

Noise Technical Report for the Castlerock Project, City of San Diego, California

Prepared for

Prepared by

Pardee Homes 6025 Edgewood Bend Court San Diego, CA 92130 Contact: Jimmy Ayala RECON Environmental, Inc.

1927 Fifth Avenue

San Diego, CA 92101-2358

P 619.308.9333 F 619.308.9334

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Jessica Fleming, Acoustical Analyst

Jessien Horning

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# 1.0 Summary

The proposed Castlerock project is located adjacent to Mast Boulevard between Fanita Drive and West Hills Parkway in the city of San Diego at the border of San Diego and the city of Santee. Because the project site is located adjacent to the city of Santee's western boundary and services could logically be provided by Santee, annexation to the City of Santee is being sought. Annexation is the preferred option ("Annexation Scenario"). The proposed project could be developed in the City of San Diego without annexation to the City of Santee with a few modifications. Therefore, this report also includes a discussion of the project without annexation to the City of Santee ("No Annexation Scenario").

The proposed project would construct 283 detached single-family residences, 147 detached small lot units (referred to as "green court" units), approximately 4.09 acres of public parks, 0.64 acre (0.49 acre usable) of pocket parks, a pedestrian trail, and public streets and private driveways on an undeveloped 203.6-acre site, within the East Elliott Community Plan. The remainder of the property would remain undisturbed as open space, except for small areas needed for brush management.

The No Annexation Scenario would involve slight changes in the land uses with 282 detached single-family residences and 140 detached small lot units.

This report analyzes impacts to the proposed residential lots from future traffic noise generated on Mast Boulevard, as well as from other noise sources in the area. Impacts are assessed in accordance with the guidelines, policies, and standards established by the City of San Diego and the City of Santee. Measures are recommended, as required, to reduce significant impacts to noise-sensitive areas.

# 1.1 Traffic Noise

Construction of noise barriers ranging from three to four feet high along the southern pad edge as detailed below will result in noise levels for ground-floor exterior usable areas below 65 community noise equivalent level (CNEL) for both the Annexation and the No Annexation Scenarios. With construction of the proposed barriers, ground-floor noise levels at exterior usable areas throughout the project site will be at or below 65 CNEL.

Even with the construction of the proposed barriers, first-, and second-floor exterior noise levels could exceed 60 CNEL for the residential units adjacent to Mast Boulevard for both the Annexation and the No Annexation Scenarios. For the single-family residential units on these pads, the City of San Diego assumes that typical light-frame

construction will provide 15 decibels of noise reduction. If exterior levels are above 60 CNEL, therefore, the interior level may exceed the City of San Diego's 45 CNEL standard.

Thus, at the time that building plans are available for the affected units detailed below, and prior to the issuance of building permits, a detailed acoustical analysis will be required ensuring that interior noise levels due to exterior sources will be below the 45 CNEL standard. The analysis shall consider the first-, and second-floor habitable rooms of the identified residential units along Mast Boulevard.

Additionally, where exterior noise levels are projected to exceed 60 CNEL (residential units along Mast Boulevard), it will be necessary for the windows to be closed in order to achieve the necessary exterior to interior noise reduction. Consequently, the design for these affected units shall include a ventilation or air conditioning system to provide a habitable interior environment when the windows are closed.

# 1.2 High School

There is a high school stadium adjacent to the project that is located within the city of Santee. Noise from football stadium activities at the high school may result in periodic temporary noise at the proposed residential units. As discussed below, noise impacts would be less than significant and no mitigation is required.

# 1.3 Construction Noise

Construction shall be limited to the hours of 7:00 A.M. to 7:00 P.M. Monday through Saturday as stated in the City of San Diego and the City of Santee's Noise Abatement and Control Ordinances. In accordance with the noise ordinances, no construction shall take place on Sundays or on legal holidays, as specified in Section 21.04 of the San Diego Municipal Code and Section 8.12.290 of the Santee Municipal Code, with the exception of Columbus Day and George Washington's Birthday.

Compliance with the City of San Diego and the City of Santee's noise ordinances will ensure that construction noise impacts are not significant.

# 1.4 Sycamore Landfill

Noise levels due to operations at the Sycamore Landfill would not exceed the applicable limits of 62.5 dB(A)  $L_{\rm eq}$  during the day, 60.0 dB(A)  $L_{\rm eq}$  in the evening, and 57.5 dB(A)  $L_{\rm eq}$  during the night at the landfill property boundary. Noise impacts would not be significant.

#### 1.5 Sewer Lift Station

Under the No Annexation Scenario, a new City of San Diego sewer lift station would be required and is proposed to be located at the corner of Street A and the emergency access road. Noise generated by the sewer lift station could result in potential noise impacts to future residents of the proposed project. Implementation of mitigation discussed below would reduce impacts from the sewer lift station to a level below significant for the No Annexation Scenario.

# 1.6 MCAS Miramar Air Traffic

Marine Corps Air Station (MCAS) Miramar is located approximately seven miles west of the project site. The project site is located well outside the 60 CNEL noise contour line published by the <u>U.S. Marine Corps and the U.S. Departments of the Air Force, the Army, and the Navy.</u> Impacts due to air traffic at MCAS Miramar would be less than significant.

# 2.0 Introduction

The proposed Castlerock project is located adjacent to Mast Boulevard in the city of San Diego at the border of San Diego and the city of Santee. Figure 1 shows the regional location of the project. Figure 2 shows an aerial photograph of the project site. Figure 3 shows the proposed vesting tentative map for the project. The proposed project would construct 283 detached single family residences and 147 single-family detached units clustered on larger lots (referred to as "green court" units). The No Annexation Scenario would involve slight changes in the land uses with 282 detached single-family residences and 140 green court units. For the purposes of this noise analysis, all units were considered to be single-family units. For both scenarios, the lot plan adjacent to Mast Boulevard would be the same.

This report analyzes impacts to the proposed residential units from future traffic noise generated on Mast Boulevard, as well as from other area noise sources. Impacts are assessed in accordance with the guidelines, policies, and standards established by the City of San Diego and the City of Santee. Measures are recommended, as required, to reduce significant impacts to noise-sensitive areas.

The analysis is based on traffic figures projected in the project traffic report (Urban Systems Associates, Inc. 2011).

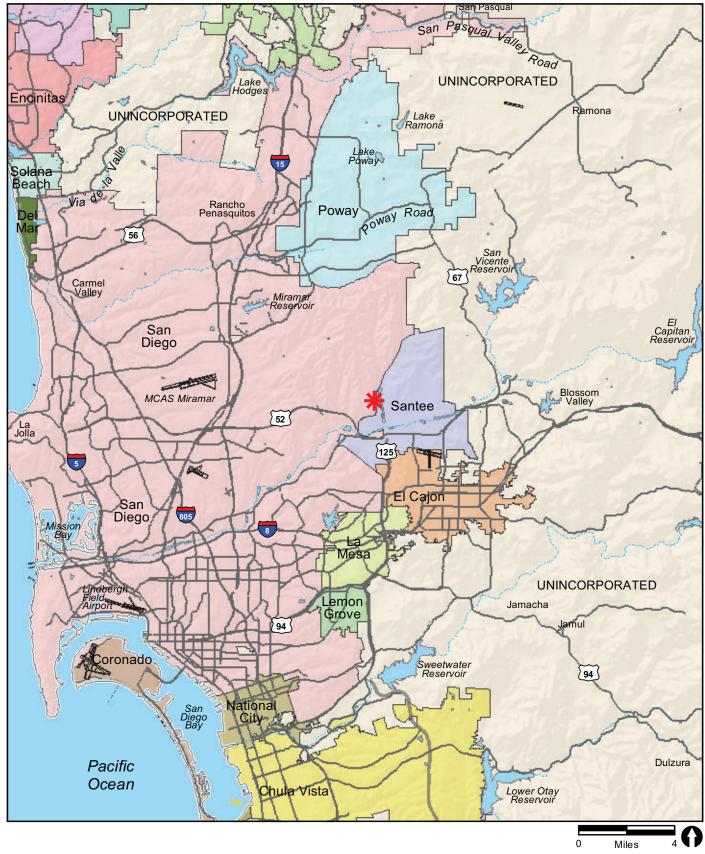
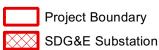






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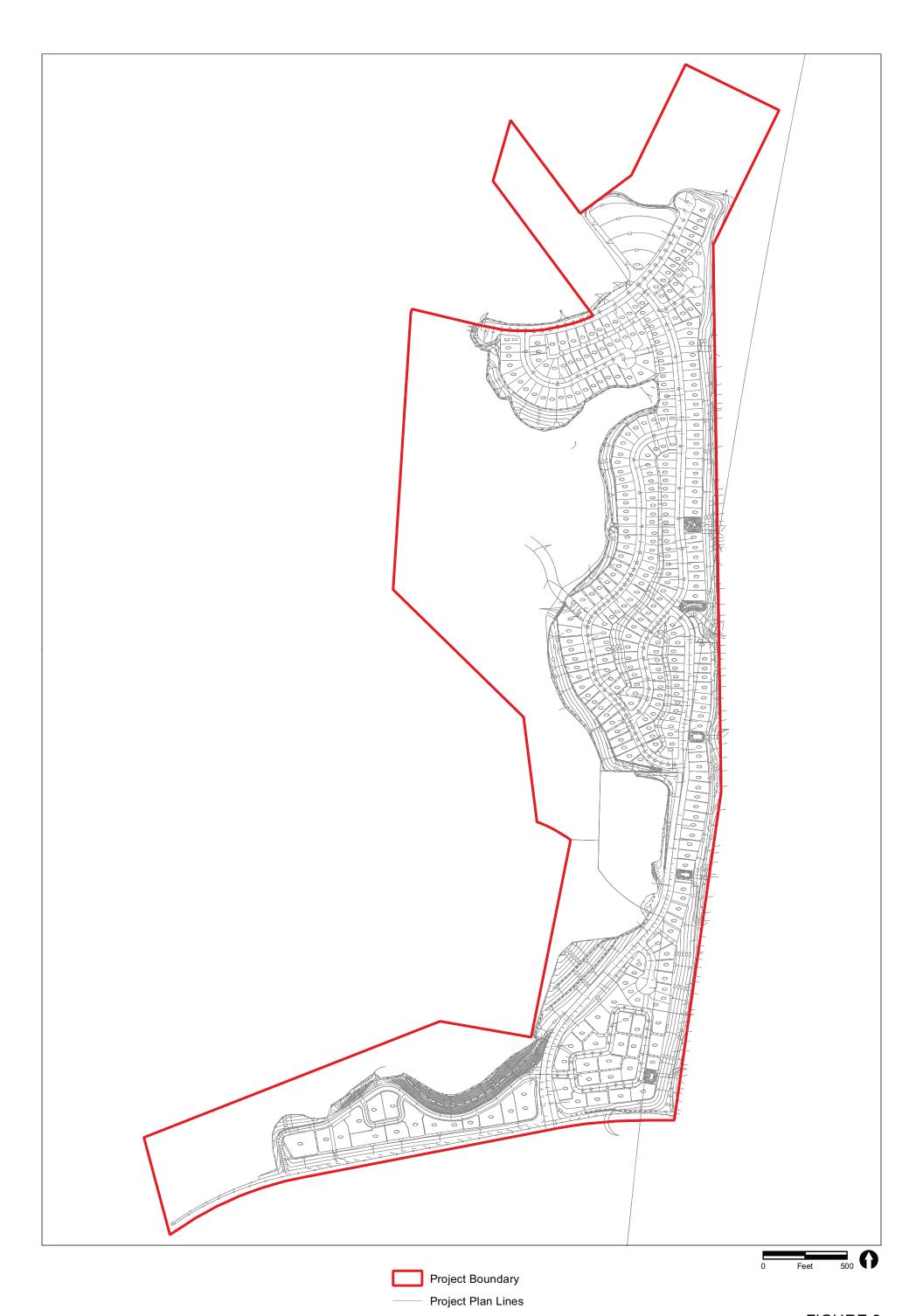




FIGURE 3

# 3.0 Analysis Methodology

# 3.1 Applicable Standards and Definitions of Terms

The hourly equivalent sound level ( $L_{eq(1)}$ ) is the average A-weighted decibel [dB(A)] sound level over a one-hour period. The CNEL is a 24-hour A-weighted average sound level [dB(A)  $L_{eq}$ ] from midnight to midnight obtained after the addition of 5 dB to sound levels occurring between 7:00 P.M. and 10:00 P.M. and of 10 dB to the sound levels occurring between 10:00 P.M. and 7:00 A.M. A-weighting is a frequency correction that often correlates well with the subjective response of humans to noise. Adding 5 dB and 10 dB to the evening and nighttime hours, respectively, accounts for the added sensitivity of humans to noise during these time periods.

In general, the noise level standards established by the City of San Diego are more restrictive than those established by the City of Santee. Therefore, for a conservative analysis, impacts to future sensitive receivers under both the Annexation and the No Annexation Scenarios were evaluated in relation to the noise level standards promulgated in the City of San Diego General Plan (2008) and the City Noise Abatement and Control Ordinance. The only exception is the high school stadium located adjacent to the project site. The high school is located within the city of Santee and noise from the stadium is governed by the City of Santee Municipal Code.

**City of San Diego.** The City of San Diego's exterior noise level standard for single-family residences and neighborhood parks is 65 CNEL, and the City's interior noise level standard for single family residences is 45 CNEL.

The City of San Diego assumes that standard construction techniques will provide a 15-dB reduction of exterior noise levels to an interior receiver. With these criteria, standard construction could be assumed to result in interior noise levels of 45 CNEL or less when exterior sources are 60 CNEL or less. When exterior noise levels are greater than 60 CNEL, consideration of specific construction techniques is required.

The Sycamore Landfill is located directly west of the project site in the city of San Diego. Noise from the landfill is governed by the City of San Diego Municipal Code. The standard for industrial uses is an hourly noise level 75 dB(A)  $L_{eq}$  not to be exceeded anytime. The standard for residential uses is 50 dB(A)  $L_{eq}$  from 7:00 A.M. to 7:00 P.M., 45 dB(A)  $L_{eq}$  from 7:00 P.M. to 10:00 P.M., and 40 dB(A)  $L_{eq}$  from 10:00 P.M. to 7:00 A.M. The City's Noise Abatement and Control Ordinance also states that the sound level limit at a location on the boundary between two zoning districts is the arithmetic mean of the respective limits for the two district. Therefore, the noise level limits for the Sycamore Landfill adjacent to the proposed project are 62.5 dB(A)  $L_{eq}$  from 7:00 A.M. to 7:00 P.M.,

60 dB(A)  $L_{\rm eq}$  from 7:00 P.M. to 10:00 P.M., and 57.5 dB(A)  $L_{\rm eq}$  from 10:00 P.M. to 7:00 A.M.

Construction noise is also governed by the City of San Diego Municipal Code. Section 59.5.0404 of the City's Noise Abatement and Control Ordinance states that:

- A. It shall be unlawful for any person, between the hours of 7:00 P.M. of any day and 7:00 A.M. of the following day, or on legal holidays as specified in Section 21.04 of the San Diego Municipal Code, with exception of Columbus Day and Washington's Birthday, or on Sundays, to erect, construct, demolish, excavate for, alter or repair any building or structure in such a manner as to create disturbing, excessive or offensive noise . . . .
- B. ... it shall be unlawful for any person, including the City of San Diego, to conduct any construction activity so as to cause, at or beyond the property lines of any property zoned residential, an average sound level greater than 75 decibels during the 12-hour period from 7:00 A.M. to 7:00 P.M.

**City of Santee.** There is a high school stadium adjacent to the project that is located within the city of Santee. Noise from the stadium is governed by the City of Santee Municipal Code. Section 8.12.360 of the Santee Municipal Code exempts "those reasonable sounds emanating from authorized school bands, school athletic and school entertainment events."

In addition, construction noise is governed by the City of Santee Noise Abatement and Control Ordinance (Chapter 8.12 of the Santee Municipal Code). It states that:

... it shall be unlawful for any person to operate any single or combination of powered construction equipment at any construction site on Mondays through Saturdays except between the hours of 7:00 A.M. and 7:00 P.M.

No construction is allowed, except under emergency conditions, on Sundays and holidays. Additionally,

No such equipment, or combination of equipment regardless of age or date of acquisition, shall be operated so as to cause noise at a level in excess of seventy-five decibels for more than eight hours during any twenty-four-hour period when measured at or within the property lines of any property which is developed and used either in part or in whole for residential purposes.

# 3.2 Existing Noise Level Measurements

Existing noise levels at the project site were measured using two Larson-Davis Model 720 Type 2 Integrating Sound Level Meters, serial numbers 0264 and 0266. The following parameters were used:

Filter: A-weighted

Response: Fast Time History Period: 5 seconds

The meters were calibrated before the day's measurements. Four ground-floor simultaneous measurements (five feet above the ground) were made for approximately 15 minutes adjacent to Mast Boulevard. During the measurements, traffic was counted on Mast Boulevard.

# 3.3 Traffic Noise Analysis

#### 3.3.1 Traffic Parameters

Existing traffic volumes on Mast Boulevard are estimated to be 20,905 average daily traffic (ADT) from West Hills Parkway to the high school access and 21,386 ADT from the high school access to Pebble Beach Drive (Urban Systems Associates, Inc. 2011).

Future year 2030 traffic volumes for Mast Boulevard between West Hills Parkway and the high school access and for Mast Boulevard between the high school access to Pebble Beach Drive are projected to be 27,241 and 26,341 ADT, respectively, with buildout of the proposed project (Urban Systems Associates, Inc. 2011). Since the Annexation Scenario would result in eight more residential units and, therefore, slightly greater traffic volumes on area roadways when compared to the No Annexation Scenario, these year 2030 traffic volumes with buildout of the proposed project were used for calculating future traffic noise levels in this analysis.

Mast Boulevard is posted at 35 miles per hour (mph) in the project vicinity. There is a traffic signal at the intersection of Mast Boulevard and Medina Drive. An average traffic speed of 45 mph for Mast Boulevard was found to match traffic following and the noise measurement data well. This speed was used in the analysis of future traffic noise for modeling Mast Boulevard.

The traffic mix data used in the model was predominantly cars. There were no trucks observed during the measurement periods. Nevertheless, to be conservative a typical traffic mix of 97 percent cars, 2 percent medium trucks, and 1 percent heavy trucks was used for projecting future noise levels.

The internal streets and Medina Drive (see Figures 2 and 3) would not carry significant traffic and were not modeled. Also, a row of houses is located between Medina Drive and the project site.

Table 1 summarizes the future traffic parameters used in this analysis.

TABLE 1
YEAR 2030 ROADWAY TRAFFIC PARAMETERS

Roadway	ADT	Percent Autos	Percent Medium Trucks	Percent Heavy Trucks	Speed (mph)
Mast Boulevard (West Hills Pkwy to high school access)	27,241	97	2	1	45
Mast Boulevard (high school access to Pebble Beach Dr.)	26,341	97	2	1	45

The day, evening, and nighttime traffic distribution was assumed to be 77 percent daytime traffic, 10 percent evening traffic, and 13 percent nighttime traffic. With these assumptions, the CNEL is approximately two decibels above the average daytime hourly equivalent noise level.

# 3.3.2 Analysis of Traffic Noise

Noise generated by future traffic was projected using the Federal Highway Administration Traffic Noise Model (TNM) Version 2.5. The TNM program calculates noise levels at selected receiver locations using input parameter estimates such as projected hourly average traffic rates; vehicle mix, distribution, and speed; roadway lengths and gradients; distances between sources, barriers, and receivers; and shielding provided by intervening terrain, barriers, and structures.

Locations and elevations of the project site and adjacent properties and roadways were obtained from computer-aided design files.

Receivers, roadways, and barriers are input into the TNM model using three-dimensional coordinates. The Y-axis pointed north and the X-axis pointed east.

The TNM model allows the user to choose from a number of ground conditions. As seen in the aerial photograph shown in Figure 2, the project site is currently vacant undeveloped land. For this reason, hard soil conditions were assumed in the modeling of noise measurement conditions. Pavement ground conditions were assumed for the analysis of future conditions, since a large portion of the site between the roadways and the structures would be paved. The average annual temperature in the project area is 65 degrees Fahrenheit. The average relative humidity was assumed to be 69 percent

based on the yearly average humidity at Lindbergh Field (Western Regional Climate Center 2010).

Exterior traffic noise levels to first- and second-floor receivers were calculated. Calculations were completed for a daytime hour, and the resulting hourly  $L_{eq}s$  were weighted and combined into CNEL values. Projected CNEL values based on the traffic distributions used here are approximately 2 dB higher than the daytime hourly  $L_{eq}$  calculated by TNM, as indicated above.

# 4.0 Existing Conditions

The existing project site is currently undeveloped. There is a substation adjacent to the project that will remain (see Figure 2 and 3). The areas south and east of the project site are developed residential land and a high school, and the areas to the north and west of the project site are undeveloped (see Figure 2). Mast Boulevard lies on the project's southern boundary. A high school exists to the south of the project site. Mast Boulevard is a four-lane prime arterial with a posted speed limit of 35 mph.

Noise measurements were taken on the project site on Wednesday, May 5, 2004 between the hours of 1:01 P.M. and 2:44 P.M. The weather was hot and sunny with a slight breeze. A total of four 15-minute measurements were made on the project site as described below. The primary source of on-site noise was due to traffic on Mast Boulevard. The locations of the measurements are shown on Figure 4 and the noise measurement data are contained in Attachment 1.

Measurement 1 was located near the north end of Medina Drive on the east side of the project area. It was located approximately where future pad edges would be. During the 15-minute measurement period, the average noise level was 40.2 dB(A) at location 1. Traffic was counted on Medina Drive during the measurement interval. Three cars was the total count.

Measurements 2 and 3 were located adjacent to Mast Boulevard. Measurement 2 was 50 feet north of the Mast Boulevard centerline while Measurement 3 was 90 feet north of the Mast Boulevard centerline. These measurements were taken near each other to assist with modeling existing noise conditions at the project site. Noise levels were measured simultaneously at these two locations. Traffic was also counted on Mast Boulevard during the measurement interval. Table 2 summarizes the results of the traffic counts taken during Measurements 2 and 3.

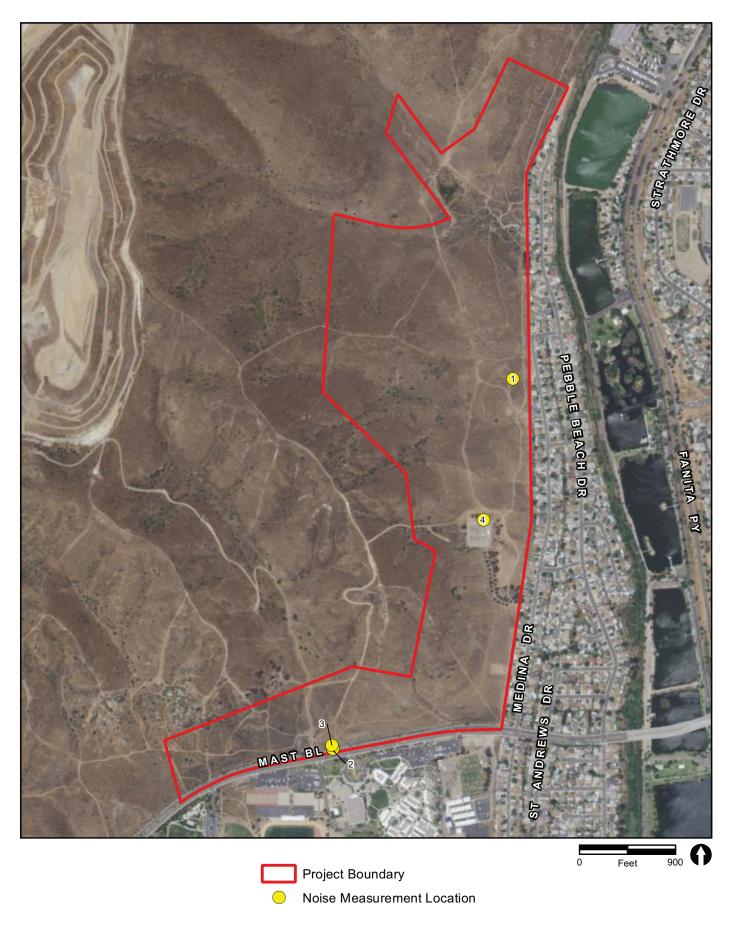




TABLE 2
15-MINUTE TRAFFIC COUNTS

	Cars	Medium Trucks	Heavy Trucks	Buses	Motorcycles
Mast Boulevard (westbound)	77	0	0	1	1
Mast Boulevard (eastbound)	117	0	0	0	2

During the 15-minute measurement period, the average noise level was 67.1 dB(A) at location 2 and 64.1 dB(A) at location 3.

Measurement 4 was located adjacent to the north end of the substation. During the 15-minute measurement period, the average noise level was 45.3 dB(A), due to the substation and ambient noise.

The results of the noise measurements are summarized in Table 3.

TABLE 3
COMPARISON OF MEASURED AND MODELED NOISE LEVELS

Measurement	Measured Noise Levels [dB(A) $L_{eq}$ ]	Modeled Noise Levels [dB(A) $L_{eq}$ ]	Difference
1	40.2	Not modeled	
2	67.1	66.6	-0.5
3	64.1	63.7	-0.4
4	45.3	Not modeled	

To determine whether the computer-modeled parameters to be used were reasonable, the TNM model was run for measurement locations 2 and 3 with the observed traffic volumes and mixes for Mast Boulevard indicated in Table 2. The TNM model was not run for measurement locations 1 and 4 because noise levels were not due to traffic volumes on a specific road, but rather ambient background noise.

For this project site, pavement ground conditions were assumed for modeling noise measurement locations 2 and 3 (see Figure 4).

The model output should be close to the same level as the measured value if the model is accurately representing the existing physical conditions. TNM input and output data for modeling the measured conditions are provided in Attachment 2.

The average traffic speed on Mast Boulevard was varied until the TNM output reasonably matched the measured noise levels. As indicated previously, the average

traffic speed for Mast Boulevard that resulted in good agreement with the measurements was 45 mph. This modeled speed also fell within the range of speeds observed by traffic following.

Table 3 shows the measured noise levels compared with the modeled noise levels using these assumptions. From Table 3 it can be seen that the modeled parameters in TNM result in relatively good agreement between the measured and modeled noise levels (within 1 dB). Therefore, the parameters used in TNM for modeling the existing conditions are reasonable.

# 5.0 Future Acoustical Environment and Impacts

The methods used in the analysis of future conditions are described in the Analysis Methodology section of this report. Traffic parameters used are specified in Table 1 above.

# 5.1 Traffic Noise Analysis

Noise levels were modeled for a series of receivers located throughout the project area to determine the future noise contours over the project site due to traffic on the area roadways.

TNM input and output are provided in Attachment 3. The resulting noise contours at five feet above the ground are shown in Figure 5. These noise contours include the effects of future grading on the property. The noise contours do not take into account any noise mitigation measures or shielding provided by the proposed buildings. Pavement conditions were used in modeling noise levels at these receivers.

As seen from Figure 5, future traffic noise levels are projected to exceed 65 CNEL at the residences located adjacent to Mast Boulevard.

To refine the model, noise levels were also modeled at 20 locations at the residences adjacent to Mast Boulevard. Pavement conditions were assumed for these receivers. TNM input and output are provided in Attachment 4. Figure 6 shows the locations of these modeled receivers. As stated above, the lot configuration adjacent to Mast Boulevard for both scenarios would be the same.

Table 4 provides the future projected noise levels at these receiver locations. As shown in this table, future noise levels adjacent to Mast Boulevard are projected to exceed 65

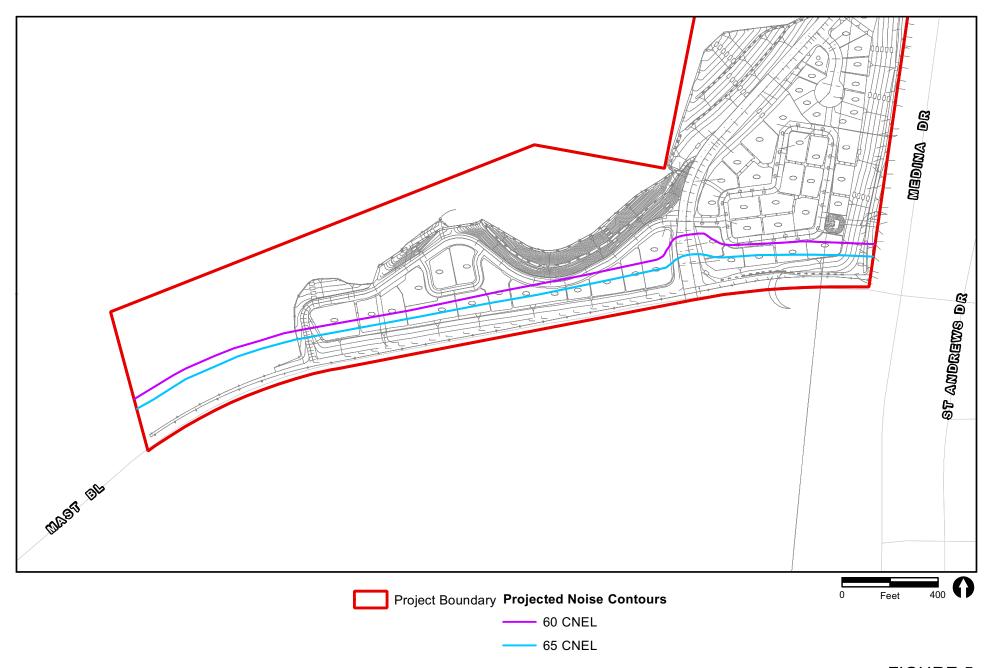


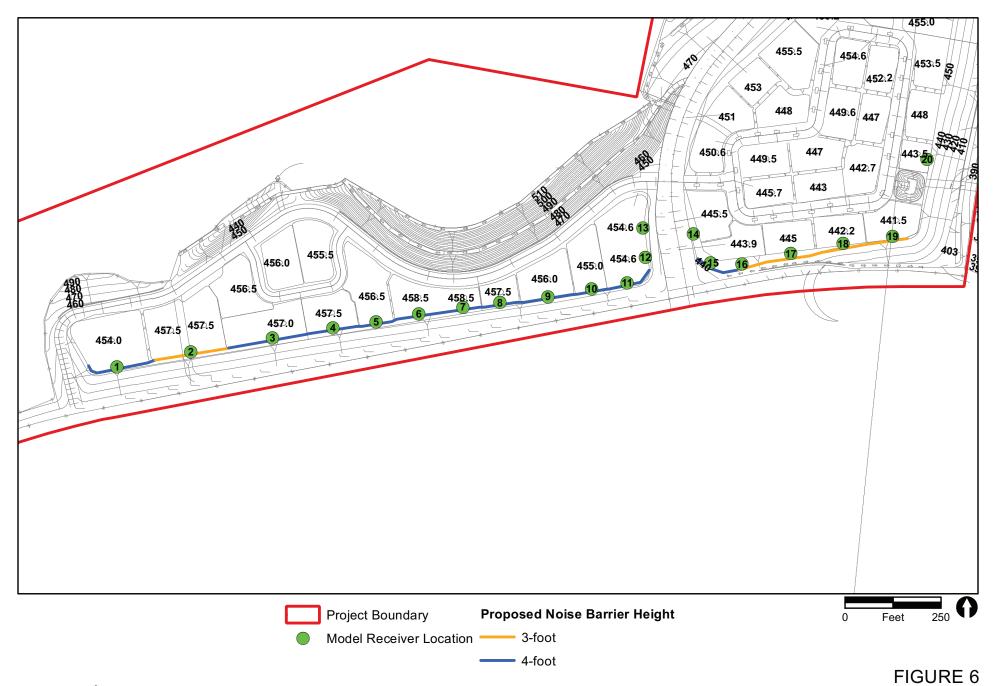


FIGURE 5
Future Projected Noise Contours

TABLE 4
FUTURE TRAFFIC-GENERATED NOISE LEVELS

Receiver _	Projected Noise Level with No Constructed Noise Barriers (CNEL) First-Floor Second-Floor		Projected Noise Level with Constructed Noise Barriers (CNEL)		
Number	First-Floor	Second-Floor	First-Floor	Second-Floor	
1	68	67	62	67	
2	68	68	65	68	
3	68	68	62	68	
4	68	68	62	68	
5	69	68	63	68	
6	69	69	63	69	
7	69	69	63	69	
8	69	69	63	69	
9	70	70	65	70	
10	70	70	64	70	
11	70	70	64	70	
12	65	66	64	65	
13	61	62	61	61	
14	63	64	63	63	
15	69	69	65	69	
16	70	70	65	70	
17	69	69	64	69	
18	69	68	63	68	
19	68	67	62	67	
20	59	59	59	59	

**BOLD** = exceeds 65 CNEL





CNEL at the residences located adjacent to Mast Boulevard (Receivers 1 through 11 and 15 through 19) without mitigation.

# 5.2 High School

Noise from football stadium activities at the high school may result in periodic temporary noise at the proposed residential units. The football stadium is located approximately 640 feet south of the nearest project residence. Loudspeaker noise levels at a typical high school football stadium during a game have been found to generate 77.5 dB(A) at 60 feet from the speakers (RECON 2003). This noise level would reduce to approximately 57 dB(A) at a distance of 640 feet. The periodic noise from the football stadium may be perceived as "nuisance noise" by future residents. The City of Santee Municipal Code exempts noise from the stadium and, therefore, noise resulting from the stadium is not considered a significant impact.

# 5.3 Construction Noise

Noise associated with the earthwork, construction, and surface preparation of the proposed project will result in short-term, temporary impacts to the existing residences to the east of the project site. A variety of noise-generating equipment would be used during the construction phase of the project such as scrapers, dump trucks, backhoes, front-end loaders, jackhammers, and concrete mixers, along with others.

Table 5 indicates the types of construction equipment typically involved in construction projects. This type of equipment can individually generate noise levels that range between 77 and 91 dB(A) at 50 feet from the source, as listed in Table 5. Ground-clearing activities generally generate the greatest average construction noise levels. These activities are estimated to generate average noise levels of 83 to 84 dB(A) L<sub>eq</sub> 50 feet from the site of construction (Bolt, Beranek, and Newman, Inc. 1971). This value is based on empirical data on the number and types of equipment at a construction site and their average cycle of operation.

TABLE 5
MEASURED NOISE LEVELS OF
COMMON CONSTRUCTION EQUIPMENT

	Approximate Noise
Equipment	Level (dBA)
Air compressor	81
Backhoe	85
Concrete Mixer	85
Dozer	80
Generator	78
Grader	85
Jackhammer	88
Loader	79
Paver	89
Pneumatic tool	86
Saw	78
Scraper	88
Truck	91

SOURCE: Bolt, Beranek, and Newman 1971. NOTE: Noise levels at 50 feet from the source.

Construction noise generally can be treated as a point source and would attenuate at approximately 6 dB(A) for every doubling of distance. A noise level of 84 dB(A)  $L_{\rm eq}$  would attenuate to 75 dB(A)  $L_{\rm eq}$  at approximately 150 feet from the noise source.

Construction activities, such as grading, which generate the loudest noise levels will occur over the entire site and would not be situated at any one location for a long period of time. Therefore, the acoustic center of the construction activity was assumed to be the center of the project site. As can be seen in Figure 2, existing single-family homes are a minimum of 170 feet to the east of the center of the project site. Therefore, construction noise levels are anticipated to be below City standards.

As discussed above, Section 59.5.0404 of the City of San Diego's Noise Ordinance states that average construction noise levels may not exceed 75 decibels during the 12-hour period from 7:00 A.M. to 7:00 P.M. Furthermore, construction is prohibited between 7:00 P.M. and 7:00 A.M. on Sundays, and on legal holidays, as specified in Section 21.04 of the San Diego Municipal Code, with exception of Columbus Day and Washington's Birthday.

In addition, the City of Santee Noise Abatement and Control Ordinance (Chapter 8.12 of the Santee Municipal Code) states that:

... it shall be unlawful for any person to operate any single or combination of powered construction equipment at any construction site

on Mondays through Saturdays except between the hours of 7:00 A.M. and 7:00 P.M.

No construction is allowed, except under emergency conditions, on Sundays and holidays. Additionally,

No such equipment, or combination of equipment regardless of age or date of acquisition, shall be operated so as to cause noise at a level in excess of seventy-five decibels for more than eight hours during any twenty-four-hour period when measured at or within the property lines of any property which is developed and used either in part or in whole for residential purposes.

# 5.4 Sycamore Landfill Expansion

The Sycamore Canyon Landfill is located about 1,700 feet west of the project site on the opposite side of a ridgeline. The landfill project proposes the construction of 15-foot-high noise berms at all landfill property boundaries including across the ridgeline that separates the landfill from the Castlerock project site once the height of the landfill reaches 850 feet above mean sea level.

The City of San Diego noise ordinance applicable limits at the landfill boundary are  $62.5 \text{ dB(A)} \text{ L}_{eq}$  during the day,  $60 \text{ dB(A)} \text{ L}_{eq}$  in the evening, and  $57.5 \text{ dB(A)} \text{ L}_{eq}$  during the night. Noise at the Sycamore landfill boundary would not exceed 62.5 dB(A) Leq during the day, 60.0 dB(A) Leq in the evening, and 57.5 dB(A) Leq during the night with the berms in place (Gorden Bricken and Associates 2006). Additionally, these noise levels would attenuate to 31.9 dB(A) Leq during the day, 29.4 dB(A) Leq in the evening, and 26.9 dB(A) L<sub>eq</sub> during the night at the project site. These noise levels are well below the applicable noise ordinance standards. Additionally, as currently proposed, the Landfill Expansion Master Plan Final EIR sets forth mitigation measures (to be implemented when adjacent residential development occurs), which require that operations at the landfill at night shall be at least 200 feet from the landfill property boundary. Truck hauling would not exceed applicable limits and would be required to stay at least 150 feet from the property boundary during the day, 200 feet from the landfill property boundary in the evening, and 325 feet from the landfill property boundary during the night. Construction of the landfill expansion would occur only in the daytime hours and would not exceed limits. Thus, noise generated by the Sycamore Landfill would not impact future residents of the proposed project.

#### 5.5 Sewer Lift Station

The topography of the Castlerock project site prevents gravity service directly to the City's METRO interceptor. Therefore, under the No Annexation Scenario, a new City of San Diego sewer lift station would be required and is proposed to be located at the corner of Street A and the emergency access road. The pump station would consist of a 28-foot-by-25-foot building of block wall construction housing two 25-horsepower pumps. Noise generated by the sewer lift station could result in noise levels that exceed the City of San Diego's noise ordinance. The Annexation Scenario would not require a sewer lift station.

### 5.6 MCAS Miramar Air Traffic

MCAS Miramar is located approximately seven miles west of the project site. The air traffic at MCAS Miramar includes rotary (helicopter) and fixed-wing (other military aircraft) traffic. The project site is downwind of the MCAS landing pattern and Field Carrier Landing Practice Flight Corridors for fixed-wing operations. The project site is also located adjacent to the downwind leg of the Field Carrier Landing Practice pattern and directly underneath the Yuma-Sycamore flight corridors for rotary-wing aircraft arriving from and departing to the east. Noise levels due to this air traffic were obtained from the Air Installations Compatible Use Zone document published by the U.S. Marine Corps and U.S. Department of Navy (2005). noise contours published by the U.S. Departments of the Air Force, the Army, and the Navy (1996). The project site is located well outside the 60 CNEL noise contour line. Therefore, impacts due to air traffic at MCAS Miramar are less than significant.

# 6.0 Mitigation

As discussed above, implementation of the project is anticipated to result in significant noise impacts due to traffic noise from Mast Boulevard. In addition, for the No Annexation Scenario, impacts from the required sewer lift station would also be potentially significant. Compliance with the City of San Diego noise ordinance would reduce potential construction noise impacts to below a level of significance. With implementation of the mitigation measures discussed below, all potential noise impacts would be reduced to less than significant.

#### 6.1 Traffic Noise

As discussed above, exterior noise levels at residences located adjacent to Mast Boulevard were projected to exceed 65 CNEL. Construction of noise barriers ranging from three to four feet high along the southern pad edge as shown in Figure 6 will result in ground floor noise levels at or below 65 CNEL for both the Annexation and the No Annexation Scenarios. Noise barrier heights are relative to the pad elevations as illustrated in Figure 6.

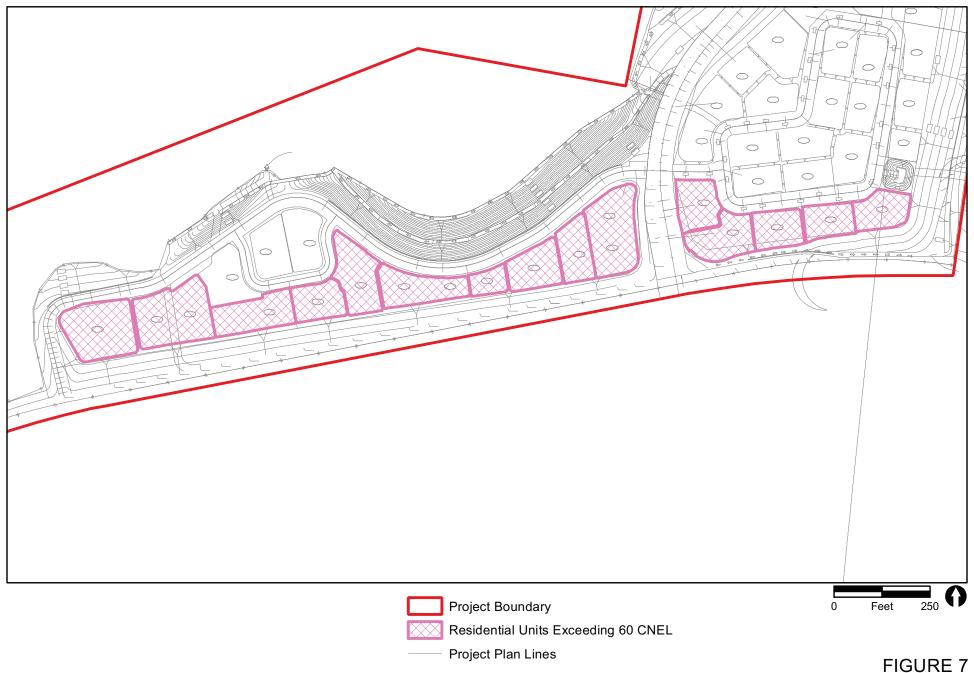
Table 4 shows the resulting noise levels at the modeled receivers after construction of noise barriers. The TNM input and output for modeling the noise barriers are contained in Attachment 4.

The effectiveness of a barrier is dependent upon the quality of construction and the barrier material mass and acoustical properties. Barriers should be free of cracks and holes. The transmission loss through a barrier should be at least 10 decibels greater than the estimated barrier attenuation (Federal Highway Administration 1979:34). If a barrier attenuates noise levels by 5 dB(A) at a receiver location, the barrier transmission loss must be at least 15 dB(A) to prevent audible noise from traveling through the barrier and adding to the acoustical environment. Examples of acceptable barrier materials include, but are not limited to, masonry block, wood frame with stucco, 0.5-inch-thick Plexiglas, or 0.25-inch-thick plate glass. If transparent barrier materials are used, no gaps should occur between the panels.

As seen in Table 4, even with the construction of the proposed barriers, both first- and second-floor exterior noise levels are projected to exceed 60 CNEL for the residential units adjacent to Mast Boulevard for both the Annexation and the No Annexation Scenarios. For single-family residential units on these pads, the City assumes that typical light-frame construction will provide 15 decibels of noise reduction. If exterior levels are above 60 CNEL, therefore, the interior level may exceed the City's 45 CNEL standard.

Thus, at the time that building plans are available for the affected residential units along Mast Boulevard (Figure 7), and prior to the issuance of building permits, a detailed acoustical analysis will be required ensuring that interior noise levels due to exterior sources will be below the 45 CNEL standard. The analysis shall consider the first- and second-floor habitable rooms of the identified units along the southern pad edges adjacent to Mast Boulevard.

Additionally, where exterior noise levels are projected to exceed 60 CNEL (along the southern pad edges adjacent to Mast Boulevard as indicated in Figure 7), it will be necessary for the windows to be closed in order to achieve the necessary exterior to interior noise reduction. Consequently, the design for these affected units shall include





Residential Units Exceeding 60 CNEL

a ventilation or air conditioning system to provide a habitable interior environment when windows are closed.

## 6.2 Construction Noise

Construction shall be limited to the hours of 7:00 A.M. to 7:00 P.M. Monday through Saturday as stated in the City of San Diego and the City of Santee's Noise Abatement and Control Ordinances. In accordance with the noise ordinances, no construction shall take place on Sundays or on legal holidays, as specified in Section 21.04 of the San Diego Municipal Code and Section 8.12.290 of the Santee Municipal Code, with the exception of Columbus Day and George Washington's Birthday.

Compliance with the City of San Diego and the City of Santee's noise ordinances will ensure that construction noise impacts at the residences to the east are not significant.

#### 6.3 Sewer Lift Station

Prior to the issuance of a building permit for the sewer lift station at the intersection of Street A and the emergency access road, the applicant shall submit building plans to the City Engineer. The lift station shall be designed to be at or below the allowable decibel level at the property line. An acoustical study shall be performed that would confirm engineering and architectural design and materials would reduce noise levels from the lift station to below 40 dB(A) L<sub>eq</sub> at the property line per San Diego Municipal Code 59.5.0401.

Implementation of this mitigation would reduce impacts from the sewer lift station to a level below significant for the No Annexation Scenario.

# 7.0 References Cited

Bolt, Beranek, and Newman, Inc.

1971 Noise from Construction Equipment and Operations, Building Equipment, and Home Appliances. Prepared for the U.S. Environmental Protection Agency, Office of Noise Abatement and Control. NTID300.1. December 31. Cambridge, Mass.

Federal Highway Administration

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#### Gordon Bricken and Associates

2006 Noise Technical Report prepared for the Sycamore Canyon Landfill Expansion.

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2003 Noise Technical Report for Maranatha High School, County of San Diego, California. RECON Number 3457N. June 30.

#### Urban Systems Associates

2011 Transportation Analysis for Castlerock. Prepared for Pardee Homes. February 14.

#### U.S. Departments of the Air Force, the Army, and the Navy

- 1996 Realignment of NAS Miramar Environmental Impact Statement. Prepared by Ogden Environmental and Energy Services. February.
- 2005 Marine Corps Air Station, Miramar AICUZ Update. Air Installations Compatible Use Zones. Revised March 2005.

#### Western Regional Climate Center

2010 Western U.S. Climate Historical Summaries: http://www.wrcc.dri.edu/cgi-bin/cliMAIN.pl?ca2706 and http://www.wrcc.dri.edu/cgi-bin/clilcd.pl?ca23188. Accessed October 18.

# **ATTACHMENTS**

# ATTACHMENT 1 Noise Measurement Data

#### KEY TO FILE CODES

#### ATTACHMENT 1

Meter 264 Measurement Location 3 (at five feet high)

Meter 266 Measurement Locations 1, 2, and 4 (at five feet high)

C:\NOISE\LARDAV\SLMUTIL\05MAY\_13.bin Interval Data

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Measurement 1	0	05May 04	13:01:10	49.9	42.0	59.0	53.3	36.6	78.0	0.0
0	Ō	05May 04	13:02:00	60.0	38.3	56.1	45.1	36.1	56.1	0.0
0	0	05May 04	13:03:00	60.0	41.5	59.3	48.3	37.0	58.9	0.0
0	0	05May 04	13:04:00	60.0	40.1	57.9	48.7	35.6	60.3	0.0
0	0	05May 04	13:05:00	60.0	39.8 43.0	5/.5	44.Z	3/.6	57.U 67.1	0.0
0	0	05May 04	13.00.00	60.0	38.0	55.7	42.2	36.5	54.0	0.0
0	Ö	05May 04	13:08:00	60.0	42.4	60.2	51.1	37.0	62.4	0.0
0	0	05May 04	13:09:00	60.0	38.6	56.3	45.7	36.2	60.5	0.0
0	0	05May 04	13:10:00	60.0	36.3	54.1	38.7	35.0	53.9	0.0
0	0	05May 04	13:11:00	60.0	36.8	54.6	45.5	34.9	62.5	0.0
0	0	05May 04	: 13:12:00 : 13:13:00	60.0	39.4 41 4	59 2	43.9	30.5	58.7	0.0
0	Ö	05May 04	13:14:00	60.0	38.7	56.4	42.4	35.7	58.7	0.0
0	0	05May 04	13:15:00	60.0	39.0	56.7	50.3	35.7	65.1	0.0
0	0	05May 04	13:16:00	49.9 60.0 60.0 60.0 60.0 60.0 60.0 60.0 6	41.2	57.2	49.9	37.1	72.1	0.0
Measurement 2	0	05Mar 0/	1 12./2.05	54.5 60.0 60.0 60.0 60.0 60.0 60.0 60.0 60	65 0	02 1	7/ 2	17 1	06 6	0.0
0	0	05May 04	13:44:00	60.0	65.0	82.8	75.4	44.6	87.7	98.5
0	Ō	05May 04	13:45:00	60.0	66.5	84.3	73.6	44.3	86.3	0.0
0	0	05May 04	13:46:00	60.0	67.5	85.3	74.8	43.0	87.1	0.0
0	0	05May 04	13:47:00	60.0	68.9	86.7	75.0	49.1	88.6	0.0
0	0	05May 04	13:48:00	60.0	63.8	81.5	70.8	46.8	83.7	0.0
0	0	05May 04	13:49:00	60.0	64 5	82 3	75.0	49.3	86 7	98.5 0.0
0	Ö	05May 04	13:51:00	60.0	52.7	70.5	61.3	45.3	73.5	0.0
0	0	05May 04	13:52:00	60.0	72.7	90.5	88.5	47.5	101.6	108.9
0	0	05May 04	13:53:00	60.0	69.9	87.7	81.3	49.8	102.5	102.9
0	0	05May 04	13:54:00	60.0	63.3	81.1	75.2	46.0	86.3	0.0
0	0	05May 04	: 13:55:00 : 13:56:00	60.0	68 0	84.0	76.8	47.8	88.5 87.7	0.0
0	0	05May 04	13:57:00	60.0	67.0	84.7	73.5	57.8	86.6	101.0
0	0	05May 04	13:58:00	60.0	67.0	84.8	76.2	49.9	88.8	0.0
0	0	05May 04	13:59:00	60.0	64.8	82.6	75.3	47.8	87.2	98.5
0	0	05May 04	14:00:00	60.0	66.8	84.6	74.8	48.4	88.2	0.0
0	0	05May 04	14:01:00 1 14:02:00	60.0	59.9 69.5	//.6 87 3	67.8 81.8	48.4 50.5	80.5 92.6	101.0
0	0	05May 04	14:02:00	60.0	67.2	85.0	75.6	53.3	86.9	98.5
0	0	05May 04	14:04:00	55.7	62.6	80.0	72.6	47.7	84.6	98.5
Measurement 4	0	0.514	. 14 00 00	F 0 0						
0	0	05May 04	14:29:00 14:30:00 14:31:00	59.9		63.0 64.0	52.5 50.8	41.8	75.9 68.8	0.0
0	0	05May 04	14:30:00	60.0	46.5	64.3	52.2	42.9	63.9	0.0
0	Ō	05May 04	14:32:00	60.0	44.5	62.3	53.3	41.2	78.6	0.0
0	0	05May 04	14:33:00	60.0	48.0	65.8	55.4	41.9	74.8	0.0
0	0	05May 04	14:34:00	60.0	47.5	65.3	54.3	41.4	66.5	0.0
0	0	05May 04	14:35:00	60.0	46.5	64.3	53.2	42.5	64.5	0.0
0	0	05May 04	14:30:00	60.0	40.3	61 2	57.0	41.0	70 2	0.0
0	Ő	05May 04	14:38:00	60.0	43.6	61.4	50.7	40.5	69.8	0.0
0	0	05May 04	14:39:00	60.0	44.0	61.8	50.6	40.0	64.1	0.0
0	0	05May 04	14:40:00	60.0	42.6	60.3	47.4	40.3	61.5	0.0
0	0	05May 04	14:41:00	60.0	41.8	59.6	46.3	40.2	66.7	0.0
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0	Ő	05May 04	14:44:00	0.3	45.0	40.3	46.8	42.0	68.7	0.0
0	Ō	05May 04	15:54:20	60.0 60.0 60.0 60.0 60.0 60.0 60.0 60.0	47.9	62.9	65.4	38.4	83.8	0.0

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## **ATTACHMENT 2**

**TNM Input/Output—Measured Conditions** 

**INPUT: ROADWAYS** 

3536.2

**RECON Environmental** 

Jessica Fleming

RUN:

24 February 2011 TNM 2.5

INPUT: ROADWAYS

PROJECT/CONTRACT:

3536.2

Castlerock - Measured Receivers

Average pavement type shall be used unless a State highway agency substantlates the use of a different type with the approval of FHWA

		of a different type with the approval of FHWA											
Roadway		Points											
Name	Width	Name	No.	Coordinates	(pavement)		Flow Control			Segment			
				X	Y	Z	Control Device	Speed Constraint	Percent Vehicles Affected	Pvmt Type	On Struct		
	ft			ft	ft	ft		mph	%		1		
EB Mast	12.0	1	1	6,325,705.5	1,889,497.6	418.00				Average	+		
		2	2	6,326,078.5	1,889,569.5	422.00				Average			
		3	3	6,326,328.5						Average	_		
		4	4	6,326,508.0					+	Average	+		
		5	5	6,326,805.5		-				Average			
WB Mast	12.0	1	6	6,326,790.5	1,889,740.1					Average			
		2	7	6,326,493.5	1,889,684.2					Average			
		3	8	6,326,319.0	1,889,650.4					Average			
		4	9	6,326,043.5	1,889,597.5					Average			
		5	10	6,325,682.5						Average			

3536.2

**RECON Environmental** 

24 February 2011

Jessica Fleming

**TNM 2.5** 

INPUT: TRAFFIC FOR LAeq1h Volumes

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - Measured Receivers

Roadway	Points											
Name	Name		Segmen	t								
			Autos		MTruck	MTrucks		HTrucks			Motorcy	ycles
			V	S	V	S	V	S	V	S	V	S
			veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph
EB Mast	1	1	468	45							8	3 45
	2	2	468	45							8	3 45
	3	3	468	45							8	3 45
	4	4	468	45							8	3 45
	5	5										
WB Mast	1	6	308	45					4	4 45	5 4	45
	2	7	308	45					4	4 45	5 4	45
	3	8	308	45					4	4 45	5 4	45
	4	9	308	45					4	4 45	5 4	45
	5	10										

**INPUT: RECEIVERS** 

3536.2

**RECON Environmental** 

Jessica Fleming

24 February 2011

**TNM 2.5** 

INPUT: RECEIVERS

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - Measured Receivers

Re	ceiver	

Name	No.	#DUs	Coordinates	(ground)		Height	<b>Input Sou</b>	nd Levels	and Criteria	1	Active
			X	<b>Y</b>	Z	above Ground	į.	Impact Co		NR Goal	in Calc.
		f	ft	ft	ft	ft	dBA	dBA	dB	dB	
2	3	1	6,326,295.0	1,889,678.9	427.00	5.00	0.00	66	3 10.0	8	0 Y
3	4	1	6,326,287.0	1,889,712.4							

**RESULTS: SOUND LEVELS** 

3536.2

**RECON Environmental** 

Jessica Fleming

24 February 2011

**TNM 2.5** 

Calculated with TNM 2.5

RESULTS: SOUND LEVELS

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - Measured Receivers

BARRIER DESIGN:

INPUT HEIGHTS

0

0.0

0.0

Average pavement type shall be used unless

a State highway agency substantiates the use

of a different type with approval of FHWA.

ATMOSPHERICS:

65 deg F, 69% RH

No.   House   Existing   LAeq1h   LAeq1h   LAeq1h   LAeq1h   Calculated   Crit'n   Calculated   Calculat	Receiver								or a unite	ent type with	approval of	FHWA.		
LAeq1h	Name	No.	#DUs	Existing	No Barrier					With Barrier				
Sub'l Inc   Sub'				LAeq1h			1	existing	Туре	-		ction		
3 1 0.0 66.6 66 66.6 10 Snd Lvl 66.6 0.0 8 -8.0  Dwelling Units  # DUs Noise Reduction Min Avg Max dB dB  dB dB dB  MI Selected 2 0.0 0.0 0.0 0.0						Crit'n	Calculated	1	Impact	LAeq1h	Calculated	Goal	minus	
3 1 0.0 66.6 66 66.6 10 Snd Lvl 66.6 0.0 8 -8.0  Dwelling Units  # DUS Noise Reduction Min Avg Max dB dB dB  All Selected 2 0.0 0.0 0.0 0.0				dBA	dBA	dBA	dB	dB		dBA	dB	dB		
4 1 0.0 63.7 66 63.7 10 63.7 0.0 8 -8.0  Dwelling Units  # DUS Noise Reduction Min Avg Max dB dB dB  All Selected 2 0.0 0.0 0.0 0.0	2	3	1	0.0	66.6	66	66.6	10	Sndlyl	66.6	-			
Dwelling Units         # DUS Min         Noise Reduction Max         Max           All Selected         2         0.0         0.0         0.0	3	4	1	0.0	63.7			-				-	8	-8.0
dB dB dB  All Selected 2 0.0 0.0 0.0	Dwelling Units		# DUs				03.7	10		63.7	0.0	)	8	-8.0
All Selected 2 0.0 0.0 0.0				Min	Avg	Max								
All Selected 2 0.0 0.0 0.0				dB	dB	dB								
All Impacted	All Selected		2	0.0	0.0									
	All Impacted		- 1	0.0										
1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	All that meet NR Goal		,		0.0									Í

0.0

## **ATTACHMENT 3**

TNM Input/Output—Future Conditions, Contour Receivers

22 February 2011 TNM 2.5

INPUT: ROADWAYS

RUN:

PROJECT/CONTRACT:

3536.2

**Castlerock - Contour Receivers** 

Average pavement type shall be used unless a State highway agency substantiates the use of a different type with the approval of FHWA

Roadway		Points									
Name	Width	Name	No.	Coordinates	(pavement)		Flow Co			Segment	
				X	Υ	Z	Control Device	Speed Constraint	Percent Vehicles Affected	Pvmt Type	On Struct?
	ft			ft	ft	ft		mph	%		
EB Mast west of school	12.0	1	1	6,324,981.5	1,889,224.6					Average	
		2	2	6,325,123.0	1,889,305.2	416.00				Aver <b>a</b> ge	
		3	3	6,325,334.0	1,889,402.8	-				Average	
		4	4			1				Average	
		5	5	6,325,700.0						Aver <b>a</b> ge	
		6	6				1				
EB Mast east of school	12.0	6	7	1	1,889,574.6	-				Average	
		7	8							Average	
		8	9							Average	
		9	10	6,326,799.5	1,889,715.9					Average	
		10	11	6,327,120.5			4			Average	
		11	12	6,327,211.5						Average	
		12	13	6,327,334.5	1,889,813.4					Average	
		13	14	6,327,502.0	1,889,830.2		1			Average	
		14	15	6,327,665.5	1,889,837.2					Average	
		15	16	6,327,813.0	1,889,837.2	402.00	)			Average	
		16	17	6,327,906.5	1,889,818.0	396.00	)			Average	
		17	18	6,328,096.0	1,889,791.1	383.10	)			Average	
		18	19	6,328,325.5	1,889,761.2						
WB Mast west of school	12.0	1	20	6,328,331.0	1,889,796.8	367.30	)			Average	
		2	21	6,328,100.0	1,889,832.8	383.10	ס			Average	
		3	22	6,327,910.0	1,889,860.4	396.00	)			Average	
		4	23	6,327,822.0	1,889,880.6	402.00	)			Average	
		5	24	6,327,672.0	1,889,879.6	412.00	0			Average	
		6	25	6,327,506.0	1,889,872.9	9 422.00	0			Average	

INPUT: ROADWAYS	3536.2
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		7 2	6,327,328.5	1,889,854.6	430.00	Average
- 2 2		8 2	6,327,201.0	1,889,836.6	434.00	Average
•		9 2	6,327,085.0	1,889,813.8	436.00	Average
		10 2	9 6,326,793.0	1,889,758.8	436.00	Average
		11 3	6,326,518.0	1,889,704.0	430.00	Average
		12 3	6,326,327.0	1,889,668.5	426.00	Average
		13 3	6,326,084.0	1,889,620.5	422.00	
WB Mast east of school	12.0	13 3	6,326,084.0	1,889,620.5	422.00	Average
		14 3	4 6,325,713.5	1,889,550.5	418.00	Average
		15 3	6,325,505.5	1,889,502.5	416.00	Average
		16 3	6 6,325,274.0	1,889,424.8	414.00	Average
		17 3	7 6,325,110.0	1,889,347.0	416.00	Average
		18 3	6,324,952.5	1,889,255.9	420.00	

**RECON Environmental** 

22 February 2011

Jessica Fleming

**TNM 2.5** 

INPUT: TRAFFIC FOR LAeq1h Volumes

PROJECT/CONTRACT: 3536.2

RUN: Castlerock - Contour Receivers

Roadway	Points											
Name	Name	No.	Segmen	it								
			Autos		MTrucks	S	HTruck	S	Buses		Motorc	ycles
			V	S	V	S	V	S	V	S	V	S
			veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph
EB Mast west of school	1	1	848	45	17	45	5 9	9 45				
	2	2	848	45	17	45	5 9	45				
	3	3	848	45	17	45	5 9	9 45				
	4	4	848	45	17	45	5 9	45			ii .	
	5	5	848	45	17	45	5 9	9 45				
	6	6										
EB Mast east of school	6	7	820	45	17	45	5 8	3 45				
	7	8	820	45	17	45	5 8	3 45				
	8	9	820	45	17	45	5 8	3 45				
	9	10	820	45	17	45	5 8	3 45				
	10	11	820	45	17	45	5 8	3 45				
	11	12	820	45	17	45	5 8	3 45				
	12	13	820	45	17	45	5 8	3 45				
	13	14	820	45	17	45	5 8	3 45				
	14	15	820	45	17	45	5 8	3 45				
	15	16	820	45	17	45	5 8	3 45				
	16	17	820	45	17	45	5 8	3 45				
	17	18	820	45	17	45	5 8	3 45				
	18	19										
WB Mast west of school	1	20	848	45	17	45	5 9	9 45				
	2	21	848	45	17	45	5 9	45				
	3	22	848	45	17	45	5 9	9 45				

INPUT: TRAFFIC FOR LAe 1h Vo	lumes					3536.2	2		
	4	23	848	45	17	45	9	45	
	5	24	848	45	17	45	9	45	
	6	25	848	45	17	45	9	45	
	7	26	848	45	17	45	9	45	
	8	27	848	45	17	45	9	45	
	9	28	848	45	17	45	9	45	
	10	29	848	45	17	45	9	45	
	11	30	848	45	17	45	9	45	
	12	31	848	45	17	45	9	45	
	13	32					İ		
WB Mast east of school	13	33	820	45	17	45	8	45	
	14	34	820	45	17	45	8	45	
	15	35	820	45	17	45	8	45	
	16	36	820	45	17	45	8	45	
	17	37	820	45	17	45	8	45	
	18	38					1		

**RECON Environmental** 

Jessica Fleming

22 February 2011

**TNM 2.5** 

**INPUT: RECEIVERS** 

PROJECT/CONTRACT:

3536.2

RUN:

**Castlerock - Contour Receivers** 

Name	No.	#DII-	Coordinates	/aua		11.1.1.					
Name	INO.	#DUS	Coordinates		_	Height			and Criteria		Active
			X	Υ	Z	above	Existing	Impact Cr		NR	in
						Ground	LAeq1h	LAeq1h	Sub'l	Goal	Calc.
			ft	ft	ft	ft	dBA	dBA	dB	dB	
1	5	1	6,325,878.5	1,889,719.1	457.50	5.00	0.00	66	10.0	8.	0 Y
2	6	1	6,325,971.5	1,889,753.5	457.00	5.00	0.00	66	10.0	8.	0 Y
3	7	1	6,326,013.0	1,889,743.0	457.00	5.00	0.00	66	10.0	8.	0 Y
4	8	1	6,326,012.5	1,889,795.5	458.50	5.00	0.00	66	10.0	8.	0 Y
5	9	1	6,326,077.0	1,889,787.4	457.00	5.00	0.00	66	10.0	8.0	0 Y
6	10	1	6,325,784.0	1,890,267.2	480.00	5.00	0.00	66	10.0	8.0	0 Y
7	11	1	6,326,172.0	1,889,804.6	457.50	5.00	0.00	66	10.0	8.0	0 Y
8	12	1	6,326,220.5	1,889,812.8	457.50	5.00	0.00	66	10.0	8.0	0 Y
9	13	1	6,326,375.5	1,890,421.2	456.00	5.00	0.00	66	10.0	8.0	0 Y
10	14	1	6,326,316.0	1,889,830.0	458.50	5.00	0.00	66	10.0	8.0	0 Y
11	15	1	6,326,865.0	1,889,952.2	455.00	5.00	0.00	66	10.0	8.0	Y C
12	16	1	6,326,927.0	1,889,881.1	455.00	5.00	0.00	66	10.0	8.0	Y C
13	17	1	6,327,030.5	1,889,971.8	454.50	5.00	0.00	66	10.0	8.0	Y
14	18	1	6,327,117.0	1,890,069.1	443.00	5.00	0.00	66	10.0	8.0	Y C
15	19	1	6,327,131.0	1,889,955.0	438.00	5.00	0.00	66	10.0	8.0	) Y
16	20	1	6,326,098.5	1,889,895.5	456.00	5.00	0.00	66	10.0	8.0	) Y
17	21	1	6,326,215.5	1,889,951.0	445.50	5.00	0.00	66	10.0	8.0	) Y
18	22	1	6,325,866.0	1,889,808.9	457.50	5.00	0.00	66	10.0	8.0	) Y
19	23	1	6,327,257.5	1,889,942.9	444.00	5.00	0.00	66	10.0	8.0	Y
20	24	1	6,327,386.5	1,889,969.1	445.00	5.00	0.00	66	10.0	8.0	) Y
21	25	1	6,327,471.5	1,889,989.2	445.00	5.00	0.00	66	10.0	8.0	) Y
22	26	1	6,327,563.0	1,890,011.4	442.00	5.00	0.00	66	10.0	8.0	) Y

INPUT: RECEIVERS							35	36.2			
23	27	1	6,327,715.0	1,890,029.5	441.50	5.00	0.00	66	10.0	8.0	Y
24	28	1	6,327,699.5	1,890,134.2	442.00	5.00	0.00	66	10.0	8.0	Υ
25	29	1	6,327,191.0	1,890,082.8	445.50	5.00	0.00	66	10.0	8.0	Υ
26	30	1	6,327,351.5	1,890,154.0	449.50	5.00	0.00	66	10.0	8.0	Υ
27	31	1	6,327,133.5	1,890,440.2	480.00	5.00	0.00	66	10.0	8.0	Υ
28	32	1	6,327,225.0	1,889,974.9	444.00	5.00	0.00	66	10.0	8.0	Υ
29	33	1	6,327,269.0	1,890,017.2	444.00	5.00	0.00	66	10.0	8.0	Υ
30	34	1	6,327,521.5	1,890,042.9	442.00	5.00	0.00	66	10.0	8.0	Υ
31	35	1	6,327,798.5	1,890,441.2	453.50	5.00	0.00	66	10.0	8.0	Υ
32	36	1	6,325,934.0	1,889,670.8	445.00	5.00	0.00	66	10.0	8.0	Υ
33	37	1	6,326,135.0	1,889,706.6	445.00	5.00	0.00	66	10.0	8.0	Υ
34	38	1	6,326,331.5	1,889,734.6	445.00	5.00	0.00	66	10.0	8.0	Υ
35	39	1	6,327,418.5	1,889,942.6	445.00	5.00	0.00	66	10.0	8.0	Υ
36	40	1	6,327,622.5	1,889,985.5	441.50	5.00	0.00	66	10.0	8.0	Υ
37	38	1	6,326,622.5	1,889,848.0	457.50	5.00	0.00	66	10.0	8.0	Υ

**INPUT: BARRIERS** 

3536.2

**RECON Environmental** 

Jessica Fleming

22 February 2011

TNM 2.5

INPUT: BARRIERS

PROJECT/CONTRACT:

3536.2

RUN:

**Castlerock - Contour Receivers** 

Barrier									Points									
Name	Type	Height		if Wall	If Berm			Add'tnl	Name	No.	Coordinates	(bottom)		Height	Segmen	nt		
		Min	Max	Unit Area	\$ per Unit Vol.	Top Width	Run:Rise	S per Unit Length		man and the	X	Υ	Z		Seg Ht Incre- ment		bs On On Struc	Important ? Reflec- tions?
***		ft	ft	S/sq ft	\$/cu yd	ft	ft:ft	S/ft			ft	ft	ft	ft	ft			
Pad Edges West	W	0.00	99.99	0.00				0.00	1	41	6,325,546.5	1,889,712.0	450.00	0.00	0.00	0	0	
Market Control of the									2	42	6,325,604.0	1,889,625.2	450.00	0.00	0.00	0	0	
									3	43	6,327,038.0	1,889,858.4	450.00	0.00	0.00	0	0	
									4	44	6,327,067.0	1,889,891.2	450.00	0.00	0.00	0	0	
									5	45	6,327,055.0	1,890,029.9	450.00	0.00				
Pad Edges East	W	0.00	99.99	0.00				0.00	6	46	6,327,161.0	1,890,012.6	440.00	0.00	0.00	0	0	
									7	47	6,327,186.0	1,889,925.9	440.00	0.00	0.00	0	0	
									8	48	6,327,257.5	1,889,897.0	440.00	0.00	0.00	0	0	
									9	49	6,327,485.0	1,889,937.4	440.00	0.00	0.00	0	0	
									10	50	6,327,620.0	1,889,966.2	440.00	0.00	0.00	0	0	
7-17-1									11	51	6,327,749.0	1,889,987.5	440.00	0.00	0.00	0	0	
									12	52	6,327,807.0	1,890,214.9	440.00	0.00	0.00	0	0	
									13	53	6,327,853.0	1,890,515.6	450.00	0.00				

22 February 2011

**TNM 2.5** 

Calculated with TNM 2.5

**RESULTS: SOUND LEVELS** 

PROJECT/CONTRACT:

3536.2

RUN:

**Castlerock - Contour Receivers** 

BARRIER DESIGN:

**INPUT HEIGHTS** 

Average pavement type shall be used unless a State highway agency substantiates the use of a different type with approval of FHWA.

ATMOSPHERICS:

65 deg F, 69% RH

Receiver													
Name	No.	#DUs	Existing	No Barrier					With Barrier				
				LAeq1h Calculated	Crit'n	Increase over Calculated	Crit'n Sub'l Inc	Type impact	Calculated LAeq1h	Noise Reduc Calculated	tion Goal	Calcu minus Goal	
			dBA	dBA	dBA	dB	dB		dBA	dB	dB	dB	
1	5		0.0	62.6			10		62.6	0.0		8	-8.0
2	6		0.0	58.7	66	58.7	10		58.7	0.0		8	-8.0
3	7		0.0	62.7	66	62.7	10		62.7	0.0		8	-8.0
4	8	1	0.0	55.4	66	55.4	10		55.4	0.0		8	-8.0
5	9		0.0	56.9	66	56.9	10		56.9	0.0		8	-8.0
6	10		0.0	49.4	66	49.4	10		49.4	0.0		8	-8.0
7	11	1	0.0	57.5	66	57.5	10		57.5	0.0		8	-8.0
8	12	1	0.0	57.7	66	57.7	10		57.7	0.0		8	-8.0
9	13	1	0.0	43.8	66	43.8	10		43.8	0.0		8	-8.0
10	14	1	0.0	59.0	66	59.0	10		59.0	0.0		8	-8.0
11	15		0.0	57.3	66	57.3	10		57.3	0.0		8	-8.0
12	16	1	0.0	65.9	66	65.9	10		65.9	0.0		8	-8.0
13	17		0.0	61.2	66	61.2	10		61.2	0.0		8	-8.0
14	18		0.0	58.4	66	58.4	10		58.4	0.0		8	-8.0
15	19		0.0	64.0	66	64.0	10		64.0	0.0		8	-8.0
16	20	1	0.0	50.2	66	50.2	10		50.2	0.0		8	-8.0
17	21	1	0.0	47.5	66	47.5	10		47.5	0.0		8	-8.0
18	22	1	0.0	52.0	66	52.0	10	••••	52.0	0.0		8	-8.0
19	23	1	0.0	66.0	66	66.0	10	Snd Lvl	66.0	0.0		8	-8.0
20	24		0.0	65.0	66	65.0	10		65.0	0.0		8	-8.0
21	25	1	0.0	63.7	66	63.7	10		63.7	0.0		8	-8.0
22	26	1	0.0	60.4	66	60.4	10		60.4	0.0		8	-8.0
23	27	1	0.0	60.3	66	60.3	10		60.3	0.0		8	-8.0

RESULTS: SOUND LEVELS		-					353	6.2					
25	28		0.0	54.3	3	66	54.3	10		54.3	0.0	8	-8.0
26	29	1	0.0	58.4	1	66	58.4	10	122 (123)	58.4	0.0	8	
	30	1	0.0	56.2	2	66	56.2	10		56.2	0.0	8	-8.0
27	31	1	0.0	51.6	3	66	51.6	10		51.6	0.0		-8.0
28	32	1	0.0	63.5	5	66	63.5	10		63.5		8	-8.0
29	33	1	0.0	61.1		66	61.1	10		61.1	0.0	8	-8.0
30	34	1	0.0	57.8	}	66	57.8	10		57.8	0.0	8	-8.0
31	35	1	0.0		_	66	53.9	10			0.0	8	-8.0
32	36	1	0.0		+	66	67.1	10	Snd Lvl	53.9	0.0	8	-8.0
33	37	1	0.0			66	67.4			67.1	0.0	8	-8.0
34	38	1	0.0			66		10	Snd Lvl	67.4	0.0	8	-8.0
35	39	1	0.0				68.0	10	Snd Lvl	68.0	0.0	8	-8.0
36	40	- 1	0.0		-	66	67.1	10	Snd LvI	67.1	0.0	8	-8.0
37	38	<u>'</u>			-	66	66.0	10	Snd LvI	66.0	0.0	8	-8.0
Dwelling Units			0.0			66	64.0	10		64.0	0.0	8	-8.0
Dwening Offics		# DUs											
			Min	Avg	Max								
			dB	dB	dB								
All Selected		37	0.0	0.0		0.0							
All Impacted		6		0.0		0.0							
All that meet NR Goal		0				0.0							

## **ATTACHMENT 4**

TNM Input/Output—Future Conditions, Modeled Receivers

22 February 2011 TNM 2.5

**INPUT: ROADWAYS** 

PROJECT/CONTRACT:

3536.2

RUN: Castlerock - 1st Floor Receivers

Average pavement type shall be used unless a State highway agency substantiates the use of a different type with the approval of FHWA

3536.2

Roadway		Points									
Name	Width	Name	No.	Coordinates	(pavement)		Flow Cor	ntrol		Segment	
				X	Y	Z	Control Device	Speed Constraint	Percent Vehicles Affected	Pvmt Type	On Struct?
	ft			ft	ft	ft		mph	%		
EB Mast west of school	12.0	1	1	6,324,981.5	1,889,224.6	420.00				Average	
		2	2							Average	
		3	3	6,325,334.0						Average	
		4	4	6,325,487.5		416.00				Average	
		5	5	6,325,700.0	1,889,504.0	418.00				Average	
		6	6	6,326,073.0	1,889,574.6	422.00					
EB Mast east of school	12.0	6	7	6,326,073.0	1,889,574.6	422.00				Average	
		7	8	6,326,324.5	1,889,623.0	426.00				Average	
		8	9	6,326,499.5	1,889,657.5	430.00				Average	
		9	10	6,326,799.5	1,889,715.9	436.00				Average	
		10	11	6,327,120.5	1,889,777.4	4 <b>3</b> 6.00				Average	
		11	12	6,327,211.5	1,889,795.0	434.00				Average	
		12	13	6,327,334.5	1,889,813.4	430.00				Average	
		13	14	6,327,502.0	1,889,830.2	422.00				Average	
		14	15	6,327,665.5	1,889,837.2	412.00				Average	
		15	16	6,327,813.0	1,889,837.2	402.00				Average	
		16	17	6,327,906.5	1,889,818.0	396.00				Average	
		17	18	6,328,096.0	1,889,791.1	383.10				Average	
		18	19	6,328,325.5	1,889,761.2	367.30				J	
WB Mast west of school	12.0	1	20	6,328,331.0	1,889,796.8	367.30				Average	
		2	21	6,328,100.0	1,889,832.8	383.10				Average	
		3	22	6,327,910.0	1,889,860.4	396.00				Average	
		4	23	6,327,822.0	1,889,880.6	402.00				Average	
		5	24	6,327,672.0	1,889,879.6	412.00				Average	
		6	25	6,327,506.0	1,889,872.9	422.00				Average	

1

INPUT: ROADWAYS 3536.2

NPUT: ROADWAYS					3330.2	
		7 26	6,327,328.5	1,889,854.6	430.00	Average
		8 27	6,327,201.0	1,889,836.6	434.00	Average
		9 28	6,327,085.0	1,889,813.8	436.00	Average
		10 29	6,326,793.0	1,889,758.8	436.00	Average
		11 30	6,326,518.0	1,889,704.0	430.00	Average
		12 31	6,326,327.0	1,889,668.5	426.00	Average
		13 32	6,326,084.0	1,889,620.5	422.00	
VB Mast east of school	12.0	13 33	6,326,084.0	1,889,620.5	422.00	Average
		14 34	6,325,713.5	1,889,550.5	418.00	Average
		15 35	6,325,505.5	1,889,502.5	416.00	Average
		16 36	6,325,274.0	1,889,424.8	414.00	Average
		17 37	6,325,110.0	1,889,347.0	416.00	Average
		18 38	6,324,952.5	1,889,255.9	420.00	

22 February 2011 TNM 2.5

INPUT: TRAFFIC FOR LAeq1h Volumes

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - 1st Floor Receivers

Roadway	Points											
Name	Name	No.	Segmen	t								
			Autos		MTrucks	5	HTruck	5	Buses		Motorc	ycles
			V	S	V	S	V	S	V	S	V	S
			veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph
EB Mast west of school	1	1	848	45	17	45	9		.1			
	2	2	848	45	17	45	9	45				
	3	3	848	45	17	45	9	45				
	4	4	848	45	17	45	9	45				
	5	5	848	45	17	45	9	45				
	6	6										
EB Mast east of school	6	7	820	45	17	45	8	3 45	5			
	7	8	820	45	17	45	5 8	3 45	5			
	8	9	820	45	17	45	5 8	3 45	5			
	9	10	820	45	17	45	5 8	3 45	5			
	10	11	820	45	17	45	5 4	3 45	5			
	11	12	820	45	17	45	5	3 45				
	12	13	820	45	17	45	5	3 45	5			
	13	14	820	45	17	45	5	8 45	5			
	14	15	820	45	17	45	5	8 45	5			
	15	16	820	45	17	45	5	B 45	5			
	16	17	820	45	5 17	45	5	8 45				
	17	18	820	45	17	45	5	8 4	5			
	18	19	9									
WB Mast west of school	1	20	848	45	17	45	5	9 4	5			
	2	2	1 848	3 45	17	7 45	5	9 4				
	3	22	2 848	3 45	5 17	7 45	5	9 4	5			

INPUT: TRAFFIC FOR LAeq1h Vo	lumes					3536.2	2		
	4	23	848	45	17	45	9	45	
	5	24	848	45	17	45	9	45	
	6	25	848	45	17	45	9	45	
	7	26	848	45	17	45	9	45	
	8	27	848	45	17	45	9	45	
	9	28	848	45	17	45	9	45	
	10	29	848	45	17	45	9	45	
	11	30	848	45	17	45	9	45	
	12	31	848	45	17	45	9	45	
	13	32							
WB Mast east of school	13	33	820	45	17	45	8	45	
	14	34	820	45	17	45	8	45	
	15	35	820	45	17	45	8	45	
	16	36	820	45	17	45	8	45	
	17	37	820	45	17	45	8	45	
	18	38							

INPUT: RECEIVERS

**RECON Environmental** 

Jessica Fleming

22 February 2011

3536.2

**TNM 2.5** 

**INPUT: RECEIVERS** 

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - 1st Floor Receivers

Receiver						1	i				
Name	No.	#DUs	Coordinates			Height	1		and Criteria		Active
			X	Y	Z	above	Existing	Impact Cr		NR	in
			au yyy			Ground	LAeq1h	LAeq1h	Sub'l	Goal	Calc.
			ft	ft	ft	ft	dBA	dBA	dB	dB	
1	40	1	6,325,669.0	1,889,651.2	454.00	5.00	0.00	66	10.0	8	.0 Y
2	41	1	6,325,861.0	1,889,690.0	457.50	5.00	0.00	66	10.0	8	.0 Y
3	42	1	6,326,074.0	1,889,725.9	457.00	5.00	0.00	66	10.0	8	.0 Y
4	43	1	6,326,232.0	1,889,752.6	457.50	5.00	0.00	66	10.0	8	.0 Y
5	44	1	6,326,344.5	1,889,768.1	456.50	5.00	0.00	66	10.0	8	.0 Y
6	45	1	6,326,455.0	1,889,788.5	458.50	5.00	0.00	66	10.0	8	.0 Y
7	46	1	6,326,570.5	1,889,806.1	458.50	5.00	0.00	66	10.0	8	.0 Y
8	47	1	6,326,667.0	1,889,818.0	457.50	5.00	0.00	66	10.0	8	.0 Y
9	48	1	6,326,792.5	1,889,833.5	456.00	5.00	0.00	66	10.0	8	.0 Y
10	49	1	6,326,905.5	1,889,853.2	455.00	5.00	0.00	66	10.0	8	.0 Y
11	50	1	6,326,998.0	1,889,870.1	454.60	5.00	0.00	66	10.0	8	.0 Y
12	51	1	6,327,045.5	1,889,936.2	454.60	5.00	0.00	66	10.0	8	.0 Y
13	52	1	6,327,038.5	1,890,012.2	454.60	5.00	0.00	66	10.0	8	.0 Y
14	53	1	6,327,171.0	1,889,996.8	445.50	5.00	0.00	66	10.0	8	0 Y
15	54	1	6,327,216.0	1,889,921.5	443.90	5.00	0.00	66	10.0	8	0 Y
16	55	1	6,327,297.0	1,889,918.0	443.90	5.00	0.00	66	10.0	8	0 Y
17	56	1	6,327,423.5	1,889,945.5	445.00	5.00	0.00	66	10.0	8	.0 Y
18	57	1	6,327,560.0	1,889,971.5	442.20	5.00	0.00	66	10.0	8	.0 Y
19	58	1	6,327,689.5	1,889,990.5	441.50	5.00	0.00	66	10.0	8	.0 Y
20	59	1	6.327.779.0	1,890,191.0	443.50	5.00	0.00	66	10.0	8	.0 Y

INPUT: BARRIERS 3536.2

RECON Environmental

22 February 2011

Jessica Fleming

TNM 2.5

INPUT: BARRIERS

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - 1st Floor Receivers

Barrier									Points									
Name	Туре	Height		If Wall	If Berm	ı		Add'tnl	Name	No.	Coordinates	(bottom)		Height	Segme	ent		
		Min	Max	\$ per Unit Area	\$ per Unit Vol.	Top Width	Run:Rise	S per Unit Length			X	Y	Z	at Point		Perturbs #Up #Dr		Importan Reflec- tions?
		ft	ft	S/sq ft	\$/cu yd	ft	ft:ft	S/ft			ft	ft	ft	ft	ft			
West Pad Edges	W	0.00	99.99	0.00				0.00	1	54	6,325,595.0	1,889,653.2	454.00	0.00	1.00	6	0	
									2	55	6,325,603.5	1,889,639.6	454.00	0.00	1.00	6	0	
					1				3	56	6,325,618.0	1,889,635.2	454.00	0.00	1.00	6	0	
									4	57	6,325,749.0	1,889,660.2	454.00	0.00	1.00	6	0	
			İ						5	58	6,325,769.5	1,889,668.5	457.50	0.00	1.00	6	0	
					-				6	59	6,325,949.5	1,889,697.5	457.50	0.00	1.00	6	0	
									7	60	6,325,960.5	1,889,699.6	457.00	0.00	1.00	6	0	
							*		8	61	6,326,159.5	1,889,734.4	457.00	0.00	1.00	6	0	
							1		9	62	6,326,170.0	1,889,737.1	457.50	0.00	1.00	6	0	
									10		6,326,294.0			0.00	1.00	6	0	
									11	64	6,326,306.0	1,889,756.2	456.50	0.00	1.00	6	0	
									12	65	6,326,385.0	1,889,768.0	456.50	0.00	1.00	6	0	
									13	66	6,326,398.5	1,889,774.0	458.50	0.00	1.00	6	0	
									14	67	6,326,613.5	1,889,806.1	458.50	0.00	1.00	6	0	
		†							15	68	6,326,626.0	1,889,806.0	457.50	0.00	1.00	6	0	
									16	69	6,326,709.0	1,889,817.8	457.50	0.00	1.00	6	0	
									17	70	6,326,728.5	1,889,818.2	456.00	0.00	1.00	6	0	
									18	71	6,326,851.0	1,889,838.0	456.00	0.00	1.00	6	0	
									19	72	6,326,868.5	1,889,839.0	455.00	0.00	1.00	6	0	
									20	73	6,326,941.0	1,889,852.8	455.00	0.00	1.00	6	0	i i
									21	74	6,326,951.5	1,889,854.0	454.60	0.00	1.00	6	0	
									22	75	6,327,033.0	1,889,870.8	454.60	0.00	1.00	6	0	
									23	76	6,327,055.5	1,889,901.6	454.60	0.00	1.00	6	0	1
									24	77	6,327,044.0	1,890,039.2	454.60	0.00	)			
East Pad Edges	W	0.00	99.99	0.00	)			0.00	-		6,327,159.0		-	0.00	1.00	6	0	
						1	1	1.07	26		6,327,181.5		1	0.00	1.00	6	0	
						1			27		6,327,213.0		-	0.00	1.00	6	0	
				1	100	1	1		28		6,327,247.5	1		0.00	1.00	6	0	
		†			+	+			29		6,327,289.0		_		-		0	
			-			+			30		6,327,361.0		-				0	
			1		1				31		6,327,474.5		-		1		0	
				-	1				32		6,327,504.0	1			1		0	
				+	1		+		33		6,327,621.5			-	_		0	
		1	+			-	+	+	34		6,327,728.5		-	-	_		0	-
		-				-	-	1	35		6,327,752.0		-	-	1.00		0	+

**INPUT: BARRIERS** 

3536.2

	36	89 6,327,760.5 1,890,010.6 441.50	0.00 1.00 6 0
	37	90 6,327,809.0 1,890,225.8 440.00	0.00

22 February 2011

**TNM 2.5** 

Calculated with TNM 2.5

**RESULTS: SOUND LEVELS** 

PROJECT/CONTRACT:

3536.2

RUN:

**Castlerock - 1st Floor Receivers** 

**BARRIER DESIGN:** 

INPUT HEIGHTS

Average pavement type shall be used unless a State highway agency substantiates the use of a different type with approval of FHWA.

ATMOSPHERICS:

65 deg F, 69% RH

Name	No.	#DUs	Existing	No Barrier					With Barrier			
			LAeq1h	h LAeq1h I		Increase over existing T		Туре	Calculated	Noise Reduc	tion	
				Calculated	Crit'n	Calculated	Crit'n Sub'l inc	Impact	LAeq1h	Calculated	Goal	Calculated minus Goal
			dBA	dBA	dBA	dB	dB		dBA	dB	dB	dB
1	40	1	0.0	65.9	66	65.9	10	••••	65.9	0.0		8 -8.
2	41	1	0.0	66.0	66	66.0	10	Snd Lvl	66.0	0.0		8 -8.
3	42	1	0.0	66.3	66	66.3	10	Snd Lvl	66.3	0.0		8 -8.
4	43	1	0.0	66.5	66	66.5	10	Snd Lvl	66.5	0.0		8 -8.
5	44	1	0.0	66.8	66	66.8	10	Snd Lvl	66.8	0.0		8 -8.
6	45	1	0.0	66.8	66	66.8	10	Snd Lvl	66.8	0.0		8 -8.
7	46	1	0.0	67.0	66	67.0	10	Snd Lvl	67.0	0.0		8 -8.
8	47	1	0.0	67.4	66	67.4	10	Snd Lvl	67.4	0.0		8 -8.
9	48	1	0.0	67.8	66	67.8	10	Snd Lvl	67.8	0.0		8 -8.
10	49	1	0.0	67.9	66	67.9	10	Snd Lvl	67.9	0.0		8 -8.
11	50	1	0.0	67.9	66	67.9	10	Snd Lvl	67.9	0.0		8 -8.
12	51	1	0.0	62.8	66	62.8	10		62.8	0.0		8 -8.
13	52	1	0.0	59.4	66	59.4	10		59.4	0.0	İ	8 -8.
14	53	1	0.0	61.4	66	61.4	10		61.4	0.0		8 -8.
15	54	1	0.0	66.7	66	66.7	10	Snd Lvl	66.7	0.0		8 -8.
16	55	1	0.0	68.2	66	68.2	10	Snd Lvl	68.2	0.0		8 -8.
17	56	1	0.0	67.4	66	67.4	10	Snd Lvl	67.4	0.0		8 -8.
18	57	1	0.0	66.7	66	66.7	10	Snd Lvl	66.7	0.0		8 -8.
19	58	1	0.0	66.1	66	66.1	10	Snd Lvl	66.1	0.0		8 -8.
20	59	1	0.0	57.2	66	57.2	10		57.2	0.0		8 -8.

Dwelling Units	# DUs	Noise i	Reduction		
		Min	Avg	Max	
		dB	dB	dB	

## RESULTS: SOUND LEVELS

3536.2

All Selected	20	0.0	0.0	0.0
All Impacted	15	0.0	0.0	0.0
All that meet NR Goal	0	0.0	0.0	0.0

RECON Environmental

Jessica Fleming

22 February 2011

**TNM 2.5** 

INPUT: RECEIVERS

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - 2nd Floor Receivers

Name	No	No. #DUs Coordinates (ground)			Height	Input Sou	out Sound Levels and Criteria				
Name	No.	#DUS	X ft	Υ	Z	above Ground		Impact Criteria		a NR	Active in
					ft			<b>LAeq1h</b> dBA	Sub'l	Goal	Calc.
										dB	
1	40	1	6,325,669.0	1,889,651.2	454.00	15.00	0.00	66	10.0	8.	0 Y
2	41	1	6,325,861.0	1,889,690.0	457.50	15.00	0.00	66	10.0	8.	0 Y
3	42	1	6,326,074.0	1,889,725.9	457.00	15.00	0.00	66	10.0	8.	0 Y
4	43	1	6,326,232.0	1,889,752.6	457.50	15.00	0.00	66	10.0	8.	0 Y
5	44	1	6,326,344.5	1,889,768.1	456.50	15.00	0.00	66	10.0	8.	0 Y
6	45	1	6,326,455.0	1,889,788.5	458.50	15.00	0.00	66	10.0	8.	0 Y
7	46	1	6,326,570.5	1,889,806.1	458.50	15.00	0.00	66	10.0	8.	0 Y
8	47	1	6,326,667.0	1,889,818.0	457.50	15.00	0.00	66	10.0	8.	0 Y
9	48	1	6,326,792.5	1,889,833.5	456.00	15.00	0.00	66	10.0	8.	0 Y
10	49	1	6,326,905.5	1,889,853.2	455.00	15.00	0.00	66	10.0	8.	0 Y
11	50	1	6,326,998.0	1,889,870.1	454.60	15.00	0.00	66	10.0	8.	0 Y
12	51	1	6,327,045.5	1,889,936.2	454.60	15.00	0.00	66	10.0	8.	0 Y
13	52	1	6,327,038.5	1,890,012.2	454.60	15.00	0.00	66	10.0	8.	0 Y
14	53	1	6,327,171.0	1,889,996.8	445.50	15.00	0.00	66	10.0	8.	0 Y
15	54	1	6,327,216.0	1,889,921.5	443.90	15.00	0.00	66	10.0	8.	0 Y
16	55	1	6,327,297.0	1,889,918.0	443.90	15.00	0.00	66	10.0	8.	0 Y
17	56	1	6,327,423.5	1,889,945.5	445.00	15.00	0.00	66	10.0	8.	0 Y
18	57	1	6,327,560.0	1,889,971.5	442.20	15.00	0.00	66	10.0	8.	0 Y
19	58	1	6,327,689.5	1,889,990.5	441.50	15.00	0.00	66	10.0	8.	0 Y
20	59	1	6,327,779.0	1,890,191.0	443.50	15.00	0.00	66	10.0	8.6	0 Y

22 February 2011

**TNM 2.5** 

Calculated with TNM 2.5

**RESULTS: SOUND LEVELS** 

PROJECT/CONTRACT:

3536.2

RUN:

Castlerock - 2nd Floor Receivers

BARRIER DESIGN:

**INPUT HEIGHTS** 

Average pavement type shall be used unless a State highway agency substantiates the use of a different type with approval of FHWA.

ATMOSPHERICS:

65 deg F, 69% RH

No.	#DUs	Existing	No Barrier					With Barrier			
		LAeq1h	LAeq1h		Increase over existing		Туре	Calculated	Noise Reduction		
			Calculated	Crit'n	Calculated	Crit'n Sub'i inc	Impact	LAeq1h	Calculated	Goal	Calculated minus Goal
		dBA	dBA	dBA	dB	dB		dBA	dB	dB	dB
40	1	0.0	65.5	66	65.5	10		65.5	0.0		8 -8
41	1	0.0	65.6	66	65.6	10		65.6	0.0		8 -8
42	1	0.0	65.9	66	65.9	10		65.9	0.0		8 -8
43	1	0.0	66.2	66	66.2	10	Snd Lvl	66.2	0.0		8 -8
44	1	0.0	66.5	66	66.5	10	Snd Lvl	66.5	0.0		8 -8
45	1	0.0	66.6	66	66.6	10	Snd Lvl	66.6	0.0		8 -8
46	1	0.0	66.8	66	66.8	10	Snd Lvl	66.8	0.0		8 -8
47	1	0.0	67.1	66	67.1	10	Snd Lvl	67.1	0.0		8 -8
48	1	0.0	67.6	66	67.6	10	Snd Lvi	67.6	0.0		8 -8
49	1	0.0	67.7	66	67.7	10	Snd Lvl	67.7	0.0		8 -8
50	1	0.0	67.7	66	67.7	10	Snd Lvl	67.7	0.0		8 -8
51	1	0.0	64.3	66	64.3	10		64.3	0.0		8 -8
52	1	0.0	59.6	66	59.6	10		59.6	0.0		8 -8
53	1	0.0	61.9	66	61.9	10	****	61.9	0.0		8 -8
54	1	0.0	67.0	66	67.0	10	Snd Lvl	67.0	0.0		8 -8
55	1	0.0	67.8	66	67.8	10	Snd Lvl	67.8	0.0		8 -8
56	1	0.0	67.1	66	67.1	10	Snd Lvl	67.1	0.0		8 -8
57	1	0.0	66.2	66	66.2	10	Snd Lvl	66.2	0.0		8 -8
58	1	0.0	65.4	66	65.4	10		65.4	0.0		8 -8
59	1	0.0	57.5	66	57.5	10		57.5	0.0		8 -8
Dwelling Units		Noise Rec	luction								
	41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57	42 1 43 1 44 1 45 1 46 1 47 1 48 1 49 1 50 1 51 1 52 1 53 1 54 1 55 1 56 1 57 1 58 1	dBA  40	dBA         dBA           40         1         0.0         65.5           41         1         0.0         65.6           42         1         0.0         65.9           43         1         0.0         66.2           44         1         0.0         66.6           45         1         0.0         66.8           47         1         0.0         67.1           48         1         0.0         67.6           49         1         0.0         67.7           50         1         0.0         67.7           51         1         0.0         67.7           51         1         0.0         67.7           51         1         0.0         67.7           51         1         0.0         67.7           51         1         0.0         67.7           51         1         0.0         67.7           51         1         0.0         67.0           52         1         0.0         67.0           55         1         0.0         67.8           56         1         0.0<	dBA         dBA         dBA         dBA           40         1         0.0         65.5         66           41         1         0.0         65.6         66           42         1         0.0         65.9         66           43         1         0.0         66.2         66           44         1         0.0         66.5         66           45         1         0.0         66.6         66           46         1         0.0         66.8         66           47         1         0.0         67.1         66           48         1         0.0         67.6         66           49         1         0.0         67.7         66           50         1         0.0         67.7         66           51         1         0.0         67.7         66           52         1         0.0         59.6         66           53         1         0.0         67.0         66           54         1         0.0         67.8         66           55         1         0.0         67.1         66      <	dBA         dBA         dBA         dBA         dBA         dBA         dBA         dB           40         1         0.0         65.5         66         65.5           41         1         0.0         65.6         66         65.6           42         1         0.0         65.9         66         65.9           43         1         0.0         66.2         66         66.2           44         1         0.0         66.5         66         66.5           45         1         0.0         66.8         66         66.8           46         1         0.0         67.1         66         67.1           48         1         0.0         67.6         66         67.6           49         1         0.0         67.7         66         67.7           50         1         0.0         67.7         66         67.7           51         1         0.0         67.7         66         61.9           52         1         0.0         59.6         66         59.6           53         1         0.0         67.0         66         67.0	dBA         dBA         dBA         dBA         dBA         dBA         dBA         dB         dB           40         1         0.0         65.5         66         65.5         10           41         1         0.0         65.6         66         65.6         10           42         1         0.0         65.9         66         65.9         10           43         1         0.0         66.2         66         66.2         10           44         1         0.0         66.5         66         66.5         10           45         1         0.0         66.6         66         66.6         10           46         1         0.0         66.8         66         66.8         10           47         1         0.0         67.1         66         67.1         10           48         1         0.0         67.6         66         67.6         10           49         1         0.0         67.7         66         67.7         10           50         1         0.0         67.7         66         67.7         10           52         1 <td>dBA         dBA         dBA         dBA         dBA         dBA         dBA         dBA         dBA         dB         dB         lmpact           40         1         0.0         65.5         66         65.5         10            41         1         0.0         65.6         66         65.6         10            42         1         0.0         65.9         66         65.9         10            43         1         0.0         66.2         66         66.2         10         Snd Lvl           44         1         0.0         66.5         66         66.5         10         Snd Lvl           45         1         0.0         66.6         66         66.8         10         Snd Lvl           47         1         0.0         67.1         66         67.1         10         Snd Lvl           48         1         0.0         67.6         66         67.6         10         Snd Lvl           50         1         0.0         67.7         66         67.7         10         Snd Lvl           51         1         0.0         67.7<td>  Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h    </td><td>  Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h   Calculated   Calcula</td><td>  Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h   Calculated   Goal    </td></td>	dBA         dBA         dBA         dBA         dBA         dBA         dBA         dBA         dBA         dB         dB         lmpact           40         1         0.0         65.5         66         65.5         10            41         1         0.0         65.6         66         65.6         10            42         1         0.0         65.9         66         65.9         10            43         1         0.0         66.2         66         66.2         10         Snd Lvl           44         1         0.0         66.5         66         66.5         10         Snd Lvl           45         1         0.0         66.6         66         66.8         10         Snd Lvl           47         1         0.0         67.1         66         67.1         10         Snd Lvl           48         1         0.0         67.6         66         67.6         10         Snd Lvl           50         1         0.0         67.7         66         67.7         10         Snd Lvl           51         1         0.0         67.7 <td>  Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h    </td> <td>  Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h   Calculated   Calcula</td> <td>  Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h   Calculated   Goal    </td>	Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h	Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h   Calculated   Calcula	Calculated   Crit'n   Calculated   Crit'n   Sub'l Inc   Impact   LAeq1h   Calculated   Goal

Dwelling Units	# DUs	Noise i	loise Reduction		
		Min	Avg	Max	
		dB	dB	dB	