n Values				num=	3		
Sta	n Val	Sta	n Val	Sta	n Val		
0	.03	187.3	.04	459	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.						
	187.3	459		144	202	677
						.1
						.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	660.61	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.01	Wt. n-Val.	
0.040			
W.S. Elev (ft)	660.60	Reach Len. (ft)	144.00
202.00	677.00		
Crit W.S. (ft)		Flow Area (sq ft)	
750.02			

E.G. Slope (ft/ft)	0.000085	Area (sq ft)	
750.02			
Q Total (cfs)	674.70	Flow (cfs)	
674.70			
Top Width (ft)	174.09	Top Width (ft)	
174.09			
Vel Total (ft/s)	0.90	Avg. Vel. (ft/s)	
0.90			
Max Chl Dpth (ft)	4.60	Hydr. Depth (ft)	
4.31			
Conv. Total (cfs)	73249.6	Conv. (cfs)	
73249.6			
Length Wtd. (ft)	202.00	Wetted Per. (ft)	
175.94			
Min Ch El (ft)	656.00	Shear (lb/sq ft)	
0.02			
Alpha	1.00	Stream Power (lb/ft s)	580.28
0.00 0.00			
Frctn Loss (ft)	0.00	Cum Volume (acre-ft)	
13.40			
C & E Loss (ft)	0.00	Cum SA (acres)	
4.26			

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 8

INPUT

Description:

Station Elevation Data				num=	14				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	
Elev									
0	710	89.94	710	137.54	684.23	188.84	670.63	237.78	
655.63									
345.23	646.36	394.69	655.76	429.46	656.43	451.45	663.15	482.96	
662.26									
515.68	665.79	526.53	668.84	538.31	669.65	581.5	670.03		

Manning's n Values

num=				3		
Sta	n Val	Sta	n Val	Sta	n Val	
0	.03	188.84	.035	451.45	.03	

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.						
	188.84	451.45		240	202	612
						.3
						.5

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	660.60	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.00	Wt. n-Val.	
0.035			
W.S. Elev (ft)	660.60	Reach Len. (ft)	240.00
202.00 612.00			
Crit W.S. (ft)	649.66	Flow Area (sq ft)	
1729.62			
E.G. Slope (ft/ft)	0.000006	Area (sq ft)	
1729.62			
Q Total (cfs)	674.70	Flow (cfs)	
674.70			
Top Width (ft)	221.55	Top Width (ft)	
221.55			
Vel Total (ft/s)	0.39	Avg. Vel. (ft/s)	
0.39			
Max Chl Dpth (ft)	14.24	Hydr. Depth (ft)	
7.81			
Conv. Total (cfs)	286688.6	Conv. (cfs)	
286688.6			
Length Wtd. (ft)	202.00	Wetted Per. (ft)	
224.21			
Min Ch El (ft)	646.36	Shear (lb/sq ft)	
0.00			
Alpha	1.00	Stream Power (lb/ft s)	581.50
0.00 0.00			
Frctn Loss (ft)		Cum Volume (acre-ft)	
7.65			
C & E Loss (ft)		Cum SA (acres)	
3.34			

CULVERT

RIVER: Agua Hedionda

REACH: SM Highlands RS: 7.5

INPUT

Description:

Distance from Upstream XS = 90

Deck/Roadway Width = 88

Weir Coefficient = 2.6

Upstream Deck/Roadway Coordinates

num= 10

Sta	Hi	Cord	Lo	Cord	Sta	Hi	Cord	Lo	Cord	Sta	Hi	Cord	Lo	Cord
0		680			89.94		675			137.5		670		
189		669			238		667			310		663.82		
395		667			429.5		669			483		670		
600		675												

Upstream Bridge Cross Section Data

Station Elevation Data				num=	14				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	
0	710	89.94	710	137.54	684.23	188.84	670.63	237.78	
655.63									
345.23	646.36	394.69	655.76	429.46	656.43	451.45	663.15	482.96	
662.26									
515.68	665.79	526.53	668.84	538.31	669.65	581.5	670.03		

Manning's n Values				num=	3		
Sta	n Val	Sta	n Val	Sta	n Val		
0	.03	188.84	.035	451.45	.03		

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	188.84	451.45		.3	.5

Downstream Deck/Roadway Coordinates									
num= 10									
Sta	Hi	Cord	Lo	Cord	Sta	Hi	Cord	Lo	Cord
0		680			89.94		675		
189		669			238		667		
395		667			429.5		669		
600		675							

Downstream Bridge Cross Section Data									
Station Elevation Data				num=	10				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	
0	688.21	68.13	676.53	189.82	665.81	203.13	659.96	302.09	
636.8									
343.57	638.65	411.35	639.86	472.13	638.22	527.67	665.85	580.09	
665.88									

Manning's n Values				num=	3		
Sta	n Val	Sta	n Val	Sta	n Val		
0	.03	203.13	.035	527.67	.03		

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	203.13	527.67		.3	.5

Upstream Embankment side slope vertical	=	0 horiz. to 1.0
Downstream Embankment side slope vertical	=	0 horiz. to 1.0
Maximum allowable submergence for weir flow	=	.98
Elevation at which weir flow begins	=	
Energy head used in spillway design	=	
Spillway height used in design	=	
Weir crest shape	=	Broad Crested

Number of Culverts = 1

Culvert Name	Shape	Rise	Span
Culvert #1	Circular	7	

FHWA Chart # 1 - Concrete Pipe Culvert
 FHWA Scale # 3 - Groove end entrance; pipe projecting from fill
 Solution Criteria = Highest U.S. EG
 Culvert Upstrm Dist Length Top n Bottom n Depth Blocked Entrance
 Loss Coef Exit Loss Coef
 90 102 .013 .013 0
 .5 1
 Upstream Elevation = 646.36
 Centerline Station = 345.23
 Downstream Elevation = 636.8
 Centerline Station = 300

CULVERT OUTPUT Profile #100 yr Culv Group: Culvert #1

Q Culv Group (cfs)	674.70	Culv Full Len (ft)	
# Barrels	1	Culv Vel US (ft/s)	17.53
Q Barrel (cfs)	674.70	Culv Vel DS (ft/s)	31.40
E.G. US. (ft)	660.60	Culv Inv El Up (ft)	646.36
W.S. US. (ft)	660.60	Culv Inv El Dn (ft)	636.80
E.G. DS (ft)	639.84	Culv Frctn Ls (ft)	2.28
W.S. DS (ft)	639.38	Culv Exit Loss (ft)	16.09
Delta EG (ft)	20.76	Culv Entr Loss (ft)	2.39
Delta WS (ft)	21.22	Q Weir (cfs)	
E.G. IC (ft)	660.60	Weir Sta Lft (ft)	
E.G. OC (ft)	660.50	Weir Sta Rgt (ft)	
Culvert Control	Inlet	Weir Submerg	
Culv WS Inlet (ft)	653.36	Weir Max Depth (ft)	
Culv WS Outlet (ft)	640.62	Weir Avg Depth (ft)	
Culv Nml Depth (ft)	2.83	Weir Flow Area (sq ft)	
Culv Crt Depth (ft)	6.49	Min El Weir Flow (ft)	663.83

Warning: Since the culvert has supercritical flow, the program should be
 run in mixed flow in order to check if the cross section
 downstream of the culvert has supercritical flow.

Note: The flow in the culvert is entirely supercritical.

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 7

INPUT

Description:

Station	Elevation	Data	num=	10					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
Elev									
0	688.21	68.13	676.53	189.82	665.81	203.13	659.96	302.09	
636.8									
343.57	638.65	411.35	639.86	472.13	638.22	527.67	665.85	580.09	
665.88									

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.03	203.13	.035	527.67	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.	203.13	527.67		299	226	141
						.3

.5

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	639.84	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.46	Wt. n-Val.	
0.035			
W.S. Elev (ft)	639.38	Reach Len. (ft)	299.00
226.00	141.00		
Crit W.S. (ft)	639.38	Flow Area (sq ft)	
124.25			
E.G. Slope (ft/ft)	0.019084	Area (sq ft)	
124.25			
Q Total (cfs)	674.70	Flow (cfs)	
674.70			
Top Width (ft)	138.84	Top Width (ft)	
138.84			
Vel Total (ft/s)	5.43	Avg. Vel. (ft/s)	
5.43			
Max Chl Dpth (ft)	2.58	Hydr. Depth (ft)	
0.89			
Conv. Total (cfs)	4884.0	Conv. (cfs)	
4884.0			
Length Wtd. (ft)	226.00	Wetted Per. (ft)	
139.48			
Min Ch El (ft)	636.80	Shear (lb/sq ft)	
1.06			
Alpha	1.00	Stream Power (lb/ft s)	580.09
0.00	0.00		
Frctn Loss (ft)	3.90	Cum Volume (acre-ft)	
3.94			
C & E Loss (ft)	0.09	Cum SA (acres)	
2.51			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the

need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
REACH: SM Highlands RS: 6

INPUT

Description:

Station	Elevation	Data	num=	15					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	646.12	39.1	646.12	63.94	656.12	70.61	656.12	78.77	
652.45									
150.24	643.59	202.82	636.47	254.54	632	309.92	630.37	328.81	
631.28									
367.26	638.48	417.21	661.27	512.01	662.17	542.62	670.46	600	
675.2									

Manning's n	Values	num=	3				
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	150.24	.035	367.26	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.						
	150.24	367.26		114	296	522
						.1
						.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	633.51	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.75	Wt. n-Val.	
0.035			
W.S. Elev (ft)	632.76	Reach Len. (ft)	114.00
296.00	522.00		
Crit W.S. (ft)	632.76	Flow Area (sq ft)	
133.31			
E.G. Slope (ft/ft)	0.016080	Area (sq ft)	
133.31			
Q Total (cfs)	924.00	Flow (cfs)	
924.00			
Top Width (ft)	91.03	Top Width (ft)	
91.03			
Vel Total (ft/s)	6.93	Avg. Vel. (ft/s)	
6.93			
Max Chl Dpth (ft)	2.39	Hydr. Depth (ft)	
1.46			
Conv. Total (cfs)	7286.6	Conv. (cfs)	
7286.6			

Length Wtd. (ft)	296.00	Wetted Per. (ft)	
91.25			
Min Ch El (ft)	630.37	Shear (lb/sq ft)	
1.47			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)	4.64	Cum Volume (acre-ft)	
3.27			
C & E Loss (ft)	0.01	Cum SA (acres)	
1.91			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 5

INPUT

Description:

Station Elevation Data				num=	18				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	
5.35	691	78.22	656.12	95.46	656.12	110.9	649.73	119.07	
648.46									
129.96	649.59	147.98	656.12	153.98	656.12	181.21	642.51	239.77	
625									
265.97	622	291.22	625.01	310.41	625.2	347.9	635	390.74	
647.99									
414.77	645.32	489.97	645.08	590.71	710.45				

Manning's n Values				num=	3		
Sta	n Val	Sta	n Val	Sta	n Val		
5.35	.03	181.21	.035	390.74	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.						
	181.21	390.74		249	202	154
						.1
						.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	626.54	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.84	Wt. n-Val.	
0.035			
W.S. Elev (ft)	625.70	Reach Len. (ft)	249.00
202.00 154.00			
Crit W.S. (ft)	625.70	Flow Area (sq ft)	
125.46			
E.G. Slope (ft/ft)	0.015259	Area (sq ft)	
125.46			
Q Total (cfs)	924.00	Flow (cfs)	
924.00			
Top Width (ft)	74.86	Top Width (ft)	
74.86			
Vel Total (ft/s)	7.37	Avg. Vel. (ft/s)	
7.37			
Max Chl Dpth (ft)	3.70	Hydr. Depth (ft)	
1.68			
Conv. Total (cfs)	7480.1	Conv. (cfs)	
7480.1			
Length Wtd. (ft)	202.00	Wetted Per. (ft)	
75.38			
Min Ch El (ft)	622.00	Shear (lb/sq ft)	
1.59			
Alpha	1.00	Stream Power (lb/ft s)	590.71
0.00 0.00			
Frctn Loss (ft)	3.12	Cum Volume (acre-ft)	
2.39			
C & E Loss (ft)	0.01	Cum SA (acres)	
1.35			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 4

INPUT

Description:
 Station Elevation Data num= 12

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta
0	689	77.66	689	168.69	648.92	171.18	636.81	257.14
620								
304.78	617.02	338.76	618	420.47	641.26	425.47	638.82	525.12
637.28								
589.71	675.77	600	676.63					

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.03	171.18	.035	420.47	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.						
	171.18	420.47		262	206	149
						.1
						.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	620.40	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.81	Wt. n-Val.	
0.035			
W.S. Elev (ft)	619.59	Reach Len. (ft)	262.00
206.00	149.00		
Crit W.S. (ft)	619.59	Flow Area (sq ft)	
128.14			
E.G. Slope (ft/ft)	0.015656	Area (sq ft)	
128.14			
Q Total (cfs)	924.00	Flow (cfs)	
924.00			
Top Width (ft)	80.71	Top Width (ft)	
80.71			
Vel Total (ft/s)	7.21	Avg. Vel. (ft/s)	
7.21			
Max Chl Dpth (ft)	2.57	Hydr. Depth (ft)	
1.59			
Conv. Total (cfs)	7384.8	Conv. (cfs)	
7384.8			
Length Wtd. (ft)	206.00	Wetted Per. (ft)	
81.02			
Min Ch El (ft)	617.02	Shear (lb/sq ft)	
1.55			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)	3.12	Cum Volume (acre-ft)	
1.80			
C & E Loss (ft)	0.01	Cum SA (acres)	
0.99			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 3

INPUT

Description:

Station	Elevation	Data	num=	9					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	679.69	61.42	660.18	131.25	638.04	214.06	617.82	293.57	609.91
388.1	622.78	468.95	631.79	576.7	629.46	600	641.86		

Manning's n	Values	num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
0	.03	131.25	.035	388.1	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.	131.25	388.1	399	240	89	.1
	.3					

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	614.54	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.93	Wt. n-Val.	
0.035			
W.S. Elev (ft)	613.62	Reach Len. (ft)	399.00
240.00	89.00		
Crit W.S. (ft)	613.62	Flow Area (sq ft)	
119.50			
E.G. Slope (ft/ft)	0.014702	Area (sq ft)	
119.50			
Q Total (cfs)	924.00	Flow (cfs)	
924.00			
Top Width (ft)	64.48	Top Width (ft)	
64.48			
Vel Total (ft/s)	7.73	Avg. Vel. (ft/s)	
7.73			
Max Chl Dpth (ft)	3.71	Hydr. Depth (ft)	
1.85			

Conv. Total (cfs)	7620.5	Conv. (cfs)	
7620.5			
Length Wtd. (ft)	240.00	Wetted Per. (ft)	
64.92			
Min Ch El (ft)	609.91	Shear (lb/sq ft)	
1.69			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)	3.53	Cum Volume (acre-ft)	
1.22			
C & E Loss (ft)	0.01	Cum SA (acres)	
0.64			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda

REACH: SM Highlands RS: 2

INPUT

Description:

Station Elevation Data				num=	14				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	659.48	18.83	658	70.32	662.82	138.41	661	194.46	
633.27									
247.88	610	293.92	605	299.01	603.51	335.08	609.99	414.94	
620.39									
447.36	626.37	542.94	625.5	563.04	638.46	600	642.32		

Manning's n Values				num=	3		
Sta	n Val	Sta	n Val	Sta	n Val		
0	.03	194.46	.035	414.94	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.
Expan.						
	194.46	414.94		310	212	114
						.1
						.3

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	608.97	Element	Left OB
Channel Right OB			
Vel Head (ft)	1.02	Wt. n-Val.	
0.035			
W.S. Elev (ft)	607.96	Reach Len. (ft)	310.00
212.00 114.00			
Crit W.S. (ft)	607.96	Flow Area (sq ft)	
114.11			
E.G. Slope (ft/ft)	0.014699	Area (sq ft)	
114.11			
Q Total (cfs)	924.00	Flow (cfs)	
924.00			
Top Width (ft)	57.06	Top Width (ft)	
57.06			
Vel Total (ft/s)	8.10	Avg. Vel. (ft/s)	
8.10			
Max Chl Dpth (ft)	4.45	Hydr. Depth (ft)	
2.00			
Conv. Total (cfs)	7621.3	Conv. (cfs)	
7621.3			
Length Wtd. (ft)	212.00	Wetted Per. (ft)	
57.83			
Min Ch El (ft)	603.51	Shear (lb/sq ft)	
1.81			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00 0.00			
Frctn Loss (ft)	3.16	Cum Volume (acre-ft)	
0.57			
C & E Loss (ft)	0.04	Cum SA (acres)	
0.31			

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Agua Hedionda
 REACH: SM Highlands RS: 1

INPUT

Description:
 Station Elevation Data num= 10

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta
0	637.79	185.1	638.02	210.62	625	261.76	604.26	291.83
601.15								
332.51	601	345.96	605	394.7	613.21	500.66	622	600
639.56								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.03	210.62	.035	394.7	.03

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.
Expan.	210.62	394.7		0	0	0	.1
	.3						

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	604.19	Element	Left OB
Channel Right OB			
Vel Head (ft)	0.89	Wt. n-Val.	
0.035			
W.S. Elev (ft)	603.30	Reach Len. (ft)	
Crit W.S. (ft)	603.30	Flow Area (sq ft)	
121.88			
E.G. Slope (ft/ft)	0.015127	Area (sq ft)	
121.88			
Q Total (cfs)	924.00	Flow (cfs)	
924.00			
Top Width (ft)	69.23	Top Width (ft)	
69.23			
Vel Total (ft/s)	7.58	Avg. Vel. (ft/s)	
7.58			
Max Chl Dpth (ft)	2.30	Hydr. Depth (ft)	
1.76			
Conv. Total (cfs)	7512.6	Conv. (cfs)	
7512.6			
Length Wtd. (ft)		Wetted Per. (ft)	
69.67			
Min Ch El (ft)	601.00	Shear (lb/sq ft)	
1.65			
Alpha	1.00	Stream Power (lb/ft s)	600.00
0.00	0.00		
Frctn Loss (ft)		Cum Volume (acre-ft)	
C & E Loss (ft)		Cum SA (acres)	

SUMMARY OF MANNING'S N VALUES

River:Agua Hedionda

Reach	River Sta.	n1	n2	n3
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SM Highlands	18	.03	.035	.03
SM Highlands	17	.03	.035	.03
SM Highlands	16	.03	.035	.03
SM Highlands	15	.03	.035	.03
SM Highlands	14	.03	.035	.03
SM Highlands	13	.03	.035	.03
SM Highlands	12	.03	.035	.03
SM Highlands	11	.03	.04	.03
SM Highlands	10	.03	.04	.03
SM Highlands	9	.03	.04	.03
SM Highlands	8	.03	.035	.03
SM Highlands	7.5	Culvert		
SM Highlands	7	.03	.035	.03
SM Highlands	6	.03	.035	.03
SM Highlands	5	.03	.035	.03
SM Highlands	4	.03	.035	.03
SM Highlands	3	.03	.035	.03
SM Highlands	2	.03	.035	.03
SM Highlands	1	.03	.035	.03

SUMMARY OF REACH LENGTHS

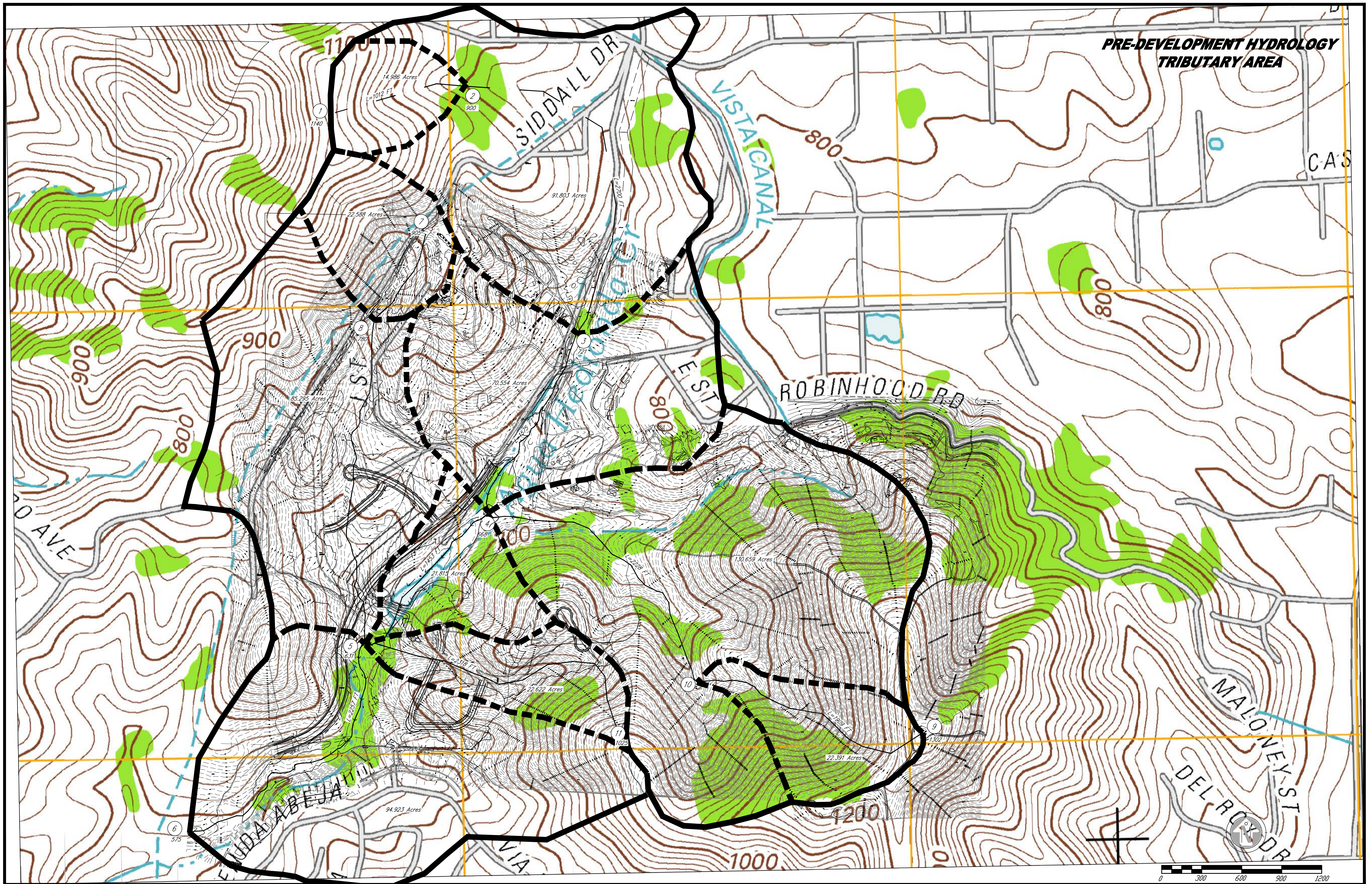
River: Agua Hedionda

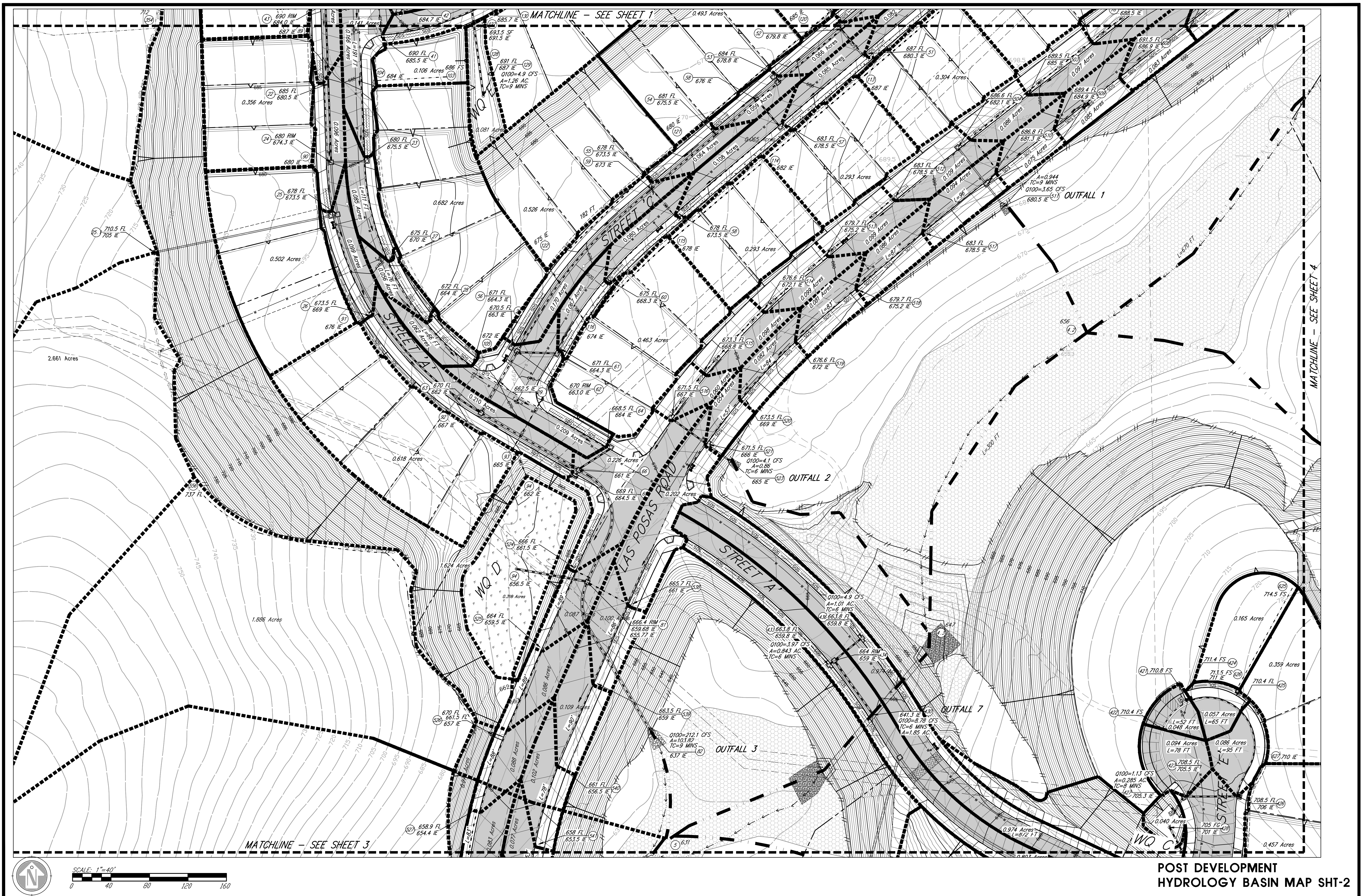
Reach	River Sta.	Left	Channel	Right
SM Highlands	18	251	201	149.5
SM Highlands	17	170	200	230
SM Highlands	16	201	201	201
SM Highlands	15	164	203	238
SM Highlands	14	336	221	89
SM Highlands	13	200	200	200
SM Highlands	12	200	200	200
SM Highlands	11	223	202	180
SM Highlands	10	138	206	267
SM Highlands	9	144	202	677
SM Highlands	8	240	202	612
SM Highlands	7.5	Culvert		
SM Highlands	7	299	226	141
SM Highlands	6	114	296	522
SM Highlands	5	249	202	154
SM Highlands	4	262	206	149
SM Highlands	3	399	240	89
SM Highlands	2	310	212	114
SM Highlands	1	0	0	0

APPENDIX 7

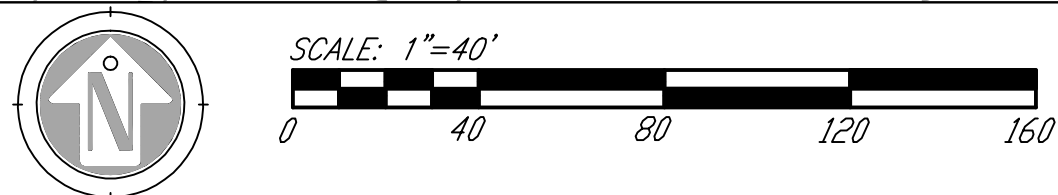
PRE- AND POST-DEVELOPMENT HYDROLOGY BASIN MAPS

**PRE-DEVELOPMENT HYDROLOGY
TRIBUTARY AREA**

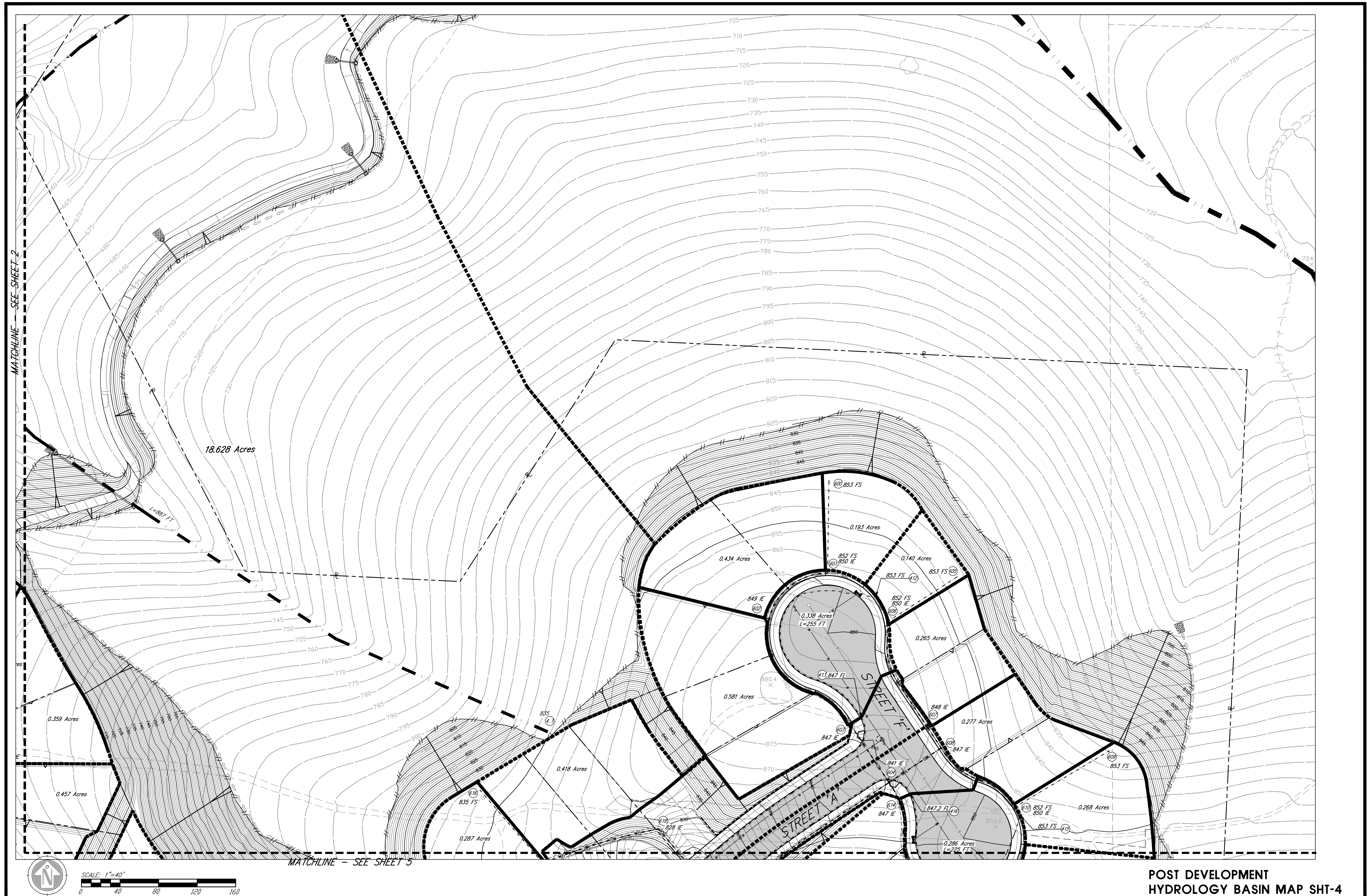




POST DEVELOPMENT HYDROLOGY BASIN MAP SHT-2



POST DEVELOPMENT
HYDROLOGY BASIN MAP SHT-3



POST DEVELOPMENT HYDROLOGY BASIN MAP SHT-4

**OVERALL
POST-DEVELOPMENT
HYDROLOGY TRIBUTARY AREA**

